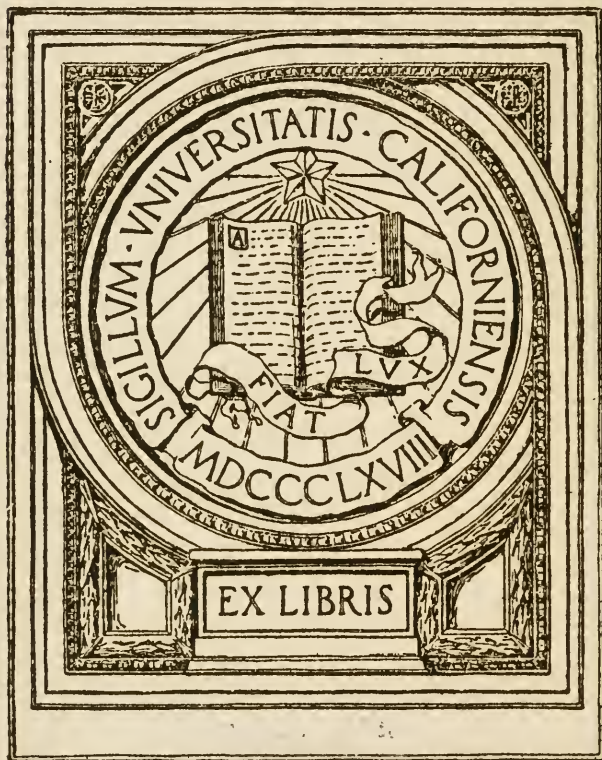
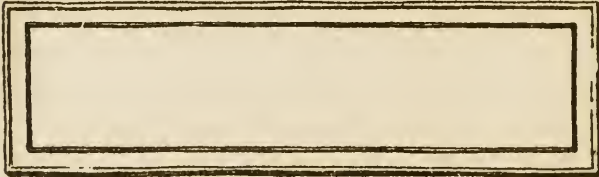


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A TREATISE  
ON  
ELEMENTARY STATICS.



# A TREATISE

ON

# ELEMENTARY STATICS

A handwritten signature in brown ink, reading "Greaves", written over a horizontal line that extends to the right and curves upwards at the end.

BY

JOHN GREAVES, M.A.,

FELLOW AND MATHEMATICAL LECTURER OF CHRIST'S COLLEGE, CAMBRIDGE.

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ANNALS OF THE PHYSICS

## PREFACE.

THERE has existed for some time past a general feeling that the Laws of Motion form the only satisfactory basis on which the science of Statics can be built. So far as I know, all the text-books in use in Cambridge except Prof. Minchin's, treat the subject from quite a different point of view. In this text-book I have endeavoured to supply the wants of students, who are not sufficiently advanced in Pure Mathematics, to read with advantage Professor Minchin's treatise on Analytical Statics.

Deducing from the Newtonian definition of force and the parallelogram of velocities, the *parallelogram of forces*, I obtain the *necessary* conditions of equilibrium for *any* material system by means of the third law, without assuming the *transmissibility of force*, or supposing the system to become rigid. From these and certain geometrical considerations follow the *sufficient* conditions of equilibrium of a rigid body. This involves the introduction of the conception of the moment of a force about a line, and certain geometrical propositions, which may be regarded as somewhat difficult for a beginner: I am in hopes that these difficulties will not be found insuperable, as it seems to me that there is a distinct gain in clearness and simplicity by this mode of treatment of the subject. The Appendix on indefinitely small quantities has been added



to enable the student, who is unacquainted with Newton's *Lemmas* and the *Differential Calculus*, to follow the methods used in the chapters on the Centre of Mass and Virtual Work.

For the sake of students beginning the subject, easy numerical examples on the preceding propositions have been embodied in the text. The articles, marked with an asterisk, may be reserved for a second reading of the subject. Explanations and illustrations are printed in smaller type than the articles relating to general principles. With the view of making the diagrams more intelligible, the bounding lines of physical surfaces are drawn thicker than lines representing forces, and lines drawn merely to obtain a geometrical solution of the problem are dotted.

I have referred continually to Thomson and Tait's *Natural Philosophy*, and have also consulted Jellett's *Theory of Friction*. Several of the Illustrative Examples are taken from Dr Wolstenholme's Collection.

I am much indebted to Mr E. W. Hobson, M.A., Fellow of Christ's College, for many valuable suggestions, and also to Mr J. B. Holt, B.A., Scholar of Christ's College, for his kind criticisms and assistance.

JOHN GREAVES.

CHRIST'S COLLEGE, CAMBRIDGE,  
*April, 1886.*

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# STATICS.

## CHAPTER I.

### STATICS OF A SINGLE PARTICLE.

1. WHEN a point is changing its position relatively to surrounding points, it is said to be *in motion* relatively to them: if it is not changing its position, it is said to be *at rest*.

If we consider not only the actual change of position, but also the time which the motion occupied, we bring in the idea of 'rate of motion' or 'velocity'.

2. *Def.* If a point moves so that the distances, measured along its path, between its positions at the ends of equal successive intervals of time, are equal to one another, no matter how short the intervals are, the velocity of the point is said to be 'uniform'. If the distances are not equal, the velocity is 'varying'.

For the velocity to be uniform, it is essential that the distances be equal, even when the intervals of time are indefinitely small: for instance, we may imagine a train travelling 30 miles during each of several successive hours, yet we should not describe its motion as uniform, if the distances travelled during the different minutes were not all equal, nor yet, even though the distances travelled during the different minutes were so, provided those travelled during the different seconds were not always the same, and so on indefinitely.

3. If we wish to give any one a clear idea of the magnitude of some physical quantity, we describe it as bearing such and such a ratio to some definite arbitrarily chosen amount of that quantity, known to him. The known definite amount is called the '*unit*' of the physical quantity generally, while the ratio is called the '*numerical measure*', or simply the *measure* of the particular amount under consideration.

If for instance, the area of a certain field be  $12\frac{1}{2}$  acres, and an acre be chosen as the unit area, the ratio of the area of the field to that of the unit is  $12\frac{1}{2}$ , which is therefore the numerical measure of the area of the field.

We shall suppose then, that we have fixed on some particular length as the unit length, and some particular interval of time as the unit of time.

If the velocity of a point be uniform, its numerical measure is the numerical measure of the distance traversed by it during the unit of time. It may happen that the point's velocity, though uniform for a finite interval of time, is not so for the unit of time: in that case, its numerical measure is that of the space the point would traverse during the unit of time, provided it moved throughout with the same velocity as during the finite time. The velocity which we call the unit velocity, or whose numerical measure is *one*, is the velocity of a point which traverses the unit of length in the unit of time.

*Def.* The *mean* or *average* velocity of a point during any interval of time is the velocity with which a point, moving uniformly during that time, would describe the same distance. Its numerical measure is therefore the numerical measure of the distance described, divided by that of the time required.

*Def.* The velocity of a point *at any instant*, is the limit of the mean velocity of the point during an interval of time including the particular instant, when the interval is diminished indefinitely.



Ex. 1. Compare the velocities of two points which move uniformly, one through 5 feet in half a second, and the other through 100 yards in a minute. *Ans.* 2 : 1.

Ex. 2. A railway train travels 160 miles in 6 hours 30 minutes. What is its average velocity in feet per second? *Ans.* 36·1 nearly.

Ex. 3. One point moves uniformly twice round the circumference of a circle, while another moves uniformly along the diameter: compare their velocities. *Ans.*  $2\pi$  : 1.

Ex. 4. A fly-wheel is 14 feet in diameter, and is observed to go round uniformly fifteen times in a minute: find the velocity of a point in the circumference. *Ans.* 11 feet per second nearly.

Ex. 5. Supposing the earth to rotate about its axis in 23 hours 56 minutes, its equatorial diameter being 7925 miles, find the velocity of a point at the equator relative to the earth's centre, in feet per second. *Ans.* 1526 nearly.

4. Now a velocity is entirely known, if its direction and magnitude are known. But as a straight line  $AB$  can be drawn in any direction, it can be drawn so as to indicate fully the *direction* of a point's velocity, provided we shew either by an arrow-head or by the order of the letters  $AB$ , the *sense* of the velocity, i.e. whether its direction be from  $A$  to  $B$  or from  $B$  to  $A$ . As we can make the line of any length, we can make it so that its length bears the same ratio to some arbitrarily chosen length as the velocity considered bears to the unit of velocity. If this be done, and we know the 'scale', i.e. the length chosen to represent the unit velocity, the line  $AB$  represents completely the velocity considered.



5. A point may be moving with several independent velocities at once: for instance, we know that the earth as a whole is describing an orbit about the sun, and that all points on the earth's surface are describing circles about the earth's axis; if then, a point be moving on the earth's surface, it has relatively to the sun, three independent velocities, viz. its velocity on the earth's surface, the velocity of the point of the earth's surface it occupies at the particular instant, relatively

to the centre of the earth, and the velocity of the earth's centre about the sun.

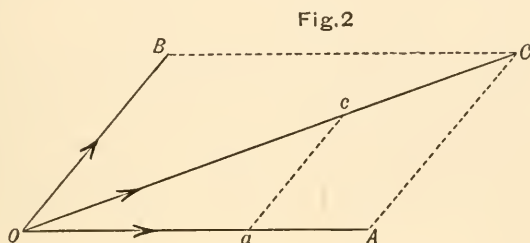
*Def.* When a point has several independent velocities, the single velocity which would alone give the point's motion is called the *resultant* of the other velocities.

Let us consider the case of a point moving in a straight line along the deck of a ship, with uniform velocity relative to the ship, which is sailing with uniform velocity in a straight line along the earth's surface. It is required to find the point's motion relative to the earth's surface, i.e. given its position at one instant, it is required to find its position at the end of a given time. Now since the point's motion on the ship's deck is entirely independent of the ship's motion, if we suppose the point fixed to the deck during the time considered, so that its motion is that of the ship, then the ship to remain stationary while the point moves for an equal time along the deck with its velocity relative to the ship, the final position of the point will be the same as if the two motions had taken place simultaneously, as they really do.

The above illustration exemplifies a general axiomatic principle, which may be stated thus: *if during a certain time a point has several independent motions, its actual position at the end of any portion of that time may be found by imagining that all the motions take place separately during a number of successive periods of time equal to the one considered, instead of supposing that all the motions take place simultaneously, which is what really takes place.* Of course the imaginary motion only gives the same initial and final positions of the point as the real one, and not in general intermediate ones, although by taking the periods of time very small, but very large in number, the imaginary motion which gives us the real position of the point at the end of each of them, will give us an infinite number of points on the point's actual path. The motions referred to above are not of necessity due to uniform velocities.

6. *Prop.* If the two independent velocities of a point be represented in magnitude, direction and sense by two straight lines drawn from or to a point, and a parallelogram be constructed on them as adjacent sides, the resultant velocity is represented in magnitude, direction and sense by the diagonal drawn from or to the point of intersection of these sides.

Let the lines  $OA$ ,  $OB$  represent in magnitude, sense and direction the velocities  $u$ ,  $v$  of the point: complete the parallelogram  $OACB$ , and join  $OC$ ; then  $OC$  shall represent the resultant velocity. If  $O$  be taken as the



initial position of the point, its position at the end of a time  $t$  can be found by supposing that it first moves with a velocity  $OA$  for a time  $t$ , and then with a velocity  $OB$  for the same time. If it moves with a velocity  $OA$  or  $u$  alone, it will at the end of a time  $t$  be at  $a$  in the line  $OA$ , where  $Oa = ut$ ; if now it moves with the velocity  $OB$  or  $v$  alone for a time  $t$ , it will arrive at  $c$ , where  $ac$  is parallel to  $OB$ , and  $ac = vt$ .  $c$  then is the position of the point at the end of a time  $t$ , when the motions take place simultaneously.

But because  $ac : Oa = AC : OA$ ,  $c$  is in  $OC$ , i.e.  $OC$  represents the *direction* of the resultant velocity. Also the magnitude of the resultant velocity is to the velocity  $OA$  as  $Oc$  is to  $Oa$ , i.e. as  $OC : OA$ : hence  $OC$  represents the *magnitude* of the resultant velocity. The *sense* of the resultant velocity is clearly  $OC$ .

The above proposition which is known as the '*Parallelogram of Velocities*' holds at any instant, even though the independent velocities be varying velocities: for it is only necessary to suppose that the time  $t$  is ultimately indefinitely small, and the above proof holds.

Ex. 1. Velocities of 4 feet and 16 feet per second in directions at right angles to each other are simultaneously communicated to a body: determine the resultant velocity. *Ans.* 16.49 feet per second.

Ex. 2. A ship whose head points N.E. is steaming at the rate of 12 knots an hour in a current which flows S.E. at the rate of 5 knots an hour, find the velocity of the ship relative to the sea bottom.

*Ans.* 13 knots an hour.

7. All the objects around us that we can see and touch, and even invisible substances, such as air, are *material* bodies or composed of *matter*. The various properties of matter, such as hardness, density, &c., can be investigated, but no definition of matter can be given which would give any idea of it to a being that had had no experience of it.

Any limited portion of matter is called a 'material body' or simply a 'body'. When we consider a body whose dimensions are so small that we are only concerned with its motion as a whole, and not with any rotational motion it may have, we describe it as a *material particle*, or simply a *particle*.

The term '*mass*' is synonymous with the phrase '*quantity of matter*', so that the mass of a body means the quantity of matter in it. We shall learn afterwards (Art. 9) what is meant by saying that the quantity of matter in one body bears a certain ratio to that in another.

8. *Statics* is the science which treats of the equilibrium of bodies under the action of '*forces*'. A definition of the term '*force*' is supplied by Newton's 1st Law, which asserts that '*Every body remains in a state of*

*rest or of uniform motion in a straight line, except in so far as it may be compelled by impressed forces to change that state'.*

Force, then, is that which alters or tends to alter the state of rest or of uniform motion in a straight line, of a body. It is not necessary to suppose that the state of rest or of uniform motion is *actually* altered by a force, because other forces may be in action which counteract the effect of the first. If we observe a body moving in any way other than uniformly in a straight line, we infer that it is acted on by force: e.g. when we find that the planets move in nearly elliptic orbits, we know that each is under the action of some force: similarly when we see that a falling body moves with gradually increasing velocity, or that another is stopped, we know that a force has acted on each of them. If a force acts for a time on a body, producing a change in the body's velocity, it is clear that if it continues to act, it will tend to produce a still further change.

9. The next question that presents itself is 'How is force measured?' or 'When may *this* force be said to bear such and such a ratio to *that* force?' We know by experience that it requires a greater effort on our part to impart velocity to a large amount of any substance than it does to impart the same velocity to a small amount, but what determines the exact ratio that exists between the two forces?

Our own sensations do not give us an accurate scale by which the forces may be measured. The answer is contained in Newton's 2nd Law, which asserts that '*Change of motion is proportional to the impressed force and takes place in the direction of that force*'.

What does the expression '*Change of Motion*' mean?

First, let us suppose that a number of different forces act on the same particle during equal intervals of time, so that the only variations in the different cases are the



differences in the magnitudes and directions of the forces and in the changes of velocity produced. In this case, '*Change of Motion*' is understood to be a quantity proportional to *change of velocity*. Hence forces are *equal* if, when they act for equal times on the same particle, they produce equal changes of velocity, and the ratio between the magnitudes of two forces is the ratio between the respective changes of velocity they produce in the same particle, after acting for equal times. The *direction* of a force is clearly defined by the latter part of the law as the direction of the change of velocity produced by the force.

It is of course to be understood that the change of velocity meant is not necessarily the increase or decrease of the particle's velocity, but that velocity which, compounded with the particle's initial velocity, will give the final velocity.

Suppose now that a number of equal forces act one on each of a number of particles for the same time, and produce the same changes in their velocities: we express the relation that holds among the particles by saying they are of '*equal mass*'.

If there be  $n$  particles of equal mass, initially all moving side by side with the same velocity, and  $n$  equal forces act, one on each, in the same direction, for the same length of time, the particles will finally be found moving side by side with the same velocity. Hence we infer, that to produce in a particle, whose mass is  $n$  times that of another, the same change of velocity that a given force produces in the latter, and in the same time, a force  $n$  times as great as the given force has to be applied to the former. It seems then, that the force varies as the *mass* of the particle, if the *change of velocity* produced in a given time is always the same, and we have seen that it varies as the *change of velocity* produced in a given time, when the *mass* remains constant. The numerical measure of a force then is proportional to the product of the mass acted upon into the change of velocity produced in a given time.

The expression 'change of motion' means the product of the mass into the change of velocity produced in the given time, or the change of *Momentum* produced in the given time, if the *momentum* of a particle be defined as the product of its mass into its velocity.

10. We are all of us familiar with some instances of the manifestation of force. For instance, we may set a body in motion or stop it by pushing it, either directly with the hand, or by means of a rod, or we may pull it by a string attached to it: we may also expose it to the action of the wind or to the pressure of steam. In all these cases the force is exerted by tangible means, but force is often manifested without any tangible means, as in the case of *gravity*, the name given to the force which causes any body near the earth to move towards it, and the planets to revolve in their orbits about the sun; also in the case of the force which causes small pieces of iron to move towards a magnet held near them. A force of this kind is called an *attraction*.

In both theoretical calculations and in actual practice we must fix on some standard force which is to be the unit. In theoretical calculations we take as our unit the 'dyne', which is the force required to generate in one second a velocity of 1 centimetre per second in a mass equal to that of a cubic centimetre of distilled water at 4° C. This is called the 'absolute unit' and the advantage in its use is, that all the terms involved in its definition are the same at all points of the earth's surface and indeed everywhere.

It is found that if bodies be allowed to fall towards the earth in a vacuum, so that the air does not resist their motion, the velocities with which they fall are increased every second by an amount always the same at the same point of the earth's surface, and nearly so all over it. The force which produces this change of motion in a body is called its 'weight': hence the weights of different bodies are proportional to their masses, since the change of velocity produced is the same for all. Assuming for the present, what we shall prove hereafter (Art. 13), that when a body is at rest under the action of two forces, they are equal in magnitude and opposite in direction, we see that the force required to support a body is equal and opposite to its weight, and would, if it acted

alone, produce in the body the same change of motion upwards that its weight does downwards.

In practice in Statics, forces are generally measured in terms of the weights they would support if they acted upwards: for instance in England that force that is just sufficient to support a certain lump of metal kept at the Mint and called the Imperial Pound, is very often regarded as the unit force, the slight variations in this force at different places being of little consequence for practical purposes.

The velocity of a falling body is increased every second by 32 feet per second, approximately.

Ex. 1. If a body weighing 60 lbs. be moved by a constant force which generates in it in a second a velocity of 5 feet per second, find what weight the force would statically support. *Ans.* 9·3 lbs. nearly.

Ex. 2. During what time must a constant force equal to the weight of one ton act upon a train of 100 tons to generate in it a velocity of 40 miles an hour? *Ans.* 3 min.  $3\frac{1}{3}$  secs.

Ex. 3. A force which can statically support 25 lbs. acts uniformly for one minute on a mass of 400 lbs.: find the velocity acquired by the body. *Ans.* 120 feet per second.

11. *Def.* The *resultant* of a number of forces is that *single* force whose effect is the same as that of the original forces.

It frequently happens that there are several forces acting simultaneously on a body: e.g. a kite in the air is acted on by its weight, by the pressure of the wind and by the tension of the string attached to it. In the case of a particle acted on by several forces, we shall shew that there is a single force which could produce exactly the same effect as the other forces do.

The second Law of motion states that the change of motion is proportional to the impressed force and takes place in the direction of that force, so that if there are several impressed forces we infer that the actual motion will be the resultant of the several independent motions which the forces would produce if they acted separately, because the law holds for each force, and therefore these independent motions must each be produced. But this

resultant change of motion might be produced by a single force, which is therefore the resultant of the original forces.

12. When a particle is in equilibrium or moving uniformly in a straight line under the action of a number of forces there is no change of motion, and therefore the resultant force must be zero; conversely, when the resultant force is zero, there is no change of motion, and the particle must be at rest or be moving uniformly in a straight line. The necessary and sufficient condition of a particle's being in equilibrium under the action of a number of forces is that their resultant be zero.

*Note.* Strictly speaking, if the resultant force on a particle is zero, it only shews that the particle's velocity is undergoing no change, and not that it is necessarily zero. As however in this subject we always suppose the particle initially at rest, if this condition holds, it will always remain so.

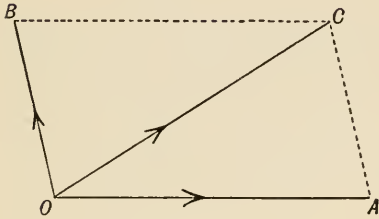
13. We have already inferred from Newton's second Law, that the direction of a force is that of the change of motion it produces, and that its magnitude is proportional to that of the change of motion: so that a force is completely defined when the magnitude and direction of the change in velocity it produces in a given time, when acting on a particle of given mass, are given. A force may therefore be represented completely by the straight line that represents this change in velocity. We are now in a position to prove a most important proposition, known as the '*Parallelogram of Forces*'.

*Prop.* If two straight lines be drawn from or to a point representing in magnitude, direction and sense, forces acting on a particle, and a parallelogram be constructed having these two lines as adjacent sides, the diagonal drawn from or to the point mentioned will represent the resultant completely.

Let  $OA$ ,  $OB$  be two straight lines representing the magnitude, direction and sense of two forces acting on

a particle. Complete the parallelogram  $OACB$ , having  $OA, OB$  for two adjacent sides, and join  $OC$ .

Fig.3



Since  $OA, OB$  represent the forces completely, they also represent the changes in velocity they would separately produce in a certain time in a particle of certain mass. By the parallelogram of velocities then,  $OC$  represents the resultant change of velocity they would produce in the same time in the same particle, and therefore represents the resultant of the original forces.

The following particular case of this proposition is very important: since the diagonal of a parallelogram always has a finite length unless the two adjacent sides are equal in length and in opposite directions, the resultant of two forces is never zero, i.e. the forces do not counter-balance one another, unless they are equal in magnitude and opposite in direction.

*Cor.* If three forces not in one plane acting on a particle, be represented in every respect by three lines  $OA, OB, OC$  drawn from a point, and a paralleliped be constructed on these lines as adjacent edges, the diagonal  $OG$  of the paralleliped represents the resultant in every respect.

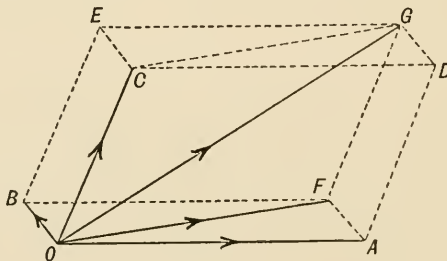


Fig.4

For  $OF$  is clearly the resultant of  $OA$  and  $OB$ , and since  $OFGC$  is a parallelogram ( $OC, FG$  being equal and



parallel),  $OG$  is the resultant of  $OF$  and  $OC$ , i.e. of  $OA$ ,  $OB$ ,  $OC$ .

Ex. 1. Find the resultant of two forces of 12 lbs. and 35 lbs. respectively, which act at right angles on a particle. *Ans.* 37 lbs.

Ex. 2. If two forces acting at right angles to each other be in the proportion of 2 to  $\sqrt{5}$ , and their resultant be 81 lbs. find the forces.

*Ans.* 6 lbs.,  $3\sqrt{5}$  lbs.

Ex. 3. The resultant of two forces which act at right angles on a particle is 51 lbs. : one of the components is 24 lbs. : find the other.

*Ans.* 45 lbs.

Ex. 4. Two forces act on a particle, and their greatest and least possible resultants are 17 lbs. and 3 lbs. : find the forces.

*Ans.* 7 lbs., 10 lbs.

Ex. 5. Two forces acting in opposite directions to one another on a particle have a resultant of 28 lbs. : and if they acted at right angles they would have a resultant of 52 lbs. : find the forces. *Ans.* 48 lbs., 20 lbs.

Ex. 6. Two forces, one of which is three times the other, act on a particle, and are such that if 9 lbs. be added to the larger, and the smaller be doubled, the direction of the resultant is unchanged : find the forces.

*Ans.* 9 lbs., 3 lbs.

Ex. 7. Shew that if the angle at which two given forces are inclined to each other is increased, their resultant is diminished.

Ex. 8. If the resultant of two forces is at right angles to one of the forces, shew that it is less than the other force.

Ex. 9. If the resultant of two forces is at right angles to one force and also equal to the other divided by  $\sqrt{2}$ , compare the forces.

*Ans.* 1 :  $\sqrt{2}$ .

14. *Prop.* If a particle be in equilibrium under the action of a number of forces, any one of them is equal and opposite to the resultant of the rest.

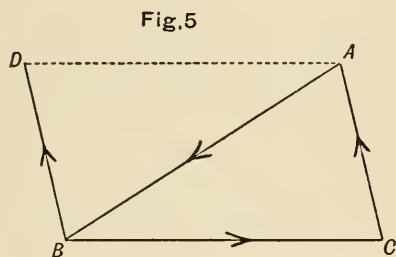
From the definition of a resultant, all the forces but one can be replaced by their resultant without altering their effect, so that this resultant force and the remaining force maintain equilibrium, which we have seen can only be the case when they are equal and opposite.

15. The following proposition known as the 'Triangle of Forces' is practically another way of stating the 'Parallelogram of Forces'.

If three forces acting on a particle can be represented in magnitude, direction and sense by the sides of a triangle, taken in order, the forces are in equilibrium.

By the phrase 'taken in order' is meant, that the arrowheads which indicate the directions of the forces, should all point the same way round the triangle, or that no two should both point to or from the same point.

Let  $ABC$  be a triangle whose sides  $AB$ ,  $BC$ ,  $CA$ , taken in order, represent in magnitude, direction and sense three forces acting on a particle—the particle shall be in equilibrium.



Complete the parallelogram  $BCAD$ . Since  $BD$  is equal and parallel to  $CA$ , it will represent the force represented by  $CA$ : but the resultant of the forces represented by  $BC$ ,  $BD$  is represented by  $BA$ , and is therefore counterbalanced by the force represented by  $AB$ , so that the three forces produce equilibrium.

represented by  $BC$ ,  $BD$  is represented by  $BA$ , and is therefore counterbalanced by the force represented by  $AB$ , so that the three forces produce equilibrium.

16. Conversely, if three forces keep a particle in equilibrium, and a triangle be drawn having its sides parallel to the directions of the forces respectively, the sides are proportional to the forces to whose directions they are respectively parallel.

Let  $BC$ ,  $BD$  (fig. 5) represent two of the forces: then, since they are in equilibrium,  $AB$  must represent the third. But  $CA$  is parallel and equal to  $BD$ , therefore the triangle  $ABC$  has its sides parallel to the three forces, and also proportional to them respectively. Any triangle then, that has its sides parallel to the three forces respectively, must have them parallel to the sides of the triangle

$ABC$ , and must therefore be equiangular to this triangle: equiangular triangles are similar ones, so that the forces are proportional to the sides, to which they are respectively parallel, of any triangle drawn in the way described.

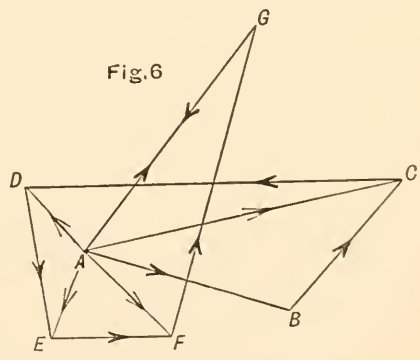
This proposition may be extended thus: if three forces keep a particle in equilibrium, and a triangle be drawn with its sides making a constant angle measured in the same direction, with the directions of the forces respectively, the sides of the triangle are respectively proportional to the forces with whose directions they make the constant angle.

For if the triangle be turned in its own plane through an angle equal to the constant angle, but in the direction opposite to that in which the angle is measured, each of its sides becomes parallel to the direction with which it previously made the constant angle, and the proposition becomes identical with the previous one.

17. The 'triangle of forces' can be easily extended to the 'polygon of forces', which is: If a particle be under the action of a number of forces, which can be represented by the sides of a polygon taken in order, the particle will be in equilibrium.

Let the sides  $AB, BC, CD, DE, EF, FG, GA$  of the polygon  $ABCDEF G$ , taken in order, represent a number of forces acting on a particle. Join  $AC, AD, AE, AF$ .

By the 'triangle of forces', the forces represented by  $AB, BC$  can be counterbalanced by  $CA$ , therefore  $AC$  represents their resultant; similar the resultant of  $AC, CD$  is represented by  $AD$ , that of  $AD, DE$  by  $AE$ , that of  $AE, EF$  by  $AF$ , and that of  $AF, FG$  by  $AG$ ; therefore the resultant of forces represented by  $AB, BC, CD, DE, EF, FG$  is represented by  $AG$ ; but forces represented by  $AG, GA$  counterbalance one another, so that the original forces are in equilibrium.



*Note.* The forces are not necessarily in one plane.

*Cor.* To obtain geometrically the resultant of a number of forces acting on a particle. Draw a series of straight lines, end to end,  $AB, BC, CD, DE, EF, FG$  to represent completely the forces, whose resultant is required, then join  $AG$ , it represents completely the resultant.

The following particular case of the polygon of forces may be noticed: the resultant of a number of forces on a particle, and in the same straight line, is their algebraical sum, the forces being estimated positive in one direction and negative in the other.

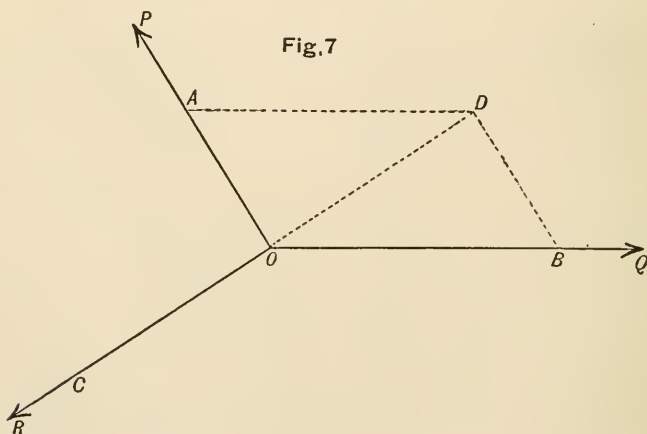
The converse of the polygon of forces does not hold, because equiangular polygons are not necessarily similar.

18. The following theorem, enunciated by Lami, is the parallelogram of forces in another form.

*Prop.* If three forces acting on a particle, keep it in equilibrium, each is proportional to the sine of the angle between the other two.

Let  $OA, OB, OC$  represent three forces  $P, Q, R$  which, acting on a particle, keep it in equilibrium.

With  $OA, OB$  as adjacent sides complete the parallelogram  $OADB$ : join  $OD$ .

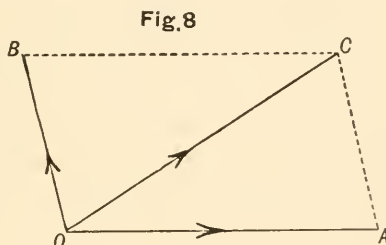


$OD$ ,  $OC$  must be equal and opposite, since  $OD$  represents the resultant of  $P$  and  $Q$ .

$$\begin{aligned} P : Q : R &= OA : OB : OC = OA : AD : OD \\ &= \sin ODA : \sin AOD : \sin OAD \\ &= \sin DOB : \sin AOD : \sin AOB \\ &= \sin BOC : \sin AOC : \sin AOB \\ &= \sin \overline{Q, R} : \sin \overline{P, R} : \sin \overline{P, Q}. \end{aligned}$$

19. The magnitude of the resultant  $R$ , of two forces  $P$  and  $Q$ , which act on a particle, and whose directions make an angle  $\theta$  with one another, may be easily found.

Let  $OA$ ,  $OB$  represent the forces  $P$ ,  $Q$  respectively. Complete the parallelogram  $OBCA$ , and join  $OC$ : the latter represents  $R$ .



$$\begin{aligned} \text{But } OC^2 &= OB^2 + BC^2 - 2OB \cdot BC \cdot \cos OBC, \\ BC &= AO, \text{ and } OBC = 180^\circ - AOB \\ &= 180^\circ - \theta, \\ \therefore R^2 &= P^2 + Q^2 + 2PQ \cos \theta. \end{aligned}$$

Ex. 1. If forces of 3 lbs. and 4 lbs. have a resultant of 5 lbs., at what angle do they act? Ans.  $90^\circ$ .

Ex. 2. If one of two forces acting on a particle is 5 lbs., and the resultant is also 5 lbs., and at right angles to the known force, find the magnitude and direction of the other force.

Ans.  $5\sqrt{2}$  lbs., making an angle of  $135^\circ$  with the other force.



Ex. 3. At what angle must forces  $P$  and  $2P$  act on a particle in order that their resultant may be at right angles to one of them? *Ans.*  $120^\circ$ .

Ex. 4. If three forces, whose magnitudes are expressed by the numbers 3, 6, 9, act on a particle, and keep it at rest, shew that they must all act in the same straight line.

Ex. 5. If the three forces in Ex. 4 act in directions represented by the sides of an equilateral triangle, taken in order: determine their resultant. *Ans.* A force  $3\sqrt{3}$ , acting at right angles to the force 6.

Ex. 6. Three forces acting on a particle keep it in equilibrium: the greatest force is 5 lbs., and the least is 3 lbs., and the angle between two of the forces is a right angle: find the other force. *Ans.* 4 lbs.

Ex. 7. Two equal forces act at a certain angle on a particle, and have a certain resultant: also if the direction of one of the forces be reversed and its magnitude be doubled, the resultant is of the same magnitude as before: shew that the two equal forces are inclined at an angle of  $60^\circ$ .

Ex. 8. Determine the resultant of four forces of 5, 6, 9, 10 lbs. acting on a particle and represented in direction by  $OA$ ,  $OB$ ,  $OC$ ,  $OD$ , respectively, where  $O$  is the point of intersection of the diagonals of a square  $ABCD$ .

*Ans.*  $4\sqrt{2}$  lbs., in the direction bisecting the angle  $COD$ .

Ex. 9. Forces  $P$ ,  $P\sqrt{3}$ , and  $2P$  act on a particle: find the angles between their respective directions that there may be equilibrium.

*Ans.* Between  $P$  and  $P\sqrt{3}$ ,  $90^\circ$ ; between  $P$  and  $2P$ ,  $120^\circ$ ; between  $P\sqrt{3}$  and  $2P$ ,  $150^\circ$ .

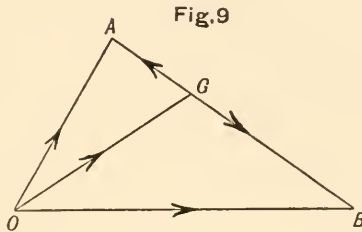
Ex. 10. Five equal forces act on a particle, in directions parallel to five consecutive sides of a regular hexagon taken in order; find the magnitude and direction of their resultant.

*Ans.* The direction is parallel to the third force, and the magnitude equal that of any one force.

20. The following proposition is sometimes useful.

If two forces acting on a particle be represented by  $m$  times the line  $OA$ , and  $n$  times the line  $OB$ , respectively, their resultant is represented by  $(m+n)$  times the line  $OG$ , where  $G$  is the point between  $A$  and  $B$ , such that  $mAG = nBG$ .

By the 'triangle of forces'  $mOA$  is equivalent to  $mGA$  and  $mOG$ , and the force  $nOB$  to  $nGB$  and  $nOG$ . But since  $mAG = nBG$ , and they are opposite, these two forces counterbalance one another, so that we are left with  $(m + n) OG$  only.



21\*. *Def.* Let  $A_1, A_2, A_3 \dots A_n$  be a series of points; join  $A_1A_2$ , and take  $B_1$  between them, so that

$$A_1B_1 = B_1A_2;$$

join  $B_1A_3$ , and take  $B_2$  between them, so that

$$2B_2B_1 = B_2A_3;$$

join  $B_2A_4$  and take  $B_3$  between them, so that

$$3B_3B_2 = B_3A_4,$$

and so on until we arrive at  $B_{n-1}$ : this point is called the 'centroid' of  $A_1, A_2, A_3 \dots A_n$ .

The centroid of the  $n$  points  $A_1, A_2 \dots A_n$  is sometimes defined as the point whose distance from any plane is one  $n^{\text{th}}$  the sum of the distances of  $A_1, A_2 \dots A_n$  from that plane. We can easily shew that the definition of the centroid we have already given leads to this definition also.

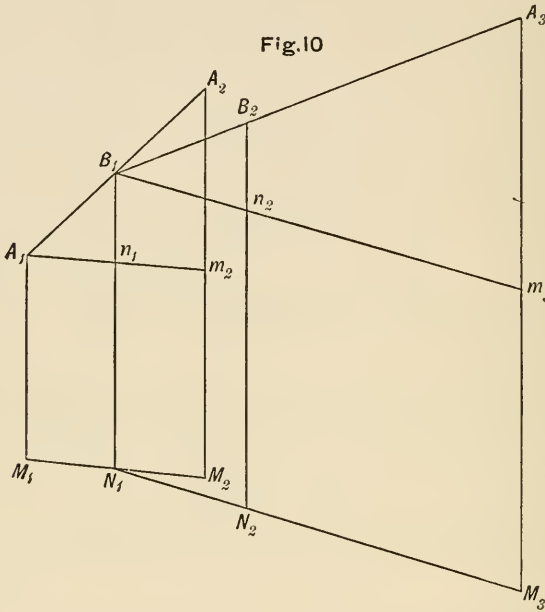
Draw  $A_1M_1, A_2M_2$  &c.  $B_1N_1, B_2N_2$  &c. perpendicular to any given plane. Draw  $A_1n_1m_2$  parallel to  $M_1N_1M_2$ , and  $B_1n_2m_3$  parallel to  $N_1N_2M_3$ .

$$\begin{aligned} A_1M_1 + A_2M_2 &= n_1N_1 + A_2m_2 + m_2N_2 \\ &= 2n_1N_1 + 2B_1n_1 = 2B_1N_1, \end{aligned}$$

$$\begin{aligned} A_1M_1 + A_2M_2 + A_3M_3 &= 2B_1N_1 + m_3M_3 + A_3m_3 \\ &= 3n_2N_2 + 3B_2n_2 = 3B_2N_2. \end{aligned}$$



This proves the statement for two and three points, and by the method of induction the proof can easily be extended to any number of points.



*Note.* The distances from the plane must be considered positive when they are on one side of it, negative when they are on the other. We may suppose that any number of the points become coincident: for instance, if  $A_2$  and  $A_3$  coincide with  $A_1$ ,  $B_1$  and  $B_2$  will also coincide with  $A_1$ , and  $B_3$  will be in the line  $A_1A_4$ , and such that  $B_3A_4 = 3B_3A_1$ . We may extend the idea of the centroid by supposing that some of the points are negative, in which case the process of finding the centroid will be somewhat modified: for instance, if  $A_3$  be a negative point,  $B_2$  will be in  $A_3B_1$ , but beyond  $B_1$  not between  $B_1$  and  $A_3$ , and such that  $B_2A_3 = 2B_2B_1$ : as  $B_2$  is the centroid of two positive and one negative point  $B_3$  will divide the line  $B_2A_4$  equally. Also the distance of a negative point from a plane must be taken of opposite sign to what it would be if the point were a positive one, and in estimating the number of points, we must take the difference between the numbers of positive and negative points.

22\*. *Prop.* If  $OA_1, OA_2, OA_3$  &c.....  $OA_r$  represent a number of forces acting on a particle, their resultant

will be represented by  $r$  times the line  $OB_{r-1}$ , where  $B_{r-1}$  is the 'centroid' of  $A_1, A_2 \dots A_r$ .

For, by the last proposition, putting  $m = n = 1$ , the resultant of  $OA_1$  and  $OA_2$  is  $2OB_1$ ; putting  $m = 1, n = 2$ , that of  $OA_3$  and  $2OB_1$  is  $3OB_2$ , and so on, until we obtain  $rOB_{r-1}$  as the final resultant.

After reading Chap. IV. it will be obvious that the centroid of a number of points is the Centre of Mass of equal particles situate one at each point. As a direct result of this proposition we see, that the resultant attraction or repulsion on a particle of any mass of which each particle attracts or repels with a force varying as its distance and its mass conjointly, is the same as the attraction or repulsion of the whole mass collected at its Centre of Mass.

Ex. 1. Find a point such that, if it be acted on by forces represented by the lines joining it to the vertices of a triangle, it will be in equilibrium.

The required point must be the centroid of the three points, i.e. (Art. 21) the point of intersection of the lines drawn from the vertices to the middle points of the opposite sides.

Ex. 2.  $O$  is any point in the plane of a triangle  $ABC$ , and  $D, E, F$  are the middle points of the sides. Shew that the system of forces  $OA, OB, OC$  is equivalent to the system  $OD, OE, OF$ .

It can be shewn that the centroid of the points  $A, B, C$  is also that of  $D, E, F$ . v. Ex. 1.

Ex. 3. The circumference of a circle is divided into a given number of equal parts, and forces acting on a particle are represented by straight lines drawn from any point to the points of division: shew that their resultant passes through the centre of the circle, and that its magnitude varies as the distance of the point from the centre.

The centre of the circle is clearly the centroid of the points.

Ex. 4.  $AOB$  and  $COD$  are chords of an ellipse parallel to conjugate diameters: forces are represented in magnitude and direction by  $OA, OB, OC, OD$ : shew that their resultant is represented in direction by the straight line which joins  $O$  to the centre of the ellipse, and in magnitude by twice this line.

The centroid of the points  $A, B, C, D$  is midway between  $O$  and the centre.

Ex. 5. Straight lines are drawn from any point parallel to the four sides of a parallelogram: find the magnitude and direction of the resultant of the forces represented by these four straight lines. *Ans.* The direction is along the line joining the point with the centre of the parallelogram, and the magnitude is represented by twice this line.

23. *Def.* The *components* of a force, in two or in three given directions, are the forces which acting in those directions, will have the given force for resultant.

As it is frequently desirable to replace *two or more* forces by *one* (their resultant), so also is it to replace *one* force by *two* (its components), in two given directions in the same plane with it, and sometimes by *three* in three given directions, which are not all in one plane and no two of which are in the same plane as the single force.

For instance, imagine a particle, free to move in a straight groove, to be pulled by a string making an angle with the groove: it is clear that the tendency of the force is twofold, viz. to make the particle move along the groove and to press it against the groove. Also it is clear that the one effect might be produced by a force along the groove and the other by a force at right angles to the groove: these two separate forces will be the components in the corresponding directions of the force exerted by the string.

We have seen that the mechanical problem of compounding two forces into one is the same as the geometrical one of constructing the diagonal of a parallelogram, having given two adjacent sides: so also to resolve one force into its two components in two given directions in its plane, we have to construct the parallelogram, having given one diagonal and lines to which the sides are respectively parallel.

24. To find the components of a given force in *two* given directions in its plane.

Let  $OC$  represent the force. Draw  $OA$ ,  $CB$  parallel to the line giving one direction, and  $OB$ ,  $CA$  parallel to the line giving the other. By the parallelogram of forces, the force  $OC$  is the resultant of  $OA$  and  $OB$ , which, being in the given directions, are the components required.

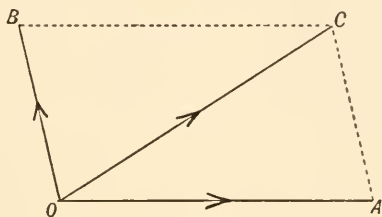
We can easily express the magnitudes of these components in terms of  $OC$  and the angles the given directions make with  $OC$ .

Let  $P$  be the force represented by  $OC$  and let the angles  $COA, COB$  be  $\alpha, \beta$ .

$$\begin{aligned} \text{Then } OA : OC &= \sin OCA : \sin OAC \\ &= \sin COB : \sin AOB \\ &= \sin \beta : \sin (\alpha + \beta); \end{aligned}$$

$$\therefore \text{ the component in direction } OA = P \frac{\sin \beta}{\sin (\alpha + \beta)}.$$

Fig. II



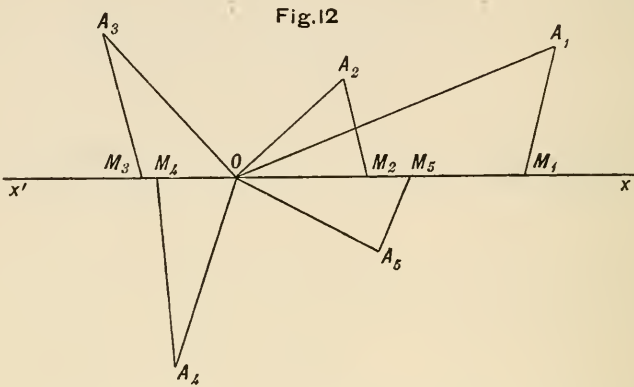
$$\text{Similarly that in direction } OB = P \cdot \frac{\sin \alpha}{\sin (\alpha + \beta)}.$$

Since we can construct any number of parallelograms having a given diagonal, the number of ways in which we can resolve a single force into two is infinite. The most important case is when the two directions along which the resolution takes place are at right angles to one another.

25. *Def.* When the directions of the two components of a force are at right angles to one another, each component is called the 'resolved part' of the force in the corresponding direction. When we speak then of the resolved part of a force in any direction, it is understood that the force is resolved into two components, one in the specified direction, and the other in the direction at right angles to it, and in the plane containing this direction and that of the original force.

Let  $Ox$  be a given straight line, and let  $OA_1, OA_2, OA_3, \dots$  represent a number of forces  $P_1, P_2, P_3, \dots$ , whose directions, which are not necessarily in one plane, make angles  $\theta_1, \theta_2, \theta_3, \&c.$  with  $Ox$ .

Produce  $xO$  backwards to  $x'$ , and draw  $A_1M_1$ ,  $A_2M_2$ ,  $A_3M_3$ , &c. perpendicular to  $xOx'$ . Then  $OM_1$ ,  $OM_2$ ,  $OM_3$ , &c.



represent the resolved parts of  $P_1$ ,  $P_2$ ,  $P_3$ , &c. respectively along  $Ox$ , and  $M_1A_1$ ,  $M_2A_2$ ,  $M_3A_3$  the resolved parts perpendicular to  $Ox$ .

It is found convenient to adopt the convention that forces in direction  $Ox$ , from left to right, be considered positive, while those in the opposite direction are considered negative.

In the above figure it will be seen that with this convention the resolved parts along  $Ox$  of  $P_1$ ,  $P_2$  and  $P_5$  are positive, while those of  $P_3$  and  $P_4$  are negative.

$OM_1 = OA_1 \cos \theta_1$ ,  $A_1M_1 = OA_1 \sin \theta_1$ ,  $OM_2 = OA_2 \cos \theta_2$ , &c. Hence the numerical values of the resolved parts of the forces along  $Ox$  are  $P_1 \cos \theta_1$ ,  $P_2 \cos \theta_2$ , &c. and those perpendicular to it are  $P_1 \sin \theta_1$ ,  $P_2 \sin \theta_2$ , &c.

It is easily seen that these values also give the algebraical values of the resolved parts, the signs being determined in accordance with the above convention.

*Note.* When the forces are in one plane, their resolved parts at right angles to  $Ox$  are in the same straight line, but not otherwise.

If  $X$ ,  $Y$  are the resolved parts of a force  $P$ , in two directions, making angles  $\theta$  and  $\frac{\pi}{2} - \theta$  respectively, with  $P$ , we have seen that

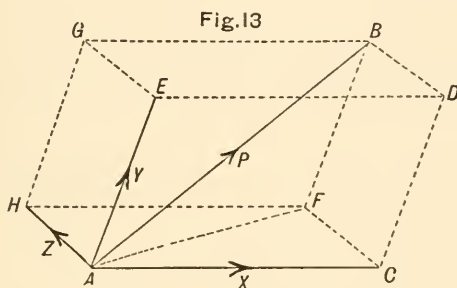
$$X = P \cos \theta, \text{ and } Y = P \sin \theta,$$

$$\therefore P = \sqrt{X^2 + Y^2} \text{ and } \tan \theta = Y/X.$$

26\*. To find the components of a force in *three* given directions, which are not all in the same plane, and no two of which are in the same plane as the original force.

Let the line  $AB$  represent the given force.

Through both  $A$  and  $B$  draw three planes parallel to



each pair of the given directions. These six planes will form the faces of a parallelepiped of which  $AB$  is the diagonal, and each edge of which will be parallel to one of the given directions.

By Art. 13 the edges  $AE$ ,  $AC$ , and  $AH$  will represent forces of which  $AB$  is the resultant, and which are therefore the required components.

The only case which is of much interest is when the given directions are mutually at right angles to one another: the components are then termed the *resolved parts* in the corresponding directions.

Let  $P$  be the given force,  $X$ ,  $Y$ ,  $Z$  the resolved parts in the directions  $AC$ ,  $AE$ ,  $AH$  respectively, which make angles



$\alpha$ ,  $\beta$ ,  $\gamma$  with  $AB$ . But  $AC = AB \cos \alpha$ ,  $AE = AB \cos \beta$ , and  $AH = AB \cos \gamma$ ,

and  $AB^2 = BF^2 + AF^2 = AE^2 + AC^2 + AH^2$ ,

$$\therefore X = P \cos \alpha, Y = P \cos \beta, Z = P \cos \gamma,$$

and  $P^2 = X^2 + Y^2 + Z^2$ .

Hence  $\cos^2 \alpha + \cos^2 \beta + \cos^2 \gamma = 1$ .

Ex. 1. Shew how to resolve a given force into two others, of given magnitude. When is this impossible?

Ex. 2. Find the components of a force  $P$ , when they both make angles of  $30^\circ$  with it. *Ans.* Each is  $P/\sqrt{3}$ .

Ex. 3. Find the components of a force  $P$  in two directions, making angles of  $60^\circ$  and  $45^\circ$  with  $P$  on opposite sides.

$$\text{Ans. } 2P/(1+\sqrt{3}) \text{ and } P\sqrt{6}/(1+\sqrt{3}).$$

Ex. 4. Three forces of 5, 2, and 7 lbs. respectively act on a particle in directions mutually at right angles: determine the magnitude of their resultant. *Ans.*  $\sqrt{78}$  lbs.

Ex. 5. Three forces, represented by three diagonals of three adjacent faces of a cube which meet, act at a point: shew that their resultant is equal to twice the diagonal of the cube.

Each of the forces may be resolved into two components, represented by those edges of the corresponding face, which meet in the point: the three forces are equivalent then to the three forces represented by twice the edges of the cube, which meet in the point, i.e. to twice the diagonal of the cube. A similar result holds for any parallelepiped.

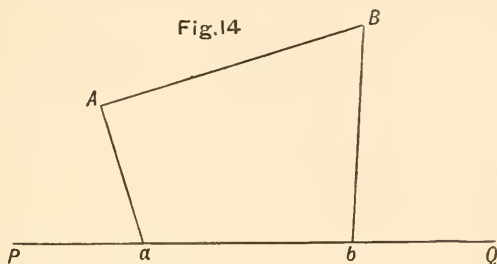
The *purely geometrical* propositions of the next three Articles are extremely useful.

27. *Def.* If perpendiculars be dropped from the ends of a given finite straight line on any other given straight line, the length intercepted between the feet of these perpendiculars is called the *orthogonal projection* of the first line on the second. (The two lines are not necessarily in one plane.)

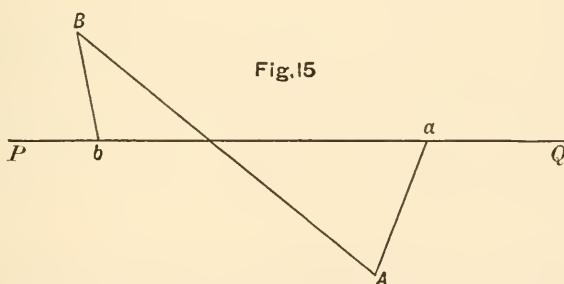
Let  $AB$  be the given finite line,  $PQ$  the line on which it is to be projected.



Draw  $Aa$ ,  $Bb$  perpendicular to  $PQ$ , then  $ab$  is the orthogonal projection of  $AB$  on  $PQ$ .



We shall make a convention here, similar to that we have already made about the resolved parts of forces: viz. if  $AB$  be regarded as drawn from  $A$  to  $B$ , its projection is  $ab$ , measured from  $a$  to  $b$ , whereas if  $BA$  be measured from  $B$  to  $A$ , its projection is  $ba$ , measured from  $b$  to  $a$ . The projections are considered positive when measured from left to right as  $ab$  is, negative when measured in the opposite direction as  $ba$ . These signs apply to figure 14: they are reversed for figure 15.

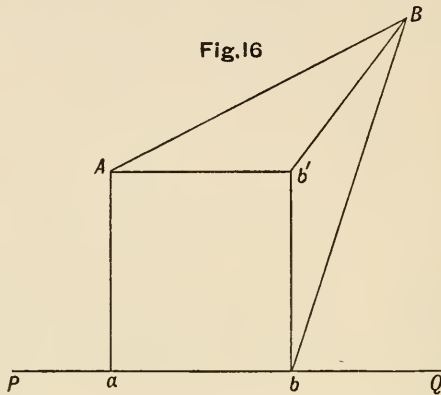


28. *Def.* The angle between two lines not in the same plane is the angle between one of them and a line, intersecting it and parallel to the other.

*Prop.* The orthogonal projection of any line on another is the product of the projected line and the cosine of the angle between them.

Let  $AB$  be any finite line,  $PQ$  the line on which it is projected,  $\alpha$  the angle between them.

Draw  $Aa$  perpendicular to  $PQ$ , and let  $Bb'b$  be a plane through  $B$  perpendicular to  $PQ$ , cutting the latter in  $b$ .



Draw  $Ab'$  parallel to  $ab$ . Then  $Ab'$  is at right angles to the plane  $Bb'b$ , the angle  $Ab'B$  is a right angle, and  $BAb' = \alpha$ . Since  $Aa, b'b$  are both perpendicular to  $ab$ , and are in the same plane, they are parallel, and  $Ab'ba$  is a parallelogram; hence  $ab = Ab' = AB \cos \alpha$ .

Observe that  $\alpha$  is the angle between  $AB$ , and a line drawn from  $A$  parallel to  $PQ$  in the direction in which the projections are estimated positively. If  $\alpha$  is an obtuse angle, the projection is negative. The angle which  $BA$  makes with  $PQ$  is two right angles greater than that which  $AB$  makes with it.

29. *Prop.* The algebraical sum of the projections of the two straight lines  $AB, BC$  on any straight line is equal to the projection of  $AC$  on the same line.

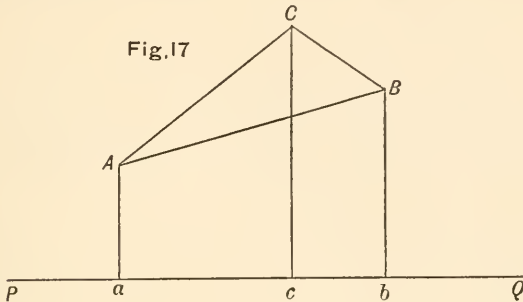
Draw  $Aa, Bb, Cc$  at right angles to the given straight line  $PQ$ , then

$$\begin{aligned} \text{projection of } AB &= ab \text{ (positive),} \\ \dots\dots\dots BC &= bc \text{ (negative),} \\ \dots\dots\dots AC &= ac \text{ (positive),} \end{aligned}$$

and

$$ab - bc = ac,$$

therefore the algebraical sum of the projections of  $AB$ ,  $BC =$  the projection of  $AC$ .



The above signs refer to the figure given; the student can convince himself of the generality of the truth of this proposition by drawing different figures.

*Cor.* The algebraical sum of the projections of the lines  $AB, BC, CD, DE, EF, FG$  (fig. 6), drawn end to end, and measured all the same way round, on any line is equal to the projection of the line  $AG$ .

For the algebraical sum of the projections of  $AB, BC =$  the projection of  $AC$ ,

$$\begin{aligned}
 &\text{that of projections of } AC, CD = \text{projection of } AD, \\
 &\dots\dots\dots AD, DE = \dots\dots\dots AE, \\
 &\dots\dots\dots AE, EF = \dots\dots\dots AF, \\
 &\dots\dots\dots AF, FG = \dots\dots\dots AG,
 \end{aligned}$$

therefore the algebraical sum of the projections of  $AB, BC, CD, DE, EF, FG =$  the projection of  $AG$ .

The same holds for any number of such lines.

30. It follows at once from the figure, or from the expressions for the resolved part of a force in any direction, and the projection of a line on a straight line, that the orthogonal projection of the line representing a force, on any straight line, represents in every respect the resolved part of the force in the corresponding direction.

*Prop.* The algebraical sum of the resolved parts in any direction of a number of forces acting on a particle, is equal to the resolved part of their resultant in that direction.

This proposition follows at once from the last, for if, (fig. 6),  $AB, BC, CD, \dots FG$  represent the forces,  $AG$  represents their resultant; and the algebraical sum of the projections on any straight line, of  $AB, BC, \dots FG$ , which projections represent the resolved parts of the forces in the corresponding direction, is equal to the projection of  $AG$ , which represents the resolved part of the resultant.

31. We can now obtain expressions for the magnitude and direction of the resultant of a number of given forces acting on a particle.

First, let the directions of the forces all lie *in one plane*.

Let  $P_1, P_2, \dots$  be the forces, whose directions make angles  $\alpha_1, \alpha_2, \&c.$ , with the line  $Ox$  in the plane of the forces: let  $Oy$  be a line at right angles to  $Ox$  in the same plane. Let  $R$  be the resultant of the forces and  $\theta$  the angle its direction makes with  $Ox$ .

Then from the proposition just proved

$$P_1 \cos \alpha_1 + P_2 \cos \alpha_2 + \dots = R \cos \theta,$$

and 
$$P_1 \sin \alpha_1 + P_2 \sin \alpha_2 + \dots = R \sin \theta,$$

therefore, 
$$R^2 = [\Sigma(P \cos \alpha)]^2 + [\Sigma(P \sin \alpha)]^2,$$

and 
$$\tan \theta = \frac{\Sigma[P \sin \alpha]}{\Sigma[P \cos \alpha]}.$$

32\*. Secondly, when the directions of the forces are not necessarily in one plane.

Let  $P_1, P_2, P_3, \&c.$  be the forces, whose directions make with three straight lines  $Ox, Oy, Oz$  mutually at right angles, angles  $\alpha_1, \beta_1, \gamma_1, \alpha_2, \beta_2, \gamma_2, \alpha_3, \beta_3, \gamma_3, \&c.$  respectively.

Let  $R$  be the resultant of these forces,  $\bar{\alpha}$ ,  $\bar{\beta}$ ,  $\bar{\gamma}$  the angles its directions make with  $Ox$ ,  $Oy$ ,  $Oz$ , respectively. Then

$$P_1 \cos \alpha_1 + P_2 \cos \alpha_2 + \dots = R \cos \bar{\alpha},$$

$$P_1 \cos \beta_1 + P_2 \cos \beta_2 + \dots = R \cos \bar{\beta},$$

$$P_1 \cos \gamma_1 + P_2 \cos \gamma_2 + \dots = R \cos \bar{\gamma},$$

$$\therefore R^2 = [\Sigma(P \cos \alpha)]^2 + [\Sigma(P \cos \beta)]^2 + [\Sigma(P \cos \gamma)]^2,$$

$$\cos \bar{\alpha} = \frac{\Sigma(P \cos \alpha)}{\sqrt{[\Sigma(P \cos \alpha)]^2 + [\Sigma(P \cos \beta)]^2 + [\Sigma(P \cos \gamma)]^2}},$$

with symmetrical expressions for  $\cos \bar{\beta}$  and  $\cos \bar{\gamma}$ .

33. If the resultant of a number of forces acting on a particle be zero, its resolved part in any direction is zero also; hence if a system of forces be in equilibrium, the algebraical sum of their resolved parts in any direction is zero. Conversely, if the algebraical sum of the resolved parts of a number of forces in any direction be zero, the resolved part of their resultant in that direction must be zero also, i.e. the resultant, if not zero, acts perpendicularly to that direction. Hence a system of coplanar forces acting on a particle is in equilibrium, provided the algebraical sums of their resolved parts in two directions in the plane are zero. If the forces are not in one plane, they are in equilibrium, provided the algebraical sums of their resolved parts in three directions not in the same plane, are severally zero.

We may assert then, that the necessary and sufficient conditions of equilibrium of a system of forces acting on a particle are, that the algebraical sum of their resolved parts in *three* directions not in the same plane, or, in the case of the forces being in one plane, that the algebraical sum of their resolved parts in *two* directions in that plane, be severally zero.

These conditions have been directly deduced from the condition that the resultant should be zero: in practice they are often found to be easier of expression than the geometrical one.

Ex. 1.  $ABCD$  is a square. A force of 3 lbs. acts along  $AB$ , one of 4 lbs. along  $AC$ , and one of 5 lbs. along  $AD$ ; find the magnitude and direction of their resultant.

*Ans.*  $\sqrt{50 + 32\sqrt{2}}$ , making with  $AB$  an angle  $\tan^{-1}(7 - 4\sqrt{2})$ .

Ex. 2. Three forces act on a particle in one plane: they are 1 lb., 5 lbs., and 3 lbs. respectively, and the force of 5 lbs. is inclined at an angle of  $30^\circ$  to each of the others: find their resultant.

*Ans.*  $\sqrt{38 + 20\sqrt{3}}$  lbs., making with the direction of the force of 5 lbs. an angle  $\cot^{-1}(5 + 2\sqrt{3})$  on the side of the force of 3 lbs.

Ex. 3. At the point  $O$  the intersection of the diagonals of a square  $ABCD$ , act forces of 2 lbs. along  $OA$ , 4 lbs. along  $OB$ , 3 lbs. parallel to  $CD$ , and 1 lb. parallel to  $DA$ : find their resultant.

*Ans.*  $\sqrt{30}$  lbs., making with  $CD$  an angle  $\tan^{-1} \frac{3\sqrt{2} + 1}{3 - \sqrt{2}}$ .

Ex. 4. Three forces  $P$ ,  $P$  and  $P\sqrt{2}$  act on a particle in directions mutually at right angles: determine the magnitude of the resultant and the angles between its direction and that of each component.

*Ans.*  $2P$ , making with either force  $P$  an angle of  $60^\circ$ , and with  $P\sqrt{2}$  an angle of  $45^\circ$ .

Ex. 5. A particle is placed at the corner of a cube, and is acted on by forces of 1, 2 and 3 lbs. respectively, along the diagonals of the faces of the cube, which meet at the particle: determine the magnitude of the resultant.

*Ans.* 5 lbs.

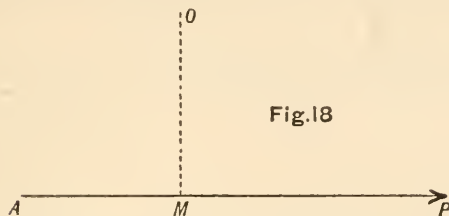
34. *Def.* The *moment* of a force about any *point* is measured by the product of the force into the length of the perpendicular from the point on the line of action of the force.

(The line of action of a force is a line, drawn through the particle on which the force acts, in the direction of the force.)

Let  $P$  be a force acting on a particle situate at  $A$ , and  $O$  be any point: draw  $OM$  perpendicular to  $P$ 's line of action, then  $P \times OM$  measures the moment of  $P$  about  $O$ . The magnitude of the moment of  $P$  is clearly independent of the position of  $A$ , provided the line of action



remain the same. It is convenient to make the convention



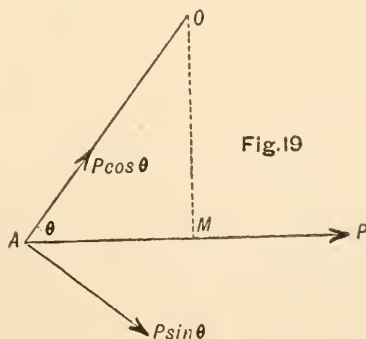
that if the force tends to move the particle round  $O$  in the same direction as the hands of a watch, when looked at from above, the moment is of one sign, when in the opposite direction, of the other sign. The latter is generally taken as the positive moment. In the above figure the moment is positive.

The moment of a force is zero, when the force itself is zero, or when its line of action passes through the point about which the moments are estimated, and in these two cases only.

The student is recommended to accept the above definition of the moment of a force, and to follow the theorems concerning it, without troubling himself at first to learn the physical meaning of the term.

35. *Prop.* The moment of a force about a given point is algebraically equal to the moment of its resolved part at right angles to the line joining the point with the particle, on which the force acts.

Let  $P$  be the force acting on the particle at  $A$ ,  $O$



the given point. Draw  $OM$  perpendicular to  $P$ 's line of action and join  $OA$ . Let  $OAM = \theta$ . The resolved part of  $P$  at right angles to  $OA$  is  $P \sin \theta$ .

$$\begin{aligned} \text{The moment of } P \sin \theta \text{ about } O &= P \sin \theta \cdot OA \\ &= P \times OM \\ &= \text{moment of } P \text{ about } O. \end{aligned}$$

It is also evident that these moments are of the same sign.

36. *Prop.* The algebraical sum of the moments of a number of coplanar forces, acting on a particle, about any point in their plane is equal to the moment of their resultant about the same point.

Let  $A$  be the position of the particle,  $O$  the given point.

$$\begin{aligned} \text{The algebraical sum of the moments of the forces about } O &= \text{the algebraical sum of the moments about } O \text{ of their} \\ &\quad \text{resolved parts perpendicular to } OA \\ &= OA \times \text{the algebraical sum of these resolved parts} \\ &= OA \times \text{resolved part of their resultant in this direction} \\ &= \text{moment of their resultant about } O. \end{aligned}$$

37. By means of the last theorem the conditions of equilibrium of a system of coplanar forces acting on a particle, can be put into a different form.

*Prop.* A system of coplanar forces acting on a particle is in equilibrium, provided the algebraical sum of the moments about each of two points in the plane but not in a straight line with the particle, be zero.

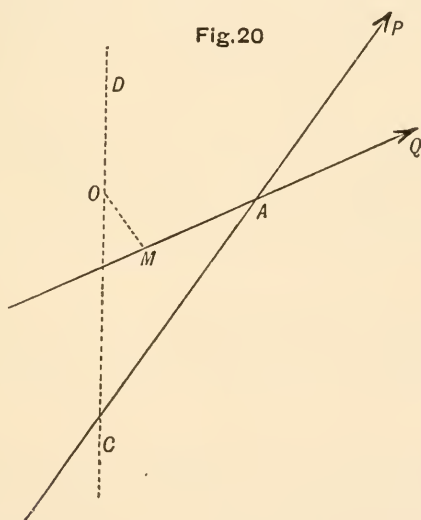
For the algebraical sum of the moments of the forces about any point in their plane is equal to the moment of their resultant about the same point: therefore the moment of their resultant about each of the two points is zero, so that either the resultant is zero, or its line of action passes through both the points; the latter cannot be the case as

the line of action passes through the particle. Hence the forces are in equilibrium.

Conversely, if the forces are in equilibrium, it follows that the algebraical sum of their moments about any point in their plane is zero.

38. *Def.* If a force be resolved into two components respectively parallel and perpendicular to a given straight line, the product of the latter component into the common perpendicular to its line of action and the given line, is called the *moment* of the force *about the given line*. If the force tend to turn the particle it acts on, in one direction about the given line, the moment receives the positive sign; if in the opposite direction, the moment is taken to be negative.

Let  $P$  be the force acting on a particle at  $A$ :  $CD$  the



given straight line. Let  $O$  be the point where  $CD$  intersects a plane through  $A$  perpendicular to  $CD$ : let  $Q$  be the resolved part of  $P$  at right angles to  $CD$ .  $Q$ 's direction is in the plane  $OA$ : draw  $OM$  perpendicular to it.

$$\begin{aligned} \text{Then } P\text{'s moment about } CD &= Q \times OM \\ &= \text{moment of } Q \text{ about } O. \end{aligned}$$

Now  $OM$  is perpendicular to  $CD$  and therefore to a plane parallel to  $CD$  containing  $P$ 's line of action. But since  $CD$  is parallel to this plane, all points in  $CD$  are at the same distance (equal to  $OM$ ) from it; and  $Q$  is the same wherever  $A$  be in the same line of action; therefore the moment of  $P$  about  $CD$  is independent of the position of  $A$  in its line of action.

It is obvious that the moment of a force about a line is zero, if its line of action and the line are coplanar or if the force is zero, and in these cases only.

39. *Prop.* The algebraical sum of the moments of a number of forces acting on a particle, about any straight line is equal to the moment of their resultant about the line.

For, if (fig. 20)  $A$  be the position of the particle,  $CD$  the given line, the algebraical sum of the moments of the forces about  $CD$  is equal to that of the moments of their resolved parts in the plane through  $A$ , perpendicular to  $CD$ , about  $O$  the point of intersection of  $CD$  with this plane, i.e. is equal to the moment about  $O$  of the resultant of these resolved parts, or to the moment about  $O$  of the resolved part in this plane, of the resultant of the original forces, i.e. to the moment of this resultant about  $CD$ .

*Cor.* Hence if the forces are in equilibrium, the algebraical sum of their moments about any line is zero, for if their resultant is zero, its moment about any line is also zero.

40. *Recapitulation.* We began by shewing from purely geometrical considerations how we can compound the independent velocities of a moving point, into a single resultant velocity, by means of the '*parallelogram of velocities.*' From Newton's *First Law* we obtained a general idea of force as that cause, which, acting on a body, tends to alter the state of rest or uniform motion in a straight line, which is the condition of all bodies not acted on by force. Newton's *Second Law* defined the direction of a

force, and stated that its magnitude is proportional to the change of momentum produced by it in any body after acting on the latter for a certain time; from this and the 'Parallelogram of Velocities' we deduced the fundamental Proposition in Statics, the 'Parallelogram of Forces.' Then followed other theorems, the 'Triangle of Forces,' the 'Polygon of Forces,' Lami's theorem, &c., modifications of the Parallelogram of Forces, which often enable us to solve Statical Problems more easily than the original proposition. Having shewn that the algebraical sum of the resolved parts in any direction of a number of forces acting on a particle is equal to the resolved part of their resultant in that direction, we obtained expressions for the magnitude and direction of the resultant of a number of forces. From this and because the sole necessary and sufficient condition of equilibrium of a number of forces acting on a particle is that their resultant be zero, we obtained a set of conditions of equilibrium which is often easily applied to the solution of problems. Another important set of conditions of equilibrium we deduced from the proposition that the algebraical sum of the moments of a number of forces, about any straight line, or in the case of coplanar forces, about a point, is equal to the moment of their resultant about the same line, or point.

41. *Tension of a String.* A very common way of transmitting force is by means of a flexible string, rope or chain. Now when a string  $AB$  is stretched by the application of forces it is a matter of everyday experience that if it be cut at any point  $P$ , the two ends on either side of  $P$  separate: what then prevented the portion  $AP$  from moving before the string was cut? Clearly the force which the other portion  $PB$  exerted on it, and similarly the latter was prevented from moving by the force which  $AP$  exerted on it. But we shall see in Art. 44 that these forces are equal to one another, and act in opposite directions along the lines joining the two adjacent particles on either side of  $P$ , i.e. along the tangent at  $P$  to the curve formed by the string; if the string is straight, these forces will act along it. Either of these forces is called the *tension* at  $P$ . If the tensions at all points of the string are the same, we speak in general of the *tension of the string*.



There is a limit to the tension which any given string can exert, and if we try to transmit a force greater than this by means of the string, it will break.

The above remarks apply to rods also if they are stretched, but the tension becomes a *pressure*, if the tendency of the forces on them is to compress them.

42\*. *Extensible Strings.* The following experimental law, due to Hooke, gives the relation between the extension of an extensible string or rod, the tension along it, and its natural length, i.e. its length when unstretched. *For strings of the same material and thickness, the extension varies as the tension and the natural length conjointly.*

If  $l$  be the natural length,  $l'$  the length when stretched,  $t$  the tension, we may write the law symbolically,

$$l' - l \propto lt,$$

or

$$l' - l = \frac{lt}{\lambda},$$

where  $\lambda$  is a constant for the particular string in question.

We assume that the tension of the string is  $t$  throughout the whole length to which we apply the law. For many substances, such as steel, this law is only true so long as the extension is small compared with the natural length, but in others, such as india-rubber, the limits within which it holds are much wider. It is easily seen that  $\lambda$  is the tension, which, if the law held whatever the extension is, would stretch the string or rod to double its natural length.

$\lambda$  is termed the *Modulus of Elasticity* for strings of the same material and thickness.

43. We shall often have to consider the equilibrium of bodies which are not free to move in any direction, but are constrained by surfaces, curves, &c. with which they are in contact. For instance, suppose a small body inside a fine tube; the only possible motion of the body is along the tube, i.e. the tube itself will supply the force necessary to prevent motion in any other direction: if then the resultant force on the body, not including the force exerted by the tube, be perpendicular to the tube, we know that the body is in equilibrium. Similarly, if a particle be on a plane, and the resultant force, not including the force exerted by the plane, be perpendicular to the plane and towards it: this force, however great, will be counteracted by the force exerted by the plane and the particle will be in equilibrium. If, however, the resultant force is away



from the plane, the particle will move, as the plane cannot exert a force to prevent motion away from itself.

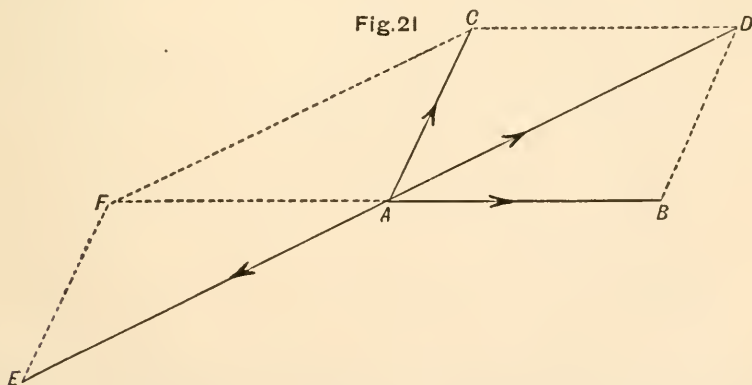
*Smooth* planes or tubes are those which can only exert forces perpendicular to themselves and are the only ones with which we shall have to do at present. A plane or tube which can oppose the motion of a particle along itself, or in other words, can exert a force not entirely perpendicular to itself, is termed *rough*. The same may be said of a curved surface if we take the tangent plane at the point where the particle touches it, as the plane considered above.

Such forces as the pressures exerted by surfaces, &c., and the tensions of inextensible strings, are called into play by the actions of other forces which tend to press the body against the surface, or to stretch the string; the former only act when the latter do. Also, if the surface and the string be supposed strong enough, each is capable of exerting a force of any magnitude, if such a force is necessary to preserve equilibrium. Such forces are termed '*passive*' forces, and it is axiomatic that their magnitudes will always adapt themselves so as to maintain equilibrium, if possible.

ILLUSTRATIVE EXAMPLES.

Ex. 1. Assuming that the Parallelogram of Forces holds as regards direction, to prove it as regards magnitude.

Let  $AB, AC$  represent two forces in magnitude and direction: complete the parallelogram  $ABDC$ , and join  $AD$ . By hypothesis  $AD$  is the direc-



tion of the resultant of the two forces. The force then which will counteract these two forces must act in the direction  $DA$ : produce  $DA$  to  $E$  so

that  $AE$  represents the magnitude of this last force. The three forces  $AB, AC, AE$  are in equilibrium.

Complete the parallelogram  $ACFE$ , and join  $AF$ . By hypothesis,  $AF$  represents the direction of the resultant of  $AC$  and  $AE$ ;  $AF$  then is in a straight line with  $AB$ ; i.e. is parallel to  $CD$ , and  $ADCF$  is a parallelogram.

$$\therefore AD = FC = AE.$$

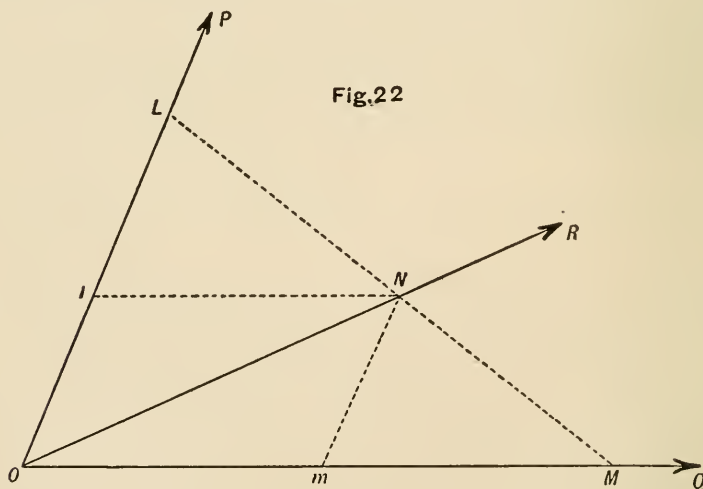
Hence  $AD$  represents the magnitude of the resultant of the forces represented by  $AB$  and  $AC$ , since it is equal to  $AE$  which represents the force that would counteract them.

The converse proposition could be proved in a similar way.

Ex. 2. Forces  $P, Q$  act at a point  $O$ , and their resultant is  $R$ : if any transversal cut their directions in the points  $L, M, N$  respectively, shew that

$$\frac{P}{OL} + \frac{Q}{OM} = \frac{R}{ON}.$$

Through  $N$  draw  $Nl$  parallel to  $OM$ , and  $Nm$  parallel to  $OL$ .



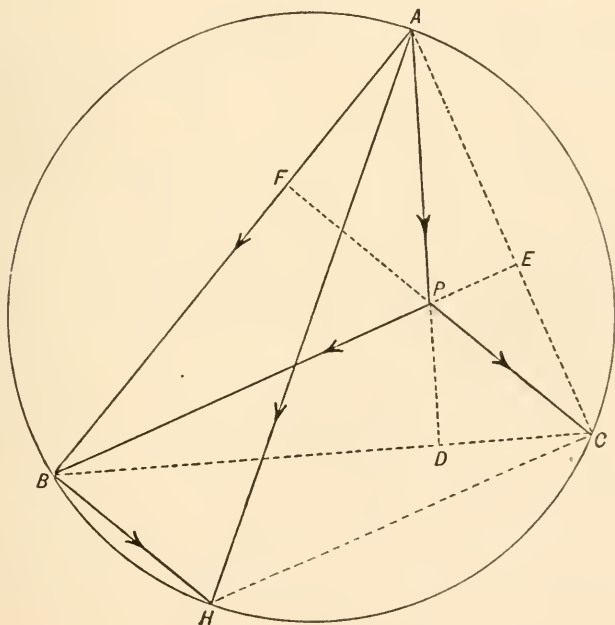
The triangle  $OLN$  has its sides parallel to the directions of the forces  $P, Q, R$  respectively, and if  $R$  be reversed, these forces are in equilibrium; hence (Art. 16) each side is proportional to the force to whose direction it is parallel, i.e.  $Ol = \mu P$ ,  $lN = \mu Q$ ,  $ON = \mu R$ .

$$\begin{aligned} \therefore \frac{P}{OL} + \frac{Q}{OM} &= \frac{1}{\mu} \left( \frac{OL}{OL} + \frac{LN}{OM} \right) \\ &= \frac{1}{\mu} \left( \frac{OL}{OL} + \frac{IL}{OL} \right) \text{ by similar triangles,} \\ &= \frac{1}{\mu} = \frac{R}{ON}. \end{aligned}$$

Ex. 3. Shew that the resultant of three forces acting on a particle and represented by  $AP$ ,  $PB$ ,  $PC$ , where  $P$  is the orthocentre of a triangle  $ABC$ , is represented in magnitude and direction by the diameter of the circle  $ABC$ , which passes through  $A$ .

Draw  $AH$  the diameter of the circle  $ABC$ : join  $BH$ ,  $CH$ : then the angle  $ABH$  is a right angle. By the 'triangle of forces' the resultant of  $AP$ ,

Fig. 23



$PB$  is represented by  $AB$ , since the forces  $AP$ ,  $PB$ ,  $BA$  acting on a particle would maintain equilibrium.

We have then to prove that  $AH$  is the resultant of  $AB$  and  $PC$ .

But by the triangle of forces,  $AH$  is the resultant of  $AB$  and  $BH$ ; hence the problem reduces to the geometrical one of proving that  $PC$  is

equal and parallel to  $BH$ . Since they are both at right angles to  $AB$  they are parallel.

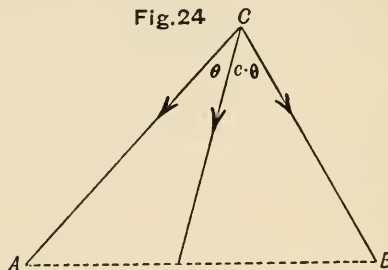
For a similar reason,  $BP$  and  $CH$  are parallel.

$\therefore PBHC$  is a parallelogram.

$\therefore PC = HB$ .

Ex. 4. Two forces act along the sides  $CA, CB$  of a triangle  $ABC$ , their magnitudes being proportional to  $\cos A, \cos B$ . Prove that their resultant is proportional to  $\sin C$ , and that its direction divides the angle  $C$  into two parts,  $\frac{1}{2}(C+B-A), \frac{1}{2}(C+A-B)$ .

Let  $k \cos A, k \cos B$  be the forces,  $R$  their resultant,  $\theta$  the angle its direction makes with  $CA$ .



If  $R$  were reversed, the three forces would be in equilibrium (Art. 14), and then each force would be proportional to the sine of the angle between the other (Art. 18).

$$\therefore R : k \cos A : k \cos B = \sin C : \sin C - \theta : \sin \theta.$$

$$\therefore \frac{\sin(C - \theta)}{\sin \theta} = \frac{\cos A}{\cos B},$$

solving for  $\theta$  we obtain  $\cot \theta = \tan B$ ,

$$\therefore \theta = \frac{\pi}{2} - B = \frac{1}{2}(A + C - B),$$

and  $C - \theta = \frac{1}{2}(C + B - A)$ ,

and  $R = \frac{k \cos B \sin C}{\sin \theta} = k \sin C$ .

Ex. 5. Three forces  $P, Q, R$  in one plane, act on a particle, the angles between  $R$  and  $Q, P$  and  $R, P$  and  $Q$  being  $\alpha, \beta$ , and  $\gamma$  respectively: prove that their resultant

$$= \{P^2 + Q^2 + R^2 + 2QR \cos \alpha + 2RP \cos \beta + 2PQ \cos \gamma\}^{\frac{1}{2}}.$$

Let  $X_1, Y_1$  be the resolved parts of  $P$  in two directions at right angles to one another,  $X_2, Y_2$  and  $X_3, Y_3$  those of  $Q$  and  $R$  respectively in the same directions. Then (Art. 31) the resultant

$$= \sqrt{\{(X_1 + X_2 + X_3)^2 + (Y_1 + Y_2 + Y_3)^2\}}.$$

But  $(X_1 + X_2)^2 + (Y_1 + Y_2)^2 = (\text{resultant of } P, Q)^2$   
 $= P^2 + Q^2 + 2PQ \cos \gamma.$

Similarly  $(X_2 + X_3)^2 + (Y_2 + Y_3)^2 = Q^2 + R^2 + 2RQ \cos \alpha$   
 and  $(X_3 + X_1)^2 + (Y_3 + Y_1)^2 = P^2 + R^2 + 2PQ \cos \beta.$

$\therefore$  adding

$$(X_1 + X_2 + X_3)^2 + (Y_1 + Y_2 + Y_3)^2 + X_1^2 + Y_1^2 + X_2^2 + Y_2^2 + X_3^2 + Y_3^2$$

$$= 2(P^2 + Q^2 + R^2 + PQ \cos \gamma + PR \cos \beta + QR \cos \alpha),$$

$$\therefore (X_1 + X_2 + X_3)^2 + (Y_1 + Y_2 + Y_3)^2$$

$$= P^2 + Q^2 + R^2 + 2PQ \cos \gamma + 2QR \cos \alpha + 2PR \cos \beta,$$

$$\therefore P^2 = X_1^2 + Y_1^2, \quad Q^2 = X_2^2 + Y_2^2, \quad R^2 = X_3^2 + Y_3^2:$$

whence the required result.

The same result can be obtained by resolving in three directions mutually at right angles, when  $P, Q, R$  are not in one plane.

Ex. 6. Forces act through the angular points of a triangle perpendicular to the opposite sides, and are measured by the cosines of the corresponding angles; shew that their resultant is  $\sqrt{(1 - 8 \cos A \cos B \cos C)}$ .

We obtain the resultant by substituting in the last example

$$\cos A \text{ for } P, \cos B \text{ for } Q, \cos C \text{ for } R,$$

$$\pi - A \text{ for } \alpha, \pi - B \text{ for } \beta, \text{ and } \pi - C \text{ for } \gamma.$$

$$\therefore \text{the square of the resultant} = \cos^2 A + \cos^2 B + \cos^2 C$$

$$- 2 \cos A \cos B \cos C - 2 \cos B \cos C \cos A - 2 \cos C \cos B \cos A$$

$$= 1 - \sin^2 A + \cos^2 B + \cos^2 C - 6 \cos A \cos B \cos C$$

$$= 1 + \cos(A - B) \cos(A + B) + \cos^2 C - 6 \cos A \cos B \cos C$$

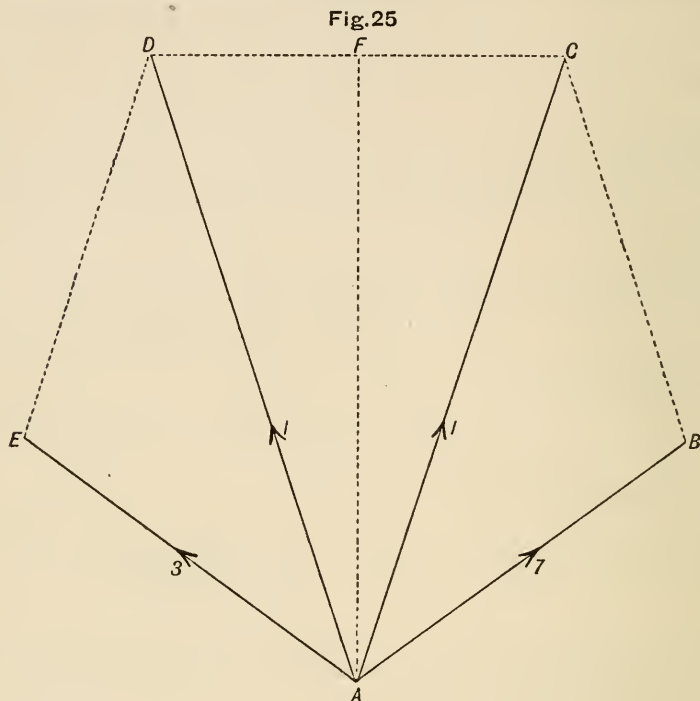
$$= 1 - \cos C \{ \cos(A - B) + \cos(A + B) \} - 6 \cos A \cos B \cos C$$

$$= 1 - 8 \cos A \cos B \cos C.$$

Ex. 7. Prove that the resultant of forces 7, 1, 1, and 3 acting from one angle of a regular pentagon towards the other angles, taken in order, is  $\sqrt{71}$ .

Let  $ABCDE$  be the pentagon,  $AB, AC, AD, AE$  the lines along which

the forces 7, 1, 1, and 3 respectively act. Draw  $AF$  at right angles to  $DC$ . The angles  $BAF$ ,  $EAF$  each  $= 54^\circ$ , the angles  $CAF$ ,  $DAF$  each  $= 18^\circ$ .



Resolve the forces in directions  $AF$ ,  $FC$ .

$$\begin{aligned}
 X, \text{ the algebraical sum of resolved parts in direction } AF \\
 &= (7+3) \cos 54^\circ + (1+1) \cos 18^\circ = 10 \cos 54^\circ + 2 \cos 18^\circ \\
 &= \frac{1}{2} \{ 5\sqrt{(10-2\sqrt{5})} + \sqrt{(10+2\sqrt{5})} \}.
 \end{aligned}$$

$$\begin{aligned}
 Y, \text{ the algebraical sum of resolved parts in direction } FC \\
 &= (7-3) \sin 54^\circ + (1-1) \sin 18^\circ = 4 \sin 54^\circ = \sqrt{5} + 1.
 \end{aligned}$$

Whence the resultant,  $\sqrt{(X^2 + Y^2)} = \sqrt{71}$ .

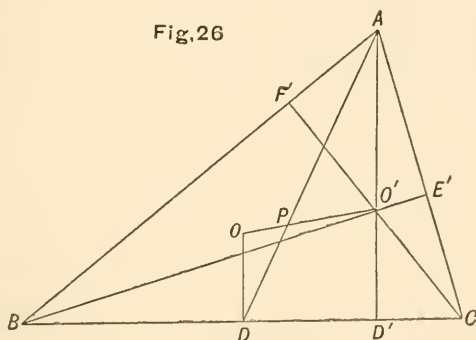
The student has sometimes a difficulty in choosing the lines along which he should resolve the forces, since all directions are open to him for that purpose: it is very important that he should select them judiciously, in order that the work may be simplified. The directions selected in the above example were chosen because they were symmetrically placed as regards the forces.



Ex. 8. Prove that if  $O$  be the centre of the circumscribing circle, and  $O'$  the centre of perpendiculars of a triangle  $ABC$ , the resultant of forces represented by  $OA$ ,  $OB$ ,  $OC$  is represented by  $OO'$ .

By Art. 22, we shall prove the required result, by proving that the centroid of  $A$ ,  $B$ ,  $C$  is in  $OO'$ , at a distance from  $O$ ,  $\frac{1}{3}$  that of  $O'$  from  $O$ .

Draw  $OD$ ,  $AO'D'$  perpendicular to  $BC$ : join  $AD$ , cutting  $OO'$  in  $P$ .



Now  $OD = R \cos A$ , and  $AO' = 2R \cos A$ ,

where  $R$  is the radius of the circle  $ABC$ .

$$\therefore AO' = 2OD \text{ and } O'P = 2OP, \text{ and } AP = 2PD.$$

Hence  $P$  is the centroid of  $ABC$ , and  $OP = \frac{1}{3}OO'$ .

Ex. 9. A given number of forces acting on a particle are represented in magnitude and direction by straight lines drawn from the focus of a conic to the curve: shew that if the sum of the forces be constant, the locus of the extremity of the line representing the resultant is a straight line.

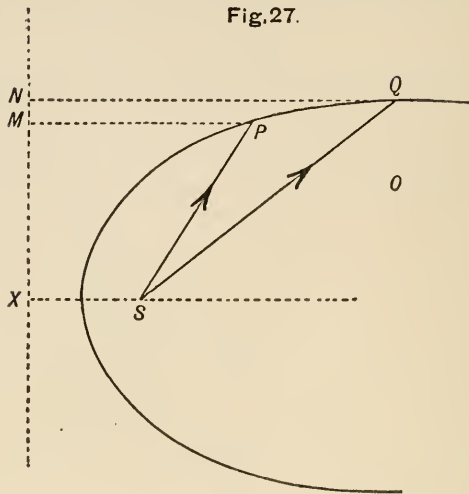
Let  $S$  be the focus; let  $SP, SQ, \dots$  be  $n$  straight lines drawn from  $S$  to the conic so that  $SP + SQ + \dots = \text{a constant}$ .

Draw  $PM, QN, \&c.$  perpendicular to the directrix corresponding to  $S$ ; then since  $SP = ePN$ ,  $SQ = eQN$ ,  $\&c.$ ,

$$PM + QN + \&c. = \text{a constant}.$$

Let  $O$  be the centroid of  $P, Q, \&c.$ , then (Art. 21) the distance of  $O$  from the directrix =  $\frac{PM + QN + \dots}{n} = \text{a constant}$ .

Hence  $O$  lies on a straight line parallel to the directrix, and the end



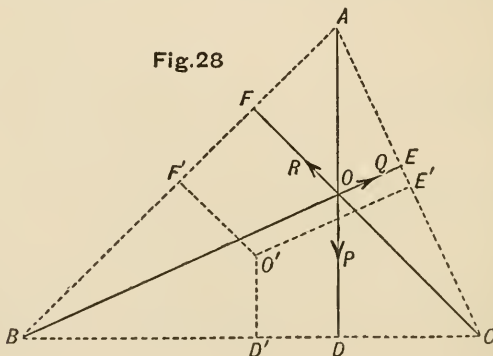
of the line representing the resultant lies on another line parallel to this, but  $n$  times its distance from the focus.

Ex. 10. Forces  $P, Q, R$  act from the angular points of a triangle  $ABC$ , perpendicular to the opposite sides: prove that if their resultant pass through the centre of the circumscribing circle,

$$P(c \cos B - b \cos C) + Q(a \cos C - c \cos A) + R(b \cos A - a \cos B) = 0.$$

Let  $O$  be the orthocentre,  $O'$  the centre of the circumscribing circle.

Let  $D, E, F$  be the feet of the perpendiculars from  $O$  on the sides of the triangle;  $D', E', F'$  the feet of the perpendiculars from  $O'$  on the same.



Since the resultant of  $P, Q, R$  passes through  $O'$ , its moment about  $O'$  is zero.

$\therefore$  the algebraical sum of the moments of  $P, Q, R$  about  $O'$  is zero (Art. 37).

$$\therefore P \cdot DD' + Q \cdot EE' - R \cdot FF' = 0,$$

$$\therefore P \left( c \cos B - \frac{a}{2} \right) + Q \left( a \cos C - \frac{b}{2} \right) - R \left( a \cos B - \frac{c}{2} \right) = 0;$$

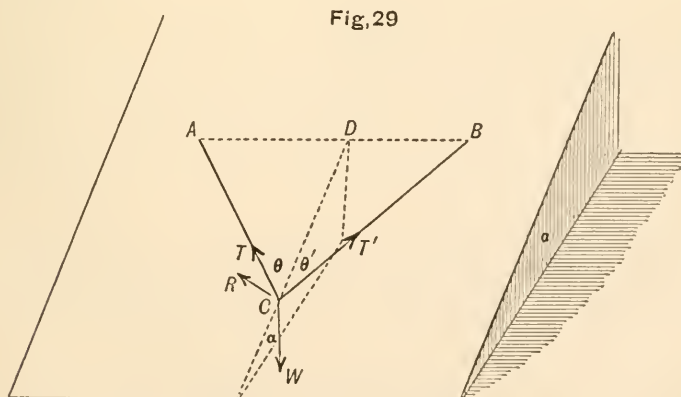
$$\therefore P (c \cos B - b \cos C) + Q (a \cos C - c \cos A) + R (b \cos A - a \cos B) = 0.$$

In the above figure we see that the forces  $P$  and  $Q$  tend to move a particle situate at  $O$  in the opposite way round  $O'$  to that in which  $R$  would move it: their moments therefore are of the opposite sign to that of  $R$ .

The student may verify for himself that the same result would be obtained were the figure different. He should specially notice in the above example that the required result was obtained by expressing that the algebraical sum of the moments about  $O'$  was zero,  $O'$  being on the line of action of the resultant.

Ex. 11. A particle of weight  $W$  is supported on a smooth inclined plane by means of two strings of given lengths, which are attached to the particle  $C$  and to fixed points  $A, B$  in a horizontal line in the plane and at a given distance apart. It is required to find the tensions of the strings.

The sides of the triangle  $ABC$  being known, the angles which  $AC, BC$  make with the horizontal line  $AB$  are known: let  $\theta, \theta'$  be their complements. Let  $\alpha$  be the inclination of the plane to the horizon. Draw  $CD$  perpendicular to  $AB$ .



The particle is in equilibrium under the action of four forces, its weight  $W$  which acts vertically downwards, the tension  $T$  of the string  $AC$ ,  $T'$ , that of  $BC$ , and the pressure of the inclined plane  $R$ , which acts at right angles to the plane.

We shall apply the conditions of equilibrium obtained in Art. 33.

Since the algebraical sum of the resolved parts of the forces in any direction is zero, those in the directions  $AB$  and  $CD$  must be zero.

$$\begin{aligned} \therefore T' \sin \theta' - T \sin \theta &= 0 \dots\dots\dots (i), \\ T \cos \theta + T' \cos \theta' - W \sin \alpha &= 0 \dots\dots\dots (ii). \end{aligned}$$

$R$  occurs in neither equation, because its direction is perpendicular to all lines in the inclined plane, and  $W$  does not occur in the first, because its direction is perpendicular to  $AB$ . The inclination of  $CD$  to the vertical is the same as that of the plane, and is therefore  $\frac{\pi}{2} - \alpha$ , so that the resolved part of  $W$  along  $CD$  is  $-W \sin \alpha$ .

From (i) and (ii) we obtain

$$T = \frac{W \sin \theta'}{\sin (\theta + \theta')}, \quad T' = \frac{W \sin \theta}{\sin (\theta + \theta')}.$$

$R$  can be obtained by equating to zero the sum of the resolved parts in the direction perpendicular to the plane, we have then

$$R - W \cos \alpha = 0,$$

or

$$R = W \cos \alpha.$$

The advantages derived from resolving in the particular directions chosen above, are obvious.

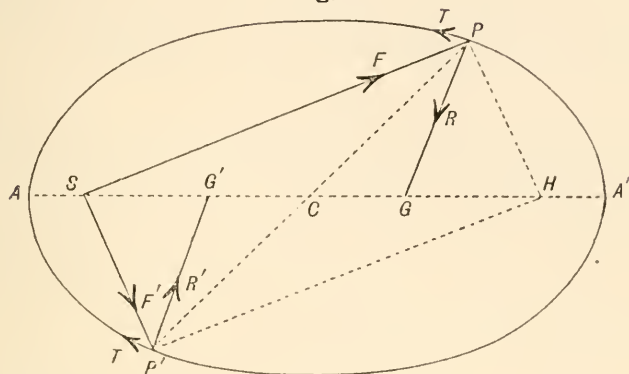
Ex. 12. Two equal particles are connected by a fine string, the particles and string being in a fine smooth elliptic tube, whose semi-circumference is equal to the length of the string. The particles are acted on by constant repulsive forces from one focus: prove that, if these forces are equal, the particles will be in equilibrium in any position in which the string is tight, and if they are unequal, in only one such position.

In this example we shall assume what will be proved hereafter (Art. 81), that the tension of a string, in equilibrium under the action of forces at each end and the pressures of a smooth surface, is everywhere the same: the force at each end must of course be equal to the tension.

Let  $S$  be the focus from which the repulsive forces act;  $P, P'$  the positions of the particles when the string is tight;  $PP'$  is therefore a dia-

meter of the ellipse. Join  $P, P'$  with the foci  $S, H$ .  $SPHP'$  is obviously a parallelogram.

Fig.30.



Let  $F, F'$  be the repulsive force on  $P, P'$  respectively: let the string lie along the semi-circumference  $PAP'$ , and let it be fixed at  $A$ . Each particle is now in equilibrium: let  $T$  be the tension of  $AP$ , and  $T'$  that of  $A'P'$ .

The forces acting on the particle  $P$  are  $F$  along  $SP$ ,  $T$  along the tangent at  $P$ , and the action of the tube along the normal at  $P$ , since the tube is smooth (Art. 43).

Since  $P$  is in equilibrium, resolving along the tangent at  $P$ , we have (Art. 33)

$$F \sin SPG - T = 0.$$

Similarly  $F' \sin SP'G' - T' = 0,$

or  $F' \sin SPG - T' = 0,$

$\therefore$  if  $F = F', T = T',$  i. e. it is not necessary to suppose the string fixed at  $A$  to insure equilibrium, as (Art. 43) the tension of the string will adapt itself to preserve equilibrium, if possible.

If, however,  $F$  and  $F'$  are unequal,  $T$  and  $T'$  will be unequal also, unless  $\sin SPG$  vanishes, i. e. unless the particles are situate at  $A$  and  $A'$ .

But the tension of  $PA$  cannot be different from that of  $P'A$ , unless the string is fixed at  $A$ , so that there is not equilibrium generally, when  $F$  and  $F'$  are unequal, and the string is free to move along the tube.

## EXAMPLES ON CHAPTER I.

1.  $ABC$  is a triangle:  $D, E, F$  are the middle points of the sides  $BC, CA, AB$  respectively: shew that forces acting on a particle and represented by the straight lines  $AD, BE, CF$  will maintain equilibrium.

2.  $A, B, C$  are three points on the circumference of a circle: forces act along  $AB$  and  $BC$  inversely proportional to these straight lines in magnitude; shew that their resultant acts along the tangent at  $B$ .

3. Two forces  $P$  and  $Q$  have a resultant  $R$  which makes an angle  $\alpha$  with  $P$ : if  $P$  be increased by  $R$  while  $Q$  remains unchanged, shew that the new resultant makes an angle  $\frac{\alpha}{2}$  with  $P$ .

4. The resultant of two forces  $P, Q$ , acting at an angle  $\theta$  is equal to  $(2m+1)\sqrt{(P^2+Q^2)}$ : when they act at an angle  $\frac{\pi}{2}-\theta$ , it is equal to  $(2m-1)\sqrt{(P^2+Q^2)}$ : shew that  $\tan \theta = \frac{m-1}{m+1}$ .

5. Compare in terms of the sides of a triangle  $ABC$  the forces which acting from  $O$ , the centre of the inscribed circle, along  $OA, OB, OC$  will balance.

6. Two forces  $P$  and  $P\sqrt{2}$  act on a particle lying on a smooth horizontal plane. If  $P$  makes an angle of  $45^\circ$  with the horizon, find the direction of  $P\sqrt{2}$  in order that the particle may be in equilibrium.

7. Find a point within a quadrilateral, such, that if it be acted on by forces represented by the lines joining it to the angular points of the quadrilateral, it will be in equilibrium.

8.  $ABC$  is a triangle,  $P$  any point in  $BC$ . If  $PQ$  represent the resultant of the forces represented by  $AP, PB, PC$ , the locus of  $Q$  is a straight line parallel to  $BC$ .

9. A heavy particle is attached to one end of a string, the other end of which is fixed. Find the force making an angle of  $30^\circ$  with the horizontal which must be applied to the particle in order that the string may deviate by an angle of  $45^\circ$  from the vertical, and find also the tension of the string.



10. Two forces  $P, Q$  act at a point  $O$  along two straight lines making an angle  $\alpha$  with each other, and have a resultant  $R$ : two other forces  $P', Q'$  acting along the same two lines have a resultant  $R'$ ; shew that the directions of  $R$  and  $R'$  will also include an angle  $\alpha$  if

$$PP' + QQ' + 2PQ' \cos \alpha = 0, \text{ or } PP' + QQ' + 2P'Q \cos \alpha = 0.$$

11. If from  $O$ , the centre of the circle inscribed in the triangle  $ABC$ , forces  $\lambda \cos \frac{A}{2}, \lambda \cos \frac{B}{2}$  act along  $OB, OA$ , prove that the magnitude of the necessary force towards  $C$ , in order that the resultant may pass through the middle point of  $AB$ , is  $\lambda \cot \frac{C}{2}$ .

12. A small ring slides on a smooth arc of a circle and rests in equilibrium under the repulsion of three forces  $P, Q, R$ , directed from points dividing the circumference in three equal parts: if its position of equilibrium lie on the smaller arc between the points from which the forces  $Q, R$  are directed, shew that the pressure exerted by the circle is

$$\{P^2 + Q^2 + R^2 - QR + RP + PQ\}^{\frac{1}{2}}.$$

13. Two particles of weights  $P$  and  $Q$  respectively, are connected by a string which lies on a smooth circle fixed in a vertical plane: shew that if  $\frac{\pi}{2}$  be the angle subtended at the centre by the string, the inclination of the chord joining  $P, Q$  to the horizontal in the position of equilibrium is

$$\tan^{-1} \frac{P \sim Q}{P + Q}.$$

14.  $OA, OB, OC \dots$  are any number of fixed straight lines drawn from a point  $O$ , and spheres are described on  $OA, OB, OC \dots$  as diameters. Any straight line  $OX$  is drawn through  $O$  and a point  $P$  taken on it so that  $OP$  is equal to the algebraical sum of the lengths intercepted on  $OX$  by the spheres. Find the locus of  $P$ .

15. Two constant equal forces act at the centre of an ellipse parallel to the directions  $SP$  and  $PH$ , where  $S$  and  $H$  are the foci and  $P$  is any point on the curve. Shew that the extremity of the line which represents their resultant lies on a circle.

16. Forces are represented by the perpendiculars from the angles of a triangle  $ABC$  on the opposite sides: shew that if their resultant passes through the centre of the nine-point circle

$$a^2(b^4 - c^4) + b^2(c^4 - a^4) + c^2(a^4 - b^4) = 0.$$

17. Three equal forces act at the orthocentre of a triangle  $ABC$ , each perpendicular to the opposite side: prove that if the magnitude of each force be represented by the radius of the circle  $ABC$ , the magnitude of the resultant will be represented by the distance between the centres of the inscribed and circumscribed circles.

18. The resultant  $R$  of any number of forces  $P_1, P_2, P_3$ , &c. is determined in magnitude by the equation

$$R^2 = \Sigma (P^2) + 2\Sigma P_r P_s \cos (P_r \cdot P_s),$$

where  $(P_r P_s)$  denotes the angles between the directions of  $P_r, P_s$ .

19.  $ABCDEF$  is a regular hexagon, and at  $A$  forces act represented in magnitude and direction by  $AB, 2AC, 3AD, 4AE, 5AF$ ; shew that the length of the line representing their resultant is  $\sqrt{351} \cdot AB$ .

20. Two small smooth rings of weights  $W$  and  $W'$ , connected by a string, slide upon two fixed wires, the former of which is vertical, and the other inclined at an angle  $\alpha$  to the horizon. A weight  $P$  is tied to the string, prove that in the position of equilibrium

$$\cot \theta : \cot \phi : \cot \alpha = W : P + W : P + W' + W,$$

where  $\theta, \phi$  are the angles which the two portions of the string make with the vertical.

21.  $ABCD, A'B'C'D'$  are two parallelograms; prove that forces acting at a point proportional to and in the same direction as  $AA', B'B, CC', D'D$ , will be in equilibrium.

22. A particle is acted upon by a number of centres of force, some of which attract and some repel, the force being in all cases proportional to the distance, and the intensities for different centres being different: shew that the resultant force passes through a fixed point for all positions of the particle, and examine the one apparent exception.

23. From any point within a regular polygon perpendiculars are drawn on all the sides: shew that the direction of the resultant of all the forces represented by these perpendiculars passes through the centre of the polygon, and find its magnitude.

24. Two heavy rings slide on a wire in the shape of an ellipse whose major axis is vertical, and are connected by a string which passes over a smooth peg at the upper focus: shew that if the weights are equal and the length of the string is equal to that of the axis major, there are an infinite number of positions of equilibrium.

25. Four particles  $A, B, C, D$  are attached to the ends of strings whose other ends are tied in a knot at  $O$ . Any two particles repel one another with a force which varies directly as the distance and the product of their masses. Shew that when the system is in equilibrium, the volumes of the tetrahedra  $OB CD, OC DA, OD AB, OA BC$  are proportional to the masses of  $A, B, C, D$  respectively.

26. In an ellipse a polygon  $PQRS$ , &c. is described so that the triangles formed with a side as base and the centre of the ellipse as vertex are of equal area. If  $O$  be any point in the plane of the ellipse, prove that the line of action of the resultant of the forces represented by  $OP, OQ, OR$ , &c. passes through the centre of the ellipse.

27. Two small heavy rings slide on a smooth wire, in the shape of a parabola, whose axis is horizontal: they are connected by a light string which passes over a smooth peg at the focus: shew that in the position of equilibrium, their depths below the axis are proportional to their weights.

28. Forces  $P, Q, R$  act in the lines  $DA, DB, DC$  and their resultant meets the plane  $ABC$  in  $G$ , shew that

$$\frac{P}{AD} : \frac{Q}{BD} : \frac{R}{CD} :: \Delta BGC : \Delta CGA : \Delta AGB.$$

If their resultant be parallel to the plane  $ABC$ , then

$$P \cdot DB \cdot DC + Q \cdot DC \cdot DA + R \cdot DA \cdot DB = 0.$$

29.  $O$  is any point on the circle circumscribing a triangle  $ABC$ , and  $OL, OM, ON$  are the perpendiculars from  $O$  on the sides. The line  $LMN$  meets the perpendiculars from  $A, B, C$  on the opposite sides in  $P, Q, R$  respectively. Prove that if forces act at  $O$  represented by  $OL, OM, ON, OP, OQ, OR$  their resultant is represented by  $3OK$ , where  $K$  is the orthocentre.

30.  $ABC$  is a triangle and  $O_1O_2O_3$  are the centres of the three escribed circles opposite to  $A, B, C$  respectively. At any point  $P$ , forces act along  $PO_1, PO_2, PO_3$  represented in magnitude by  $PO_1 \cdot BC, PO_2 \cdot CA, PO_3 \cdot AB$ , respectively. Shew that if their resultant is of constant magnitude, the locus of  $P$  is a circle concentric with the circle circumscribing the triangle  $O_1O_2O_3$ .

## CHAPTER II.

### STATICS OF SYSTEMS OF PARTICLES.

44. WHEN a body composed of a number of particles is in equilibrium, each of these particles is in equilibrium also, and the forces which act on it must therefore satisfy the conditions of equilibrium. But among the forces acting on a particle must be included, not only what are called '*external*' forces, such as the force of gravity, the pressure and tensions due to other bodies, but also '*internal*' forces, i.e. the forces of attraction and repulsion that exist among the different particles composing the body. These forces are by no means always the same in the same body: for example, it is plain that if we try to stretch a rod, the forces that the different particles composing the rod, exert one on another, are different from what they are when we try to compress it. In the former case, the external forces tend to separate particles arranged along a line parallel to the rod's length, in the latter they tend to move them nearer together. To resist these quite opposite tendencies, different internal forces must be called into play. Concerning these internal forces we have Newton's Third Law which asserts that '*action and reaction are always equal and opposite*': i.e., if the particle *A* exerts on the particle *B* a force *R*, (the *action*) in a certain direction, it is itself acted on by a force *R*, (the *reaction*) in the exactly opposite direction, and also in the same straight line, so that the line of

action of each of these forces must be the line joining  $A$  and  $B$ .

45. Without any further assumption about the internal forces that are exerted when any body is in equilibrium, we can determine conditions which must be satisfied by the external forces in such a case.

Since the algebraical sum of the resolved parts in any direction of the forces, which act on each particle of a body in equilibrium, is zero, that of the resolved parts in any direction of all the forces, external and internal, acting on all the particles, is zero also. But as the resolved part of any action is numerically equal, but of opposite sign, to that of the corresponding reaction, the algebraical sum of the resolved parts in any direction of all the internal forces vanishes separately, for the internal forces consist entirely of pairs of forces, equal and opposite to one another. Hence the algebraical sum of the resolved parts of the remaining forces, the external ones, is zero.

*Cor.* A system of forces keeping a number of particles in equilibrium will, if applied to a single particle, keep it in equilibrium, since the conditions of Art. 33 are satisfied.

46. In a similar way we can shew that the algebraical sum of the *moments about any line*, of the external forces acting on a body in equilibrium, is zero. We have only to substitute '*moments about any line*' for '*resolved parts in any direction*' and the above proof holds.

We may state then, that if any body be in equilibrium under the action of external and internal forces, the algebraical sums both of the resolved parts in any direction, and of the moments about any line, of the external forces, are zero.

If the lines of action of the external forces be *in one plane*, the algebraical sum of their moments *about any*



*point* in that plane is zero, being equal to the algebraical sum of their moments about a line through the point in question, and perpendicular to the plane.

47. It is to be noticed that what we have called internal forces are only so relatively—the force which is exerted on the particle *A* by the particle *B* is an *internal* one, when we are considering a body or system of bodies containing both particles, whereas if *B* is not contained in the system, the force is an *external* one. It is then very necessary, in applying the above conditions of equilibrium to a system of particles, to know which forces are external and which internal. The force which is an internal one when we are considering the whole body may become an external one, when only a portion of the body is under consideration.

Ex. 1. A picture weighing 10 lbs. is supported by a string which passes over a smooth peg, and has its two ends fastened to the picture: if the tension of the string be 10 lbs., shew that each string makes an angle of  $60^\circ$  with the vertical.

Apply Art. 45, choosing the vertical and horizontal as the directions along which to resolve.

Ex. 2. A rod is supported by means of two strings which are attached to a fixed point, and one to each end of the rod. Assuming that the weight of the rod acts at its middle point, prove that the tensions of the strings are proportional to their lengths.

Apply Art. 46, taking moments about the middle point of the rod.

Ex. 3. A rod of weight  $W$ , is supported at an angle of  $60^\circ$  with the horizon by means of strings attached to its ends, the one attached to the upper end making an angle of  $60^\circ$  with the horizon, but in an opposite direction to the rod: find the tensions of the two strings and the inclination of the second to the horizon, assuming that the weight of the rod acts at its middle point.

Ans.  $\frac{W\sqrt{3}}{6}$ ,  $\frac{\sqrt{21}}{6}W$ , the latter acting at an angle  $\tan^{-1} 3\sqrt{3}$ , to the horizon.

Apply Arts. 45, 46, choosing an end of the rod as the point about which to take moments, and the horizontal and vertical as the directions in which to resolve.



Ex. 4. A square  $ABCD$ , is in equilibrium under the action of four forces, one of 3 lbs. acting along  $AB$ , one of 2 lbs. along  $BC$ , and one of 3 lbs. along  $CD$ ; find the magnitude and line of action of the remaining force.

*Ans.* A force of 2 lbs., acting in direction  $CB$ , at a distance equal to  $3/2 \cdot AB$  from  $BC$ .

Apply Arts. 45, 46, resolving along  $AB$ ,  $BC$  respectively, and taking moments about  $B$ .

Ex. 5.  $AB$  is a straight weightless rod, 15 feet long; 4 lbs. is hung at  $A$ , 1 lb. at a point 3 feet from  $A$ , and a force of 11 lbs. acts vertically upwards at a point 8 feet from  $B$ ; find what weight must be attached to the rod to maintain equilibrium and where.

*Ans.* 6 lbs., 2 ft. 8 inches from  $B$ .

Ex. 6. Three forces acting at the corners of a triangle, each perpendicular to the opposite side, keep the triangle in equilibrium: prove that each force is proportional to the side to which it is perpendicular.

Take moments about two of the angular points.

Ex. 7. If three forces  $P$ ,  $Q$ ,  $R$ , acting along the bisectors of the angles of a triangle, at the angular points  $A$ ,  $B$ ,  $C$ , respectively, keep the triangle in equilibrium: prove that

$$P : Q : R = \cos \frac{A}{2} : \cos \frac{B}{2} : \cos \frac{C}{2}.$$

Take moments about two of the angular points.

48. We have then found *necessary* conditions of equilibrium for any body or system of bodies whatsoever, including liquids, flexible strings, &c.

We shall hereafter find *sufficient* conditions of equilibrium for '*rigid*' bodies.

*Def.* When the particles which compose a body, always form the same configuration, or in other words, when the body always retains the same shape and size, whatever forces be applied to it, the body is said to be *rigid*.

We have no experience of bodies, which answer this description perfectly, but we know of many substances

which answer it more or less approximately : i.e. we know of many substances, which will submit to the action of considerable forces without undergoing any appreciable change in shape or size. The results which we shall prove *absolutely* true for perfectly rigid bodies, will be so *approximately* for bodies that are approximately rigid.

49. We have already seen that any system of forces acting on a particle is equivalent to a single force, i.e. there is a single force, such that its effect on the particle could not be distinguished from that of the combined forces. The question now presents itself, whether this is so or not when the forces do not all act on a single particle, but on different particles of a system. If the particles form a rigid body, we shall see that under certain circumstances there exists a force, which together with the given forces would keep the body in equilibrium, so that the effect of this force reversed on the body as a whole, is the same as that of the original forces. But it must be remembered that it is only on the body *as a whole* that the effects are the same necessarily : the internal forces called into play by the single force, are not necessarily the same as those called into play by the system of forces, in fact are generally very different. When we cannot find a single force whose effect on the body as a whole is the same as that of the system of forces, we can always find a different system of forces whose effect will be the same, though they will not generally give rise to the same internal forces. It is usual to speak of the single force, when such a one exists, as the *resultant* of the original forces, and the second set of forces as *equivalent* to the first, though it must always be understood that they are so, strictly speaking, *only in one sense*. Even when the body is not rigid, a single force, or set of forces, which would, if the body were rigid, be equivalent in the above sense is said to be, one the resultant of, the other equivalent to, the original system of forces.

50. *Prop.* Any rigid body, under the action of any system of forces, can be *fixed* by applying single forces at

each of any *three* given points of the body not in the same straight line, the direction of the force at one point being at right angles to the plane containing the three points, and that of the force at a second point at right angles to the line joining it to the third.

Let  $A$ ,  $B$ , and  $C$  be any three points of the body. The body can be fixed by the following constraints: imagine a very small spherical socket to be made in the body at  $A$ , and a ball just smaller than the socket to be placed in it, and the ball to be fixed. Now imagine a very small hoop with its plane perpendicular to  $AB$ , to be fixed round  $B$ , and also some obstacle to be placed to prevent  $C$  from moving at right angles to the plane  $ABC$ . The first constraint prevents the body from moving in any way except by turning about  $A$ , and exerts a single force through  $A$  as the ball and socket touch in only one point: the second prevents  $B$  from turning about  $A$ , and therefore from moving at all, so that the body can now only turn about  $AB$ ; the second force acts at right angles to  $AB$ . The third constraint prevents  $C$  from moving round  $AB$ , and therefore from moving at all, and exerts a single force through  $C$  at right angles to the plane  $ABC$ . As  $C$  cannot turn about  $AB$ , it is clear that the body is now fixed.

51. This proposition can be extended to the case in which any or all of the points  $A$ ,  $B$ , and  $C$  are not situate in the body. For we may imagine them made so in effect, without introducing any forces external to the whole system, by arranging a system of rigid rods, without weight, rigidly connecting them with the body.

*Cor.* If the lines of action of the external forces all lie in one plane, the body can be fixed by the application of single forces at any *two* given points  $A$ ,  $B$  in that plane, each force being in the plane, and the direction of one being at right angles to the line  $AB$ .

For by the last proposition, if a third point  $C$  be taken in the plane but not in  $AB$ , the body can be fixed by the application of suitable forces  $P$ ,  $Q$ ,  $R$  at  $A$ ,  $B$ ,  $C$  respec-

tively, the direction of  $R$  being perpendicular to the plane, and that of  $Q$  perpendicular to  $AB$ . The body is now in equilibrium under the action of the internal forces, the original external forces, and the forces of constraint  $P$ ,  $Q$ ,  $R$ . Hence the algebraical sum of the moments about  $AB$  of all the external forces, including  $P$ ,  $Q$ , and  $R$ , is zero: but each of these moments except that of  $R$  is zero, since each of the corresponding forces either intersects  $AB$  or is parallel to it, Art. (46). The moment of  $R$  must therefore be zero, i.e.  $R$  itself is zero, since  $R$  neither meets  $AB$  nor is parallel to it. Similarly we may shew that the moment of  $Q$  about every line through  $A$  in the plane is zero, i.e.  $Q$  is either zero, or it lies in the plane in question. Also by taking moments about lines through  $B$  in the plane, except  $AB$ , we may shew that either  $P$  is zero, or it lies in the plane.

52. *Prop.* A number of forces acting on a rigid body, their lines of action all being in the same plane, will keep it in equilibrium, provided any of the following sets of conditions hold: (1) if the algebraical sum of their moments about each of three given points in the plane, but not in the same straight line, be zero; (2) if the algebraical sum of their moments about one given point in the plane, and of their resolved parts in any two given directions in the plane, be zero; (3) if the algebraical sum of their moments about two given points in the plane, and of their resolved parts in any given direction in the plane, not at right angles to the line joining the two points, be zero.

(1) Let  $A$ ,  $B$ ,  $C$  be the three given points: if the body is not in equilibrium, it can be fixed by applying forces of constraint  $P$  and  $Q$  at  $A$  and  $B$  respectively, both in the plane of the forces and  $Q$  perpendicular to  $AB$ . The whole system of forces including  $P$  and  $Q$  must satisfy the necessary conditions of equilibrium: therefore the algebraical sum of their moments about  $A$  is zero: but the algebraical sum of the moments of the original forces about  $A$  is zero, and the moment of  $P$  about  $A$  is zero



also; hence the moment of the remaining force  $Q$  is zero, i.e.  $Q$  itself is zero, as it does not pass through  $A$ . Similarly we can shew that the moments of  $P$  about both  $B$  and  $C$  are zero; hence either  $P$  is zero, or it passes through both  $B$  and  $C$ . As  $A$ ,  $B$ , and  $C$  are not in a straight line,  $P$  is zero. Hence the body is in equilibrium without any constraint.

(2) Let  $A$  be the given point, and  $B$  any other point in the plane of the forces: apply forces of constraint  $P$  and  $Q$  at  $A$  and  $B$  respectively as in (1). Then we shew as before that  $Q$  is zero. The forces *including*  $P$  must satisfy the necessary conditions of equilibrium: therefore the algebraical sum of their resolved parts in each of the two given directions is zero; but the algebraical sum of the resolved parts of the forces *excluding*  $P$ , in each of these two directions is zero, i.e. the resolved part of  $P$  in each of these directions is zero. But as the resolved part of a force is only zero, in a direction perpendicular to the force,  $P$  itself must be zero.

Hence the body is in equilibrium without constraint.

Case (3) can be proved in a similar way.

53. *Prop.* Two equal forces acting in opposite directions along the same straight line on a rigid body, but not necessarily on the same particle, keep it in equilibrium.

This is obvious as the two forces clearly satisfy the sufficient conditions of equilibrium given in the last article.

This proposition is essentially the same as the principle known as the *transmissibility of force*, which is generally assumed as an experimental fact, but which we prefer to deduce as above from the Laws of Motion. The formal statement of that principle is as follows: *when a force acts on a rigid body, it is indifferent on what particle in the line of action it acts, provided that particle is part of the body, or rigidly connected with it.* This follows directly from the proposition just proved. For let  $A$ ,  $B$

be any two particles in the line of action of the force, and rigidly connected with the body. We have just proved that a force equal and opposite to the given force, would counterbalance it, so long as the former acted at a point in  $AB$  rigidly connected with the body: hence the given force counteracts a certain other force, whether the given force acts at  $A$  or at  $B$ . As regards its effect on the body as a whole, we may say then, that it is indifferent at which point we apply the force. It is however in this sense only, that it is indifferent; if we take into consideration the internal forces brought into play in the two cases, they will probably be very different.

Imagine, for instance, a sphere resting on a smooth horizontal plane; a force of a certain magnitude, and in a certain direction will give the sphere the same change of motion, whether the force take the shape of a push behind or a pull in front, yet the internal forces in the sphere will be different in the two cases, as in the first case the tendency of the external force is to compress the sphere, whereas it has the opposite tendency in the second case.

The proof of the converse principle, viz. that if it is indifferent at which of two points a force is applied, the line of action of the force must be the line joining them, is obvious from what has gone before.

Ex. 1. A square lamina  $ABCD$  is acted upon by a force of 3 lbs. along  $AB$ , 2 lbs. along  $CB$ , 1 lb. along  $CD$ , 2 lbs. along  $AD$ ,  $\sqrt{2}$  lbs. along  $CA$ , and  $\sqrt{2}$  lbs. along  $BD$ : prove that it is in equilibrium.

Ex. 2. A weightless rod  $AB$ , 10 feet long, has weights of 7 lbs. hung at each end, and one of 11 lbs. at its middle point: a string is attached to a point 2 feet from  $A$  and after passing over a smooth peg vertically above the point of the rod to which it is attached, supports a weight of 10 lbs.: another string attached to a point 4 feet from  $B$  supports in a similar way a weight of 15 lbs. Prove that the rod is in equilibrium.

Ex. 3. A rigid rod  $AB$ , 20 inches long, is acted upon by the following forces: 3 lbs. at  $A$  along  $BA$ ,  $\sqrt{3}$  lbs. at right angles to  $AB$ , at a point 5 inches from  $A$ , 6 lbs. at a point 5 inches from  $B$ , and making an angle of  $60^\circ$  with the part of the rod on the same side as  $A$ , and  $4\sqrt{3}$  lbs.

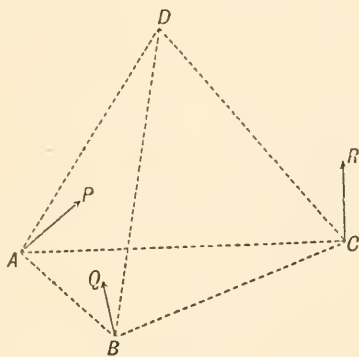


at  $B$  making an angle of  $30^\circ$  with  $AB$  produced. Prove that there will be equilibrium, provided all the forces are in one plane, and the 3rd force acts on the opposite side of the rod to the 2nd and 4th.

Ex. 4.  $ABCDEF$  is a regular hexagonal lamina: prove that it is kept in equilibrium by the following seven forces: 2 lbs. along  $AB$ ,  $CD$ ,  $DE$ ,  $FA$ , and  $AD$ , 3 lbs. along  $CB$  and 1 lb. along  $FE$ .

54.\* *Prop.* A rigid body under the action of any system of forces, is in equilibrium, provided the algebraical sum of their moments about each edge of any given tetrahedron be zero.

Let  $ABCD$  be the given tetrahedron, such that the



algebraical sum of the moments of the forces about each edge is zero. If the body is not in equilibrium under the action of the system of forces in question, it can be fixed (Arts. 50, 51) by applying suitable forces of constraint  $P$ ,  $Q$ ,  $R$  at  $A$ ,  $B$ , and  $C$  respectively. Also  $Q$  may be taken perpendicular to  $AB$ , and  $R$  perpendicular to the plane  $ABC$ .

Since the body is in equilibrium, under the action of the original forces, together with  $P$ ,  $Q$ ,  $R$ , these forces must satisfy the necessary conditions of equilibrium. Therefore the algebraical sum of their moments about  $AB$  is zero; but the algebraical sum of the moments of the original forces alone about  $AB$  is zero, and the moments

of both  $P$  and  $Q$  about  $AB$  are clearly zero, so that the moment of the remaining force  $R$  must be zero.  $R$  being perpendicular to the plane  $ABC$ , can neither intersect  $AB$  nor be parallel to it, so that its moment about  $AB$  can only vanish by  $R$  itself vanishing (Art. 38).

Similarly by taking moments about  $AC$  and  $AD$ , we see that the moment of  $Q$  about each of these lines is zero: hence  $Q$  must either be zero, or its line of action must lie in each of the planes  $BAC$ ,  $BAD$ , i.e. be the line  $AB$ ; the latter alternative is out of the question, because  $Q$  is perpendicular to  $AB$ :  $Q$  must therefore be zero.

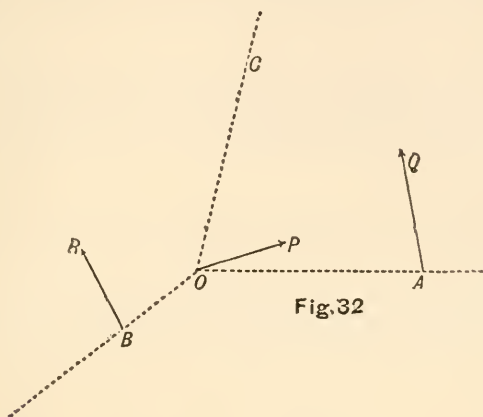
Again, by taking moments about  $BC$ ,  $DB$ , and  $DC$ , we obtain that the moment of  $P$  about each of these lines is zero, i.e. that if  $P$  is not zero, its line of action lies in each of the planes  $BAC$ ,  $BAD$ ,  $DAC$ , which is impossible.  $P$  must therefore be zero. All the forces of constraint being zero, we see that the body is in equilibrium under the action of the original forces only.

55.\* *Prop.* A rigid body under the action of any system of forces is in equilibrium, provided the algebraical sum of their moments about each of any three given straight lines intersecting in a point, but not in one plane, be zero, and the algebraical sum of their resolved parts along each of these lines be zero also.

Let  $OA$ ,  $OB$ ,  $OC$  be the straight lines, such that the algebraical sum of the moments of the forces, about each of them is zero, and that of their resolved parts along each is zero also.

As in the last proposition, if the body is not in equilibrium, it may be fixed by applying suitable forces of constraint  $P$ ,  $Q$ ,  $R$  at  $O$ ,  $A$  and  $B$  respectively;  $R$  may be taken perpendicular to the plane  $OAB$ , and  $Q$  perpendicular to the line  $OA$ . Then as before, by taking moments about  $OA$ ,  $R$  is found to be zero; and  $Q$  also by taking moments about  $OB$  and  $OC$ . But the algebraical sum of

the resolved parts of the original forces together with  $P$ , along each of the lines  $OA$ ,  $OB$ ,  $OC$  must be zero; hence



the resolved part of  $P$  along each of these lines must also be zero, i.e. if  $P$  is not zero, it is perpendicular to each of the lines  $OA$ ,  $OB$ ,  $OC$ , which is impossible as they do not lie in one plane.  $P$  must therefore be zero. The body is therefore in equilibrium under the action of the original forces alone.

The *sufficient* conditions of equilibrium of any system of forces acting on a rigid body can be expressed in many ways, other than the two given above.

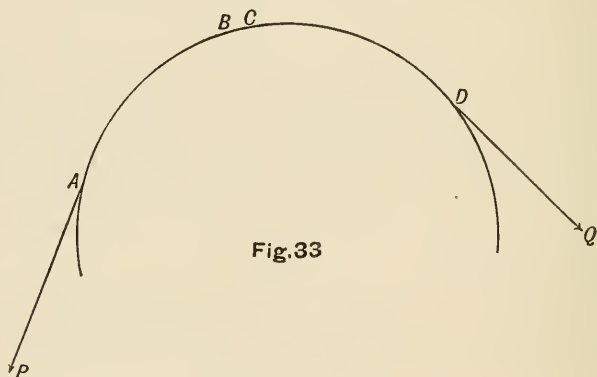
56. We have seen that if two systems of forces are equivalent, either of them reversed will counteract the other; hence it is sufficient for equivalence when both systems are in the same plane, if any one of the following sets of conditions holds. (1) If the algebraical sum of the moments about each of three points in the plane but not in the same straight line, of one system, be equal respectively to the corresponding sum of the other. (2) If the algebraical sums of the moments about one point in the plane, and of the resolved parts in two directions in it, of one system be equal respectively to the corresponding sums of the other. (3) If the algebraical sums of the

moments about each of two points in the plane, and of the resolved parts in one direction in the plane, not perpendicular to the line joining the two points, of one system, be equal respectively to the corresponding sums of the other.

Analogous conditions of equivalence can be obtained from Arts. 54, 55, for systems of forces which are not in one plane.

57. To find the resultant action on a body of a weightless string stretched round it.

Let  $PABCDQ$  be a string stretched over a body,  $A$  and  $D$  being the points where the string leaves the body. The forces acting on the part



$ABCD$  of the string are the force due to the part  $PA$ , or the *tension* at  $A$  along  $AP$ , the tension at  $D$  along  $DQ$ , and the innumerable actions of the body at every point of  $ABCD$ . Since this portion of the string is in equilibrium, the two tensions counteract all these actions along  $ABCD$ , i. e. they just balance the resultant of all these actions. But by Newton's Third Law, the resultant action of the string on the body is equal to, opposite to, and in the same straight line as, that of the body on the string. The two tensions counteract the latter of these resultants, i. e. they are equivalent to the former. We may therefore, in considering the equilibrium of the body, suppose that it is acted on *directly by the tensions at  $A$  and  $D$* , instead of supposing, what is really the case, that these tensions act on the string  $ABCD$ , and so cause it to exert on the body the innumerable small forces, to which the tensions are equivalent.

We arrive at the same conclusion by regarding the body and the portion  $ABCD$  of the string as one system of particles: in that case the tensions at  $A$  and  $B$  are forces *external* to the system, while the innumerable actions and reactions between the string and the body are *internal* forces.

Ex. 1. A smooth pulley is supported by a string which passes underneath it: find the weight of the pulley, if the tension of the string is 10 lbs. and the two parts not in contact with the pulley make angles of  $30^\circ$  with the vertical. Ans.  $10\sqrt{3}$  lbs.

Ex. 2. A rope is passed several times round a fixed rough post, the tensions exerted at the ends of the two parts of the rope not in contact with the post, are 3 lbs. and  $2\sqrt{2}$  lbs. respectively, and these two parts make an angle of  $45^\circ$  with one another. Find the resultant action of the rope on the post. Ans.  $\sqrt{29}$  lbs.

Ex. 3. A circular cylinder ( $W$ ) is placed with its axis horizontal on a smooth inclined plane: a weightless string is attached to a point in the plane and after passing over the cylinder supports a weight  $P$ , the straight portions of the string being respectively horizontal and vertical: shew that if there is equilibrium, the inclination of the plane to the horizon is

$$\tan^{-1} \{P / (P + W)\}.$$

58. We have seen how to obtain the resultant of two forces acting on the same particle; if now we have two forces acting on a rigid body, but not on the same particle, we can find a single force equivalent to them provided their lines of action either meet or are parallel, except in the case in which the forces are equal and opposite, but not in the same straight line. If their lines of action meet in a point, we may by the principle of the transmissibility of force, suppose each force to act at this point, and then their resultant is just what it would be if the forces really acted on a particle, situate there and rigidly connected with the body.

59. When the forces are parallel, their resultant is a force in the same plane, whose resolved part in each of two directions in that plane equals the algebraical sum



of the resolved parts of the two forces in the same direction, and whose moment about some point in the plane equals the algebraical sum of the moments of the two about that point.

Let  $A, B$  be two points where two parallel forces,  $P, Q$  respectively act. Then the first two conditions are

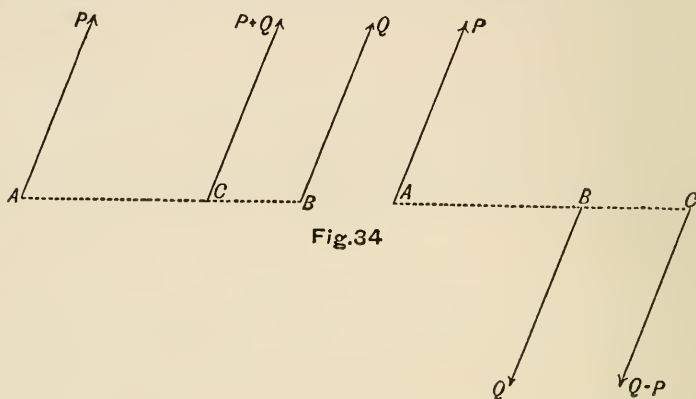


Fig.34

satisfied, provided this force acts in the same direction as  $P$  and  $Q$ , and is equal to their algebraical sum. It must then be parallel to the other two, and at such distances from them that their moments about any point in it are equal in magnitude but opposite in sign. It must then be between them if the signs of  $P$  and  $Q$  are the same, but not otherwise: its distances from them must be inversely proportional to their magnitudes. Hence if  $C$  be the point where its line of action meets  $AB$ ,  $P.AC = Q.BC$ . When  $P$  and  $Q$  act in opposite directions, the greater force will clearly lie between the less and the resultant.

*Cor.* The position of  $C$  is independent of the direction of the forces, so long as they remain parallel.

If the forces  $P$  and  $Q$  are equal in magnitude and opposite in sign, the preceding solution fails, and we can find no single force, whose effect is equal to that of the two together. Two such forces constitute a *couple*.



Ex. 1. Four forces,  $P$ ,  $2P$ ,  $3P$ , and  $4P$  act along the sides taken in order of a square: find their resultant.

*Ans.*  $2P\sqrt{2}$ , acting parallel to the diagonal joining the corner where  $2P$ , and  $3P$ , meet with the opposite corner, and at a distance from it  $\frac{5}{4}\sqrt{2}$  times a side of the square.

Ex. 2. A uniform beam 4 ft. long is supported in a horizontal position by two props which are 3 feet apart, so that the beam projects one foot beyond one of the props: shew that the pressure on one prop is double the pressure on the other.

Ex. 3. If a bicycle and its rider weigh 60 lbs. and 10 stone respectively, find how the pressure on the ground is divided between the two wheels, whose points of contact with the ground are 3 ft. 6 inches apart, while the points through which the weights of the bicycle and rider act, are distant horizontally 7 in. and 6 in. respectively from the centre of the driving wheel.

*Ans.* 170 lbs. and 30 lbs.

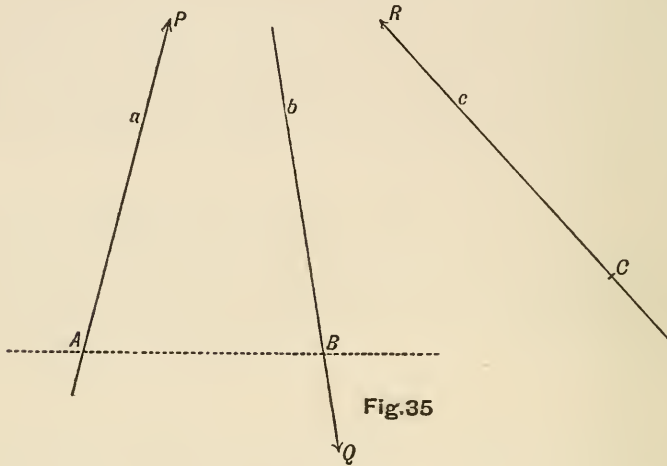
60. Since a rigid body under the action of any system of coplanar forces, can be fixed by two forces of constraint acting in that plane at two arbitrarily chosen points in it, the system must be equivalent to the forces of constraint reversed: but two forces in one plane can be replaced by a single one, unless they form a couple. Hence any system of forces in one plane is equivalent to a single force or a couple.

61. *Prop.* If three forces maintain equilibrium, their lines of action must be in one plane, and either all meet in one point or be all parallel.

Let  $P$ ,  $Q$ ,  $R$  be the three forces,  $Aa$ ,  $Bb$ ,  $Cc$ , their respective lines of action.

Since the algebraical sum of the moments of a system of forces in equilibrium about any line is zero, that of the moments of  $P$ ,  $Q$ ,  $R$  about  $AB$  vanishes: but as  $P$  and  $Q$  both intersect this line, each of their moments about it is zero, hence that of  $R$  about it must also be zero, i.e.  $Cc$  meets  $AB$  or is parallel to it. Similarly we can shew that  $Cc$  meets, or is parallel to, each of the lines obtained by

joining any point in  $Aa$ , with any point in  $Bb$ , which is impossible unless  $Aa$ ,  $Bb$  lie in one plane. Hence all three forces are in one plane.



If the forces are not all parallel, two of them meet and can be replaced by a single force, which is counterbalanced by the third force, and is therefore in the same straight line with it, i.e. the third force passes through the point of intersection of the other two.

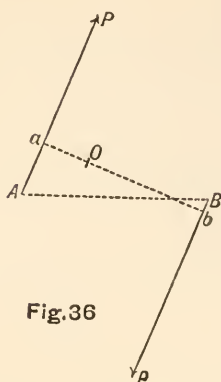
*Cor.* Two forces, whose lines of action are not in one plane, cannot be equivalent to a single force.

62. *Def.* The moment of a couple is the algebraical sum of the moments of the two forces which form it, about any point in their plane.

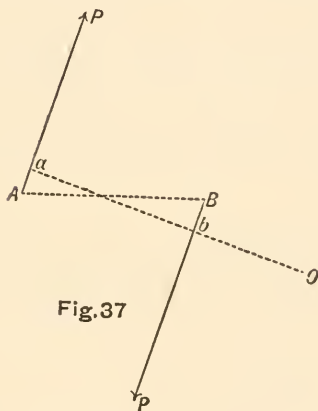
This moment can easily be shewn to be independent of the position of the point and to be equal to the product of either force into the *arm*, i.e. the perpendicular distance between the lines of action of the forces.

For let  $P$  acting at  $A$ , and  $P$  acting in the opposite direction at  $B$ , form the couple. Then the algebraical sum of the moments of the two forces about  $O$  is

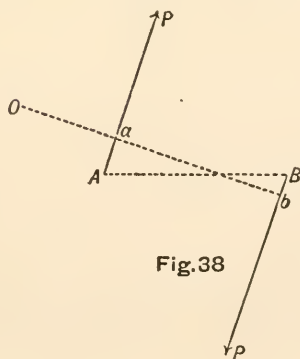
in Fig. (36),  $P (Oa + Ob) = P . ab,$



in Fig. (37),  $P (Oa - Ob) = P . ab,$



in Fig. (38),  $P (Ob - Oa) = P . ab,$



where  $Oa$ ,  $Ob$  are the perpendiculars from  $O$  on the lines of action of the forces.

If the body on which the couple acted were only free to turn round  $O$ , the tendency of the couple in all the above figures is to turn the body in the direction in which the hands of a watch move; the couples are said therefore to have moments of the same sign, or to be *like*; were the tendency of one of them to turn the body in the opposite direction, its moment would be of the opposite sign, and it would be *unlike* the other two.

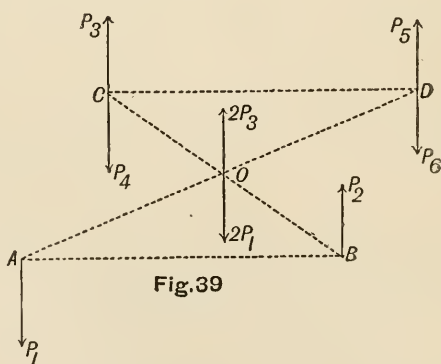
63. *Prop.* Two like couples of equal moment, in the same or parallel planes, are equivalent to one another.

(i) When the couples are in the *same* plane.

In this case the two couples form two systems of forces in one plane, such that the algebraical sums of their moments about any point whatsoever in the plane are the same; therefore the systems are equivalent to one another (Art. 56).

(ii) When the couples are in *parallel* planes.

Let  $P_1$ ,  $P_2$  be the two equal forces forming one of the couples, acting at the points  $A$ ,  $B$  respectively.



In the plane in which the other couple acts, draw  $CD$  equal and parallel to  $AB$ . Then the effect of  $P_1$ ,  $P_2$  will

not be altered by introducing at  $C$ ,  $P_3$ ,  $P_4$ , two forces in opposite directions, each equal and parallel to  $P_1$ , and also two similar forces  $P_5$ ,  $P_6$  at  $D$ . Join  $AD$ ,  $BC$ , intersecting in  $O$ ; then  $O$  bisects both  $AD$  and  $BC$ .

$P_3$  and  $P_2$  are equivalent to  $2P_3$  at  $O$ , in the same direction as  $P_3$  and  $P_1$  and  $P_6$  are equivalent to  $2P_1$  at  $O$  in the opposite direction to  $P_3$ :  $2P_3$  and  $2P_1$  at  $O$  will counteract one another, so that we are left with  $P_4$  at  $C$  and  $P_5$  at  $D$ , as equivalent to the original couple. But these two forces constitute a couple *like* to the original one, equal to it and in the given plane parallel to it: therefore as the original couple is equal to *one* couple in the parallel plane, it is by (i) equal to *any* like couple of the same moment in that plane.

64.\* The latter part of the last proposition might have been proved in a manner analogous to that adopted for the former, as follows.

Let  $A$  and  $B$  be the two couples: we shall prove that  $A$  and  $B$  reversed satisfy the sufficient conditions of equilibrium of Art. 55.

Take three straight lines, intersecting in a point, one perpendicular to the plane of each couple, and the other two in the plane of  $B$ .

It is obvious that the algebraical sum of the resolved parts of the four forces in each of these directions is zero: also the moments of  $A$  and  $B$  reversed, about the line perpendicular to their planes, are numerically equal but of opposite sign. Hence the algebraical sum of the moments of the four forces forming them about this line is zero. The moment of each of the forces forming  $B$  reversed about any line in their plane is zero, and the moments of the two forces forming  $A$ , about any line in the plane of  $B$ , are equal numerically but of opposite sign; the algebraical sum of the moments of all four forces about every straight line in the plane of  $B$  is therefore zero.

The six sufficient conditions of equilibrium of Art. 55 are therefore satisfied, and the couples  $A$  and  $B$  reversed

balance one another; in other words  $A$  and  $B$  are equivalent.

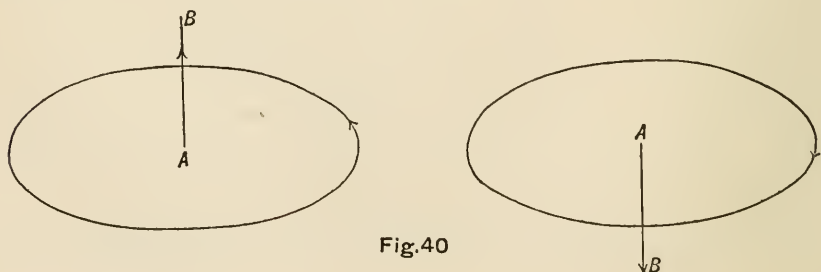
Ex. 1. Like parallel forces, each equal to  $P$ , act at three of the corners of a rhombus, perpendicular to its plane: at the other corner such a force acts that the four forces are equivalent to a couple: find the moment of the couple, provided the angle at which the last force acts be  $60^\circ$ .

*Ans.*  $2\sqrt{3} \cdot Pa$ , where  $a$  is a side of the rhombus.

Ex. 2.  $ABCDEF$  is a regular hexagon: equal forces act along  $AB$ ,  $BC$ ,  $DE$ ,  $EF$ , and two other forces, each double any one of the former forces, act along  $DC$  and  $AF$ : prove that they maintain equilibrium.

65.\* Let us consider what we require to know to determine the effect of a couple on a rigid body. It is unnecessary to know the actual position of the plane in which the couple acts, but we must know the *direction* of the plane, i.e. the direction of a line to which it is perpendicular. We do not require to know the magnitude or direction of the forces which compose the couple, but we must know the *magnitude* of its *moment* and its *sign*, i.e. the direction in which it would tend to turn the body round a line perpendicular to its plane, the line being fixed and the body rigidly connected with it.

Now a straight line at right angles to the plane of the couple, and of length proportional to the magnitude of its moment, will represent the couple in the first two respects: also, if it be understood that the line is drawn in that direction in which the axis of a right-handed screw moves, when it rotates in the same way as the couple tends to turn the body, the *sign* of the couple will also be represented.





In fig. 40, if the arrowhead on the circle indicates the direction in which the couple would tend to turn the body about  $AB$ , supposing the latter fixed and the body rigidly connected with it, the sign of the couple in accordance with the above convention would be represented by  $AB$  and not by  $BA$ .

The line which thus completely represents the couple is termed the *axis* of the couple.

66.\* We shall now prove that couples follow the *Parallelogram Law*, in other words, that if from a point the axes representing two couples be drawn, and a parallelogram be constructed on these two axes as adjacent sides, the diagonal passing through the above-mentioned point is the axis of a couple equivalent to the two, i.e. their resultant couple.

We may suppose the couples to consist of forces acting at the ends of a common arm, in which case the

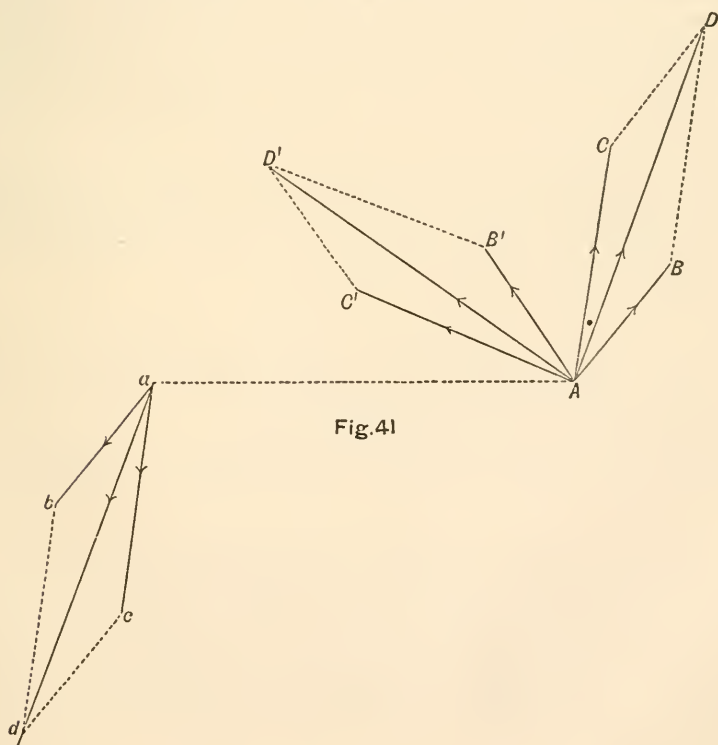


Fig. 41

moments of the couples will be respectively proportional to the forces composing them.

Let  $Aa$  be the common arm, and let  $AB, ab$  represent the two equal and parallel forces forming the first couple,  $AC, ac$  those forming the second.

Draw  $AB'$  perpendicular to  $Aa$  and  $AB$ , equal to  $AB$ , and in the direction which by the convention of Art. 65 represents the sign of the first couple: similarly draw  $AC'$  perpendicular to  $Aa$  and  $AC$ , equal to  $AC$  and in the proper direction. Then  $AB'$  and  $AC'$  are the axes of the two couples.

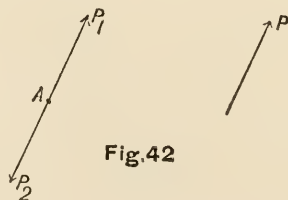
Complete the three parallelograms,  $ABCD$ ,  $abcd$ ,  $AB'C'D'$ , and join  $AD$ ,  $ad$ ,  $AD'$ . These parallelograms are clearly equal in every respect, so that  $AD = ad = AD'$ . Also  $AD, ad$  are parallel, and  $AD'$  is perpendicular to  $AD$ .

But the two forces  $AB, AC$  are equivalent to  $AD$ , and the two  $ab, ac$  to  $ad$ , so that the two couples are equivalent to  $AD, ad$ , which form a couple of which  $AD'$  is the axis. Hence the couples whose axes are  $AB', AC'$  are equivalent to a resultant couple of which  $AD'$  is the axis.

*Cor.* Hence we may deduce propositions relating to the composition and resolution of couples, analogous to those obtained in Arts. 19—26, 30—32, relating to the composition and resolution of forces.

67.\* *Prop.* Any system of forces acting on a rigid body can be reduced to a single force acting at any arbitrarily chosen point and a couple.

Let  $A$  be the arbitrarily chosen point,  $P$  any one of the forces.



We shall not alter the effect of the forces by applying at  $A$  two forces  $P_1, P_2$  each equal and parallel to  $P$ , and in opposite directions to one another.  $P_2$  which is opposite to  $P$ , forms with  $P$  a couple. Hence  $\vec{P}$  is equivalent to  $P_1$  at  $A$ , and a couple.

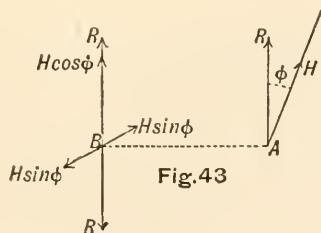
The couple vanishes in the case in which  $A$  lies in  $P$ 's line of action.

Similarly we may replace each of the other forces by a force at  $A$ , equal to it and in the same direction, and a couple.

The whole system thus reduces to a series of forces at  $A$ , respectively equal to and in the same direction as the several original forces, and a series of couples. But the forces at  $A$  are equivalent to a single resultant at  $A$ , and the couples to a single resultant couple.

*Cor.* The magnitude and direction of the single resultant is the same wherever  $A$  is, and the resultant couple is the same for all positions of  $A$  in a line parallel to the single resultant force.

68.\* *Prop.* Any system of forces acting on a rigid body is equivalent to a single force and a couple whose plane is perpendicular to the direction of the single force.



By the last proposition, the system is equivalent to a single force  $R$  acting at any given point  $A$ , and a couple  $H$ . If the axis of  $H$  make an angle  $\phi$  with the direction of  $R$ , it may be resolved into  $H \cos \phi$  in the direction of  $R$  and  $H \sin \phi$  at right angles to that direction.

Draw  $AB$  perpendicular both to  $R$  and the axis of  $H$ , and make  $AB$  equal to  $(H \sin \phi)/R$ , then applying at  $B$  two forces equal and parallel to  $R$ , but in opposite directions to one another, the system is equivalent to  $R$  at  $B$  in its original direction, the couples  $H \cos \phi$ ,  $H \sin \phi$ , and the two forces  $R$  at  $A$ , and  $R$  in the opposite direction at  $B$ . But the last two forces are equivalent to a couple whose axis is at right angles to both  $R$  and  $AB$ , i.e. is in the same straight line as the axis of the couple  $H \sin \phi$ : its moment is  $R \cdot AB$  or  $H \sin \phi$ . If  $AB$  be drawn as in fig. 43, the axes of these two couples are in opposite directions by the convention of Art. 65: the two couples therefore counteract one another, and we are left with  $R$  at  $B$  and the couple  $H \cos \phi$  whose axis is along  $R$ 's direction. Such a force and couple together form what is called a *wrench*.

$R$ 's line of action through  $B$  is termed *Poinsot's Central Axis*.

The algebraical sum of the moments of the system of forces about the axis of  $H$  through  $A$  is  $H$ , about a line through  $A$ , making an angle  $\theta$  with  $AH$ , the sum of their moments is  $H \cos \theta$ . Hence  $AH$  is called the *axis of principal moment* at  $A$ , as the sum of the moments of the forces about it is greater than that about any other line through  $A$ .

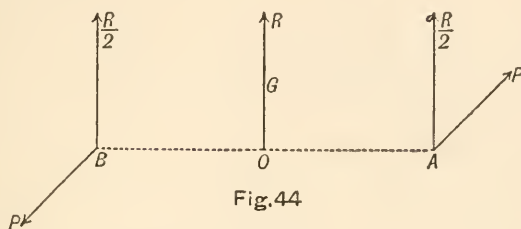
69.\* *Prop.* The algebraical sum of the moments of the forces about Poinsot's Central Axis is less than that about any other axis of principal moment.

For (Art. 68) (fig. 43) the sum of the moments about the central axis is  $H \cos \phi$ , whereas the sum of the moments about the axis of principal moment at  $A$  is  $H$ .

For this reason the Central Axis is sometimes termed the *axis of least principal moment*.

70.\* *Prop.* Any system of forces acting on a rigid body can be reduced to two equal forces equally inclined to the Central Axis.

For let  $OG$  be the central axis,  $R$  being the single resultant force, and  $H$  the moment of the resultant couple whose axis is  $OG$ .



Through  $O$  draw  $AOB$  perpendicular to  $OG$ , and make  $OA = OB$ .

We can replace  $R$  by  $R/2$  at  $A$ , and  $R/2$  at  $B$ , each in the same direction as  $R$ ; we can replace the couple  $H$  by a force  $P$  at  $A$ , and a force  $P$  at  $B$ , each perpendicular to the plane  $GOA$ , but in opposite directions, provided  $P = \frac{H}{AB}$ .

The resultant of  $P$  and  $R/2$  at  $A$ , and that of  $P$  and  $R/2$  at  $B$ , will clearly be equal to one another and will make equal angles with  $R/2$ , i.e. with the Central Axis.

71. *Recapitulation.* Regarding any body at rest whatsoever, as a collection of particles each of which is at rest, we can assert that the algebraical sum of the resolved parts in any direction, of all the forces, internal as well as external, acting on the body is zero: also that the algebraical sum of their moments about any line is zero. But as by Newton's Third Law the internal forces consist entirely of pairs, which are equal, opposite and in the same straight line as one another, the algebraical sums of the resolved parts and of the moments of the internal forces are both zero. Any system of external forces which, together with internal ones, maintain a body in equilibrium, must therefore be such that the algebraical sum of their resolved parts in any direction is zero and that of their moments about any line is zero also.



Next, considering rigid bodies only, we shew that a body under the action of any system of external forces whatsoever can be fixed by the application of suitable forces at three arbitrarily chosen points, and that the direction of one of these forces may be taken perpendicular to the plane containing the three points, and that of another perpendicular to the line joining its point of application to the third point. When the forces are coplanar, the body can be fixed by applying suitable forces at any two points in the plane of the forces, the directions of both forces being in the plane and that of one perpendicular to the line joining the two points. From this proposition follow the *sufficient* conditions of equilibrium of a system of coplanar forces acting on a rigid body. These conditions may be given in three different forms, and each form is expressed algebraically by three equations. When the forces are not in one plane the sufficient conditions of equilibrium can be put in many different forms, and each form requires for its algebraical expression six equations.

Defining two forces as equivalent, when either counteracts the other reversed, we deduce the principle known as the 'Transmissibility of Force.'

The resultant of two parallel forces is obtained by finding from the sufficient conditions of equilibrium, a force which will counteract them, and then reversing it.

It is then shewn that if three forces maintain equilibrium, they must be coplanar and either concurrent or parallel.

Then we shew that two couples are equivalent when their moments are equal and their planes coincident or parallel; hence that couples can be represented by straight lines, and that they can be compounded and resolved like forces by the Parallelogram Law. It was shewn that any system of forces in one plane is equivalent to a single force or a couple, it can now be shewn that any system of forces whatsoever, acting on a rigid body, is



equivalent to a single force and a couple acting in a plane perpendicular to the force, or to two equal forces, equally inclined to the Central Axis.

ILLUSTRATIVE EXAMPLES.

Ex. 1. If four forces acting along the sides of a quadrilateral are in equilibrium, prove that the quadrilateral is a plane one, and also, that if the quadrilateral can be inscribed in a circle, each force must be proportional to the length of the opposite side.

Let  $ABCD$  be the quadrilateral. The forces along  $AB$ ,  $BC$  have a resultant through  $B$  and in the plane  $ABC$ ; similarly those along  $AD$ ,  $DC$

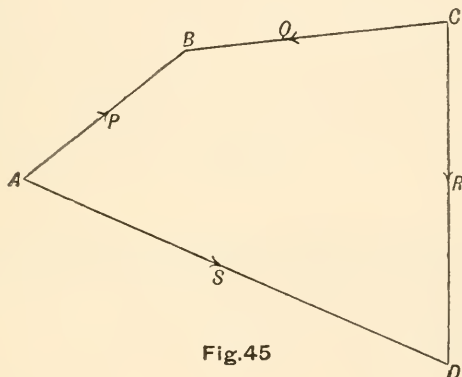


Fig.45

have a resultant through  $D$  and in the plane  $ADC$ . But as the four forces are in equilibrium, these two resultants must be in the same straight line,  $BD$ , i.e.  $BD$  is in each of the planes  $ABC$ ,  $ADC$  and the quadrilateral is a plane one.

When  $ABCD$  can be inscribed in a circle let  $P$ ,  $Q$ ,  $R$ ,  $S$  be the forces along  $AB$ ,  $CB$ ,  $CD$ ,  $AD$ , respectively.

Since the forces are in equilibrium, the algebraical sum of their moments about  $A$  is zero:

$$\therefore Q \cdot AB \sin B - R \cdot AD \sin D = 0;$$

$$\therefore \frac{Q}{AD} = \frac{R}{AB} = \text{similarly, } \frac{P}{CD} = \frac{S}{BC}.$$

Ex. 2.  $ABCD$  is a quadrilateral, and two points  $P, Q$  are taken in  $AD, BC$  such that  $AP : PD = CQ : QB$ . From  $P, Q$ , straight lines  $PP', QQ'$  are drawn parallel to, equal to, and in the same directions as  $BC$  and  $DA$  respectively. Shew that forces represented by  $AB, CD, PP', QQ'$  are in equilibrium.

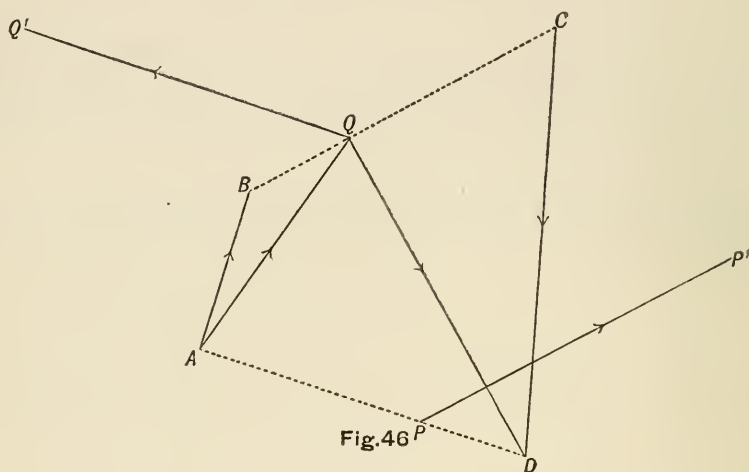


Fig. 46

The force  $PP'$  can be replaced by two forces parallel to it, at  $A$  and  $D$ :  
the force at  $A : PP' = PD : AD = BQ : BC$ ;

$\therefore$  force at  $A = BQ$ ;

similarly, that at  $D = QC$ .

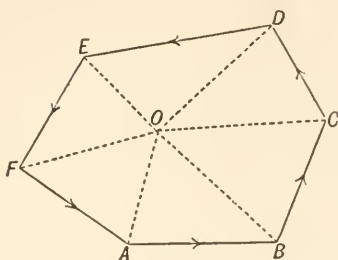
The two forces  $AB, BQ$ , acting at  $A$ , are, by the triangle of forces, equivalent to  $AQ$ ; and the two  $QC, CD$ , at  $D$ , to  $QD$ . Hence the four original forces are equivalent to  $AQ, QD$ , and  $QQ'$ , all acting through  $Q$ , and represented by the sides of the triangle  $AQD$ , taken in order. They are therefore in equilibrium.

Ex. 3. A system of forces represented by the sides of a plane polygon, taken in order, is equivalent to a couple, whose moment is represented by twice the area of the polygon.

Let the forces be represented by the sides  $AB, BC, CD, DE, EF, FA$ , of the polygon  $ABCDEF$ .

We know that if the forces are not in equilibrium, they are equivalent to a single resultant or a couple (Art. 60).

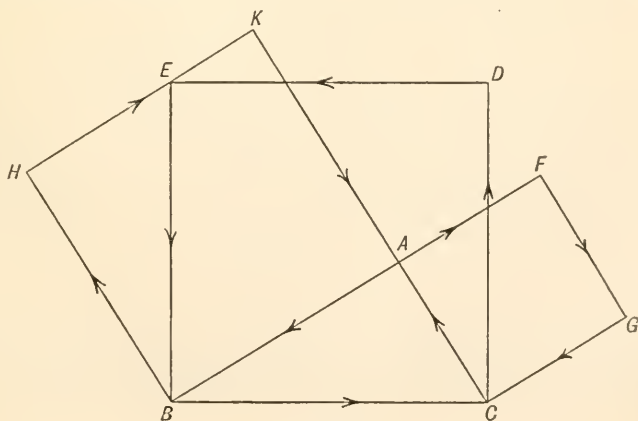
But as the algebraical sum of their resolved parts in any direction is



zero, their resultant is zero, i.e. they are in equilibrium, if they are not equivalent to a couple.

Take any point  $O$ , and join  $OA, OB, OC, \&c.$ : then the moment of  $AB$  about  $O$  is measured numerically by twice the area of the triangle  $OAB$ , since the area of  $OAB$  is equal to  $\frac{1}{2}AB$  into the perpendicular from  $O$  on  $AB$ : and similarly for the other moments. Hence the algebraical sum of the moments of  $AB, BC, \&c.$  about  $O$  is measured by twice the area of the polygon, i.e. is not zero. The system then must be equivalent to a couple, and the moment of this couple is represented by twice the area of the polygon.

Ex. 4. On the sides of a right-angled triangle  $ABC$  squares are described, the square  $BCDE$  on the hypotenuse on the same side of  $BC$  as  $A$ , and the squares  $CAFG, ABHK$  on  $CA, AB$  on the opposite side of each to the triangle: prove that the forces represented by the straight lines  $AB, BC, CA, BH, HK, KA, CD, DE, EB, AF, FG, GC$  will form a system in equilibrium.



The twelve forces are represented, four by the sides taken in order, of  $CAFG$ , four by those of  $ABHK$ , and four by those of  $BCDE$ .

The algebraical sum of their resolved parts in any direction is zero: also by the last example the algebraical sum of the moments about any point, of the first four, is represented by twice the area of  $CAFG$ , that of the second four by twice  $ABHK$ , and that of the third four by twice  $BCDE$ . If the sum of the moments of the first four be considered negative, that of the second four is negative and that of the third four is positive. Hence, since the area of  $BCDE$  is equal to the sum of the areas of  $ABHK$ ,  $CAFG$ , the algebraical sum of the moments about any point, of the twelve forces, is zero, i. e. the forces are in equilibrium.

Ex. 5. A uniform rod hangs by two strings of lengths  $l, l'$ , fastened to its ends and to two points in the same horizontal line, distant  $a$  apart, the strings crossing one another. Find the position of equilibrium, and shew that if  $\alpha, \alpha'$  be the angles that  $l, l'$  make with the horizontal

$$\sin(\alpha + \alpha') (l' \cos \alpha' - l \cos \alpha) = a \sin(\alpha - \alpha').$$

Let  $\theta$  be the angle which the rod  $AB$  makes with the vertical: let  $O$  be the point where the strings cross one another. Since the rod is in equi-

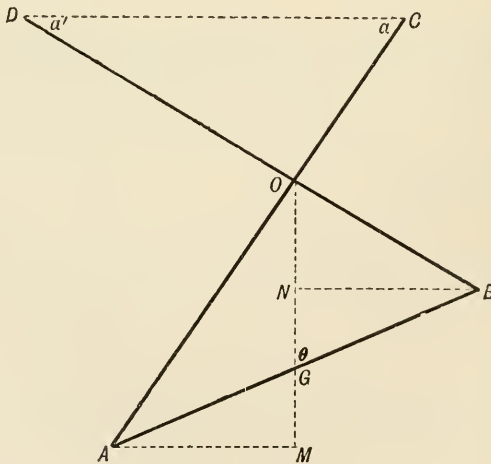


Fig.49.

librium under the action of three forces, two of which, the tensions of the strings, meet in  $O$ , the third, the weight of the rod, passes through  $O$ . But the weight acts vertically through the middle point of the rod, which

point  $G$ , must therefore be in a vertical line with  $O$ : hence the perpendiculars  $AM, BN$  on  $OG$  must be equal.

$$\therefore (l - OC) \cos \alpha = (l' - OD) \cos \alpha'.$$

But

$$\frac{OC}{\sin \alpha'} = \frac{OD}{\sin \alpha} = \frac{a}{\sin (\alpha + \alpha')},$$

$$\therefore \left\{ l - \frac{a \sin \alpha'}{\sin (\alpha + \alpha')} \right\} \cos \alpha = \left\{ l' - \frac{a \sin \alpha}{\sin (\alpha + \alpha')} \right\} \cos \alpha',$$

or  $\sin (\alpha + \alpha') (l \cos \alpha - l' \cos \alpha') = a \sin (\alpha' - \alpha) \dots \dots \dots (1).$

If  $b$  be the length of  $AB$ , we have since the algebraical sums of the vertical and horizontal projections of  $AB, BD, DC, CA$  are both zero,

$$l \sin \alpha - b \sin \theta - l' \sin \alpha' = 0,$$

$$l \cos \alpha - b \cos \theta + l' \cos \alpha' - a = 0'.$$

These equations with (1) enable us to obtain  $\alpha, \alpha'$ , and  $\theta$ , which determine the position of equilibrium.

The above is an example of a *geometrico-statical* problem, in which the position of equilibrium, which must clearly exist, is required, and is obtained from geometrical considerations.

If the weight of the rod be given, the other unknown quantities, the tensions of the strings, can be obtained by using two more conditions of equilibrium, since there are three, and one only has been used. As there are five unknown quantities, and only three sufficient conditions of equilibrium, we must have two geometrical conditions in order to completely solve the problem.

Ex. 6. A uniform heavy rod of length  $a$  is placed across a smooth horizontal rail and rests with one end against a smooth vertical wall, the distance of which from the rail is  $h$ : shew that the angle the rod makes with the horizon is  $\cos^{-1} (h/a)^{\frac{1}{3}}$ .

Let  $\theta$  be the inclination of the rod to the horizon, in the position of equilibrium. The forces acting on the rod  $AB$  are its weight vertically downwards through  $G$ , its middle point, the reaction of the wall, horizontally through  $A$ , and that of the rail  $C$ , at right angles to  $AB$ . These forces must therefore meet in a point  $D$ . Since  $ADG, ACD$  are right angles,

$$AD^2 = AC \cdot AG,$$

$$a^2 \cos^2 \theta = a \cdot h \sec \theta,$$

$$\therefore \cos^3 \theta = \frac{h}{a}.$$

Or, we might have proceeded thus: let  $R$  be the reaction of the wall,  $S$  that of the peg, and  $W$  the weight of the rod. Resolving vertically, we have

$$W - S \cos \theta = 0 \dots\dots\dots (1).$$

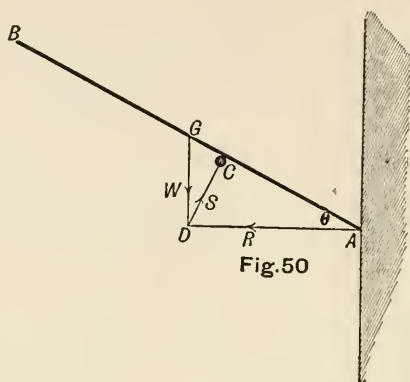


Fig. 50

Taking moments about  $A$ ,

$$S \cdot AC = W \cdot AD,$$

$$\therefore S \cdot h \sec \theta = W \cdot a \cos \theta \dots\dots\dots (2).$$

From (1) and (2)  $\cos^3 \theta = \frac{h}{a}.$

Resolving horizontally,

$$R - S \sin \theta = 0 \dots\dots\dots (3)$$

Hence  $R$  and  $S$  can be obtained.

The advantage of resolving vertically and taking moments about  $A$  is that in neither case does the force  $R$  come into the corresponding equation.

Ex. 7. Shew that the greatest inclination to the horizon at which a uniform rod can rest, partly within and partly without a fixed smooth hemispherical bowl, is  $\sin^{-1} (1/\sqrt{3})$ .

Let  $ADEC$  be the circular section of the complete sphere, made by the vertical plane containing the rod  $AB$ , which rests against the edge of the bowl at  $C$ .  $COD$  is the horizontal diameter of the sphere through  $C$ .

The rod is kept in equilibrium by its weight through  $G$ , its middle point, the reaction of the bowl at  $A$ , along the normal  $AO$ , and that at  $C$  perpendicular to  $AB$ , and therefore meeting  $AO$  on the sphere at  $E$ .

Since these three forces pass through one point,  $GE$  must be a vertical line.

Let  $ACO = \theta$ ,  $r =$  radius of the bowl.



Then

$$AC = AE \cos EAC = 2r \cos \theta \dots\dots\dots (1),$$

$$AG = AE \cdot \frac{\sin AEG}{\sin EGA} = 2r \frac{\cos 2\theta}{\cos \theta} \dots\dots\dots (2),$$

since

$$\angle AEG = \frac{\pi}{2} - EOF = \frac{\pi}{2} - 2\theta.$$

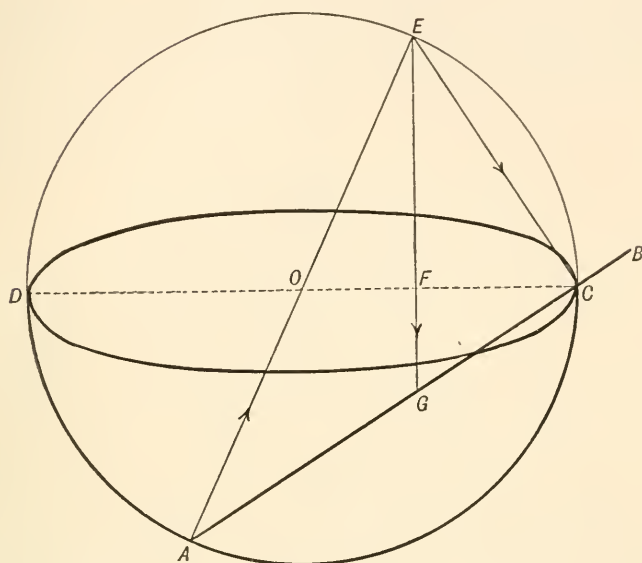


Fig.51.

Since  $AG$  is half the rod, (2) determines the position of equilibrium.

Let

$$m = \frac{AG}{AC},$$

$$\therefore m = \frac{\cos 2\theta}{\cos^2 \theta} = \frac{2 \cos^2 \theta - 1}{\cos^2 \theta},$$

$$\therefore \cos^2 \theta = \frac{1}{2 - m}.$$

$\theta$  clearly has its greatest value when  $m$  has its least value, i.e. when  $m = \frac{1}{2}$ , since  $AG$  cannot be less than half  $AC$ .

Hence the greatest value of  $\theta$  is given by

$$\cos^2 \theta = \frac{1}{2 - \frac{1}{2}} = \frac{2}{3},$$

or

$$\sin \theta = \frac{1}{\sqrt{3}}.$$

Ex. 8. Four equal spheres rest in contact at the bottom of a smooth spherical bowl, their centres being in a horizontal plane. Shew that, if another equal sphere be placed upon them, the lower spheres will separate if the radius of the bowl be greater than  $(2\sqrt{13}+1)$  times the radius of a sphere.

Let  $A, B, C, D$  be the centres of the four spheres respectively,  $O$  that of the upper sphere,  $O'$  that of the spherical bowl. Then  $AB, BC, CD,$

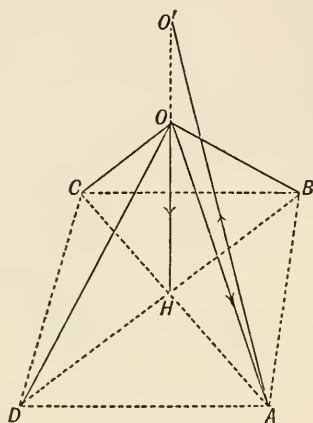


Fig.52

$DA, OA, OB, OC, OD$  are each equal to the diameter ( $2r$ ) of any one of the spheres.  $O$  and  $O'$  are clearly in the vertical line through  $H$ , the intersection of the diagonals of the square  $ABCD$ .

Then

$$\cos OAH = \frac{AH}{OA} = \frac{\frac{1}{\sqrt{2}}AB}{OA} = \frac{1}{\sqrt{2}},$$

$$\therefore OAH = 45^\circ.$$

When the lower spheres are just on the point of separating, there is no pressure between any two of them, so that each of them is in equilibrium under the action of its weight, the pressure of the upper sphere, and that of the hollow sphere. Let  $W$  be the weight of each sphere,  $R$  the reaction between the upper and any of the lower spheres. From the equilibrium of the upper sphere, resolving vertically,

$$W - 4R \cdot \frac{1}{\sqrt{2}} = 0,$$

$$\therefore R = \frac{W}{2\sqrt{2}}.$$

The resultant of  $W$  acting vertically, and  $\frac{W}{2\sqrt{2}}$  along  $OA$ , on the sphere

whose centre is  $A$ , makes with the vertical the angle  $\tan^{-1} \frac{\frac{W}{2\sqrt{2}} \cdot \frac{1}{\sqrt{2}}}{W + \frac{W}{2\sqrt{2}} \cdot \frac{1}{\sqrt{2}}}$ ,

i. e.  $\tan^{-1} \frac{1}{5}$ .

But this resultant is equal and opposite to the pressure of the bowl which acts along  $AO'$ .

Therefore  $\tan AO'H = \frac{1}{5}$ ,

$$\therefore \frac{AH}{O'A} = \sin AO'H = \frac{\frac{1}{5}}{\sqrt{1 + \frac{1}{25}}} = \frac{1}{\sqrt{26}}.$$

$$\therefore O'A = \sqrt{26} \cdot AH = 2\sqrt{13}r.$$

But the radius of the hollow sphere is equal to  $O'A$  together with  $r$ , therefore radius of the bowl =  $(2\sqrt{13} + 1)r$ .

If the bowl is any larger,  $O'$  will be further from  $H$ , and for the pressure of the bowl to counteract the resultant of the other forces on the sphere (centre  $A$ ), we shall have to suppose that the actions of the two adjacent lower spheres on it are towards their respective centres instead of away from them. But as the spheres are incapable of exerting such forces, equilibrium is not possible, i. e. the spheres will separate.

Ex. 9. A heavy bar,  $AB$ , is suspended by two equal strings of length  $l$ , which are originally parallel: find the couple which must be applied to the bar to keep it at rest after it has been twisted through an angle  $\theta$  in a horizontal plane.

Let  $C, D$  be the fixed ends of the strings;  $CA', DB'$  the original vertical positions of the strings.

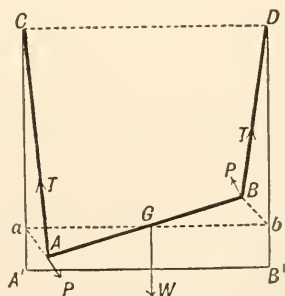


Fig. 53

Draw  $Aa, Bb$  at right angles to  $CA', DB'$  respectively. Join  $ab$  cutting  $AB$  in its middle point  $G$ . Let  $2a$  be the length of  $AB$ , and  $\phi =$  angle  $aCA$  or  $bDB$ .

Then  $CA \sin aCA = aA = 2AB \sin \frac{aGA}{2}$ ,

$$\therefore l \sin \phi = 2a \sin \frac{\theta}{2} \dots \dots \dots (1).$$

Let  $T$  be the tension of either string: they will from symmetry be the same.

Let  $P$  be the magnitude of the force which applied horizontally in opposite directions at  $A$  and  $B$ , at right angles to  $AB$ , will keep the rod in equilibrium.

Resolving vertically, we have

$$W - 2T \cos \phi = 0.$$

Taking moments about the line of action of  $W$ , we have

$$2P \cdot a - 2T \sin \phi \cdot a \cos \frac{\theta}{2} = 0.$$

Hence  $2Pa = \frac{aW \sin \phi \cdot \cos \frac{\theta}{2}}{\cos \phi} \dots \dots \dots (2).$

(1) and (2) enable us to determine  $2Pa$  in terms of  $a, l, W$  and  $\theta$ .

In this example we have assumed as obvious that a couple only is required to maintain equilibrium: it can be shewn however, that the values we have obtained for  $P$  and  $T$  will satisfy the six conditions of equilibrium of Art. 55.

EXAMPLES.

1. Four points  $A, B, C, D$  lie on a circle and forces act along the chords  $AB, BC, CD, DA$ , each force being inversely proportional to the corresponding chord: prove that the resultant passes through common points of (1)  $AD, BC$ ; (2)  $AB, DC$ ; (3) tangents at  $B, D$ , and (4) tangents at  $A$  and  $C$ .

2. If six forces acting on a body be completely represented, three by the sides of a triangle taken in order, and three by the sides of the triangle formed by joining the middle points of the sides of the original triangle, prove that they will be in equilibrium if the parallel forces act

in the same direction, and the scale on which the first three forces are represented be four times as large as that on which the last three are represented.

3. Forces  $P$ ,  $Q$ ,  $R$  act along the sides of a triangle  $ABC$ , and their resultant passes through the centres of the inscribed and circumscribed circles: prove that

$$\frac{P}{\cos B - \cos C} = \frac{Q}{\cos C - \cos A} = \frac{R}{\cos A - \cos B}.$$

4. Prove that a uniform rod cannot rest entirely within a smooth hemispherical bowl, except in a horizontal position.

5. If a uniform heavy rod be supported by a string fastened at its ends, and passing over a smooth peg; prove that it can only rest in a horizontal or vertical position.

6. A heavy equilateral triangle hung upon a smooth peg by a string, the ends of which are attached to two of its angular points, rests with one of its sides vertical; shew that the length of the string is double the altitude of the triangle.

7. A fine string  $ACBD$  tied to the end  $A$  of a uniform rod  $AB$  of weight  $W$ , passes through a fixed ring at  $C$ , and also through a ring at the end  $B$  of the rod, the free end of the string supporting a weight  $P$ ; if the system be in equilibrium prove that  $AC : BC :: 2P + W : W$ .

8. A horizontal rod, the ends of which are on two inclined planes, is in equilibrium: if  $\alpha$ ,  $\beta$  be the inclinations of the planes, prove that the centre of gravity of the rod divides it into two parts in the ratio of  $\tan \alpha$  to  $\tan \beta$ .

9. A uniform heavy rod  $AB$  has the end  $A$  in contact with a smooth vertical wall, and one end of a string is fastened to the rod at a point  $C$  such that  $AC = \frac{1}{4}AB$ , and the other end of the string is fastened to the wall; find the length of the string if the rod is in equilibrium in a position inclined to the vertical.

10. A cylindrical ruler whose radius is  $2a$ , and length  $2h$  rests on a horizontal rail with one end pressing against a smooth vertical wall, to which the rail is parallel. Shew that the angle the axis of the ruler makes with the vertical is given by  $(h \sin \theta + a \cos \theta) \sin^2 \theta + 2a \cos \theta = b$ , where  $b$  is the distance of the rail from the wall.

11. Two equal heavy spheres of one inch radius are in equilibrium within a smooth spherical cup of three inches radius. Shew that the

pressure between the cup and one of the spheres is double the pressure between the two spheres.

12. Along each side taken in order of a polygon inscribed in a circle, acts a force whose magnitude is proportional to the sum of the lengths of the two adjacent sides: prove that the system of forces is equivalent to a system of forces acting along the tangents at the corners of the polygon, each such force being proportional to the length of the chord joining the two adjacent points.

13.  $ABCD$  is a quadrilateral: forces act along the sides  $AB, BC, CD, DA$  measured by  $\alpha, \beta, \gamma, \delta$  times those sides respectively. Shew that if there is equilibrium

$$\alpha\gamma = \beta\delta.$$

Shew also that  $\triangle ABD/\triangle ABC = \alpha(\gamma - \beta)/\delta(\beta - \alpha)$ .

14. Into the top of a fixed smooth sphere of radius  $a$  is fitted firmly a fine smooth vertical rod. A bar of length  $2b$  has at one end a ring which slides on the rod; and the bar rests on the sphere. Shew that in equilibrium the angle ( $\alpha$ ) the bar makes with the horizontal is given by

$$a \sin \alpha = b \cos^3 \alpha.$$

15. Forces  $P, Q, R$  act along the sides  $BC, CA, AB$  of a triangle; shew that their resultant will act along the line joining the centre of the circumscribing circle to the intersection of perpendiculars if

$$P : Q : R :: \frac{\cos B}{\cos C} - \frac{\cos C}{\cos B} : \frac{\cos C}{\cos A} - \frac{\cos A}{\cos C} : \frac{\cos A}{\cos B} - \frac{\cos B}{\cos A}.$$

16. A kite (weight  $P$ ) having a tail (weight  $Q$ ) is stationary, with a normal to its face, the direction of the wind, which is horizontal, and the string in the same vertical plane. The tail is attached at a distance  $a$  below the kite's centre of gravity, the string at a distance  $b$  above. Shew that, neglecting the action of the wind on the tail, the inclination of the kite to the horizon is given by the equation

$$IIb \cdot \sin^2 \theta = \{Pb + Q \cdot (a + b)\} \cos \theta,$$

where  $II$  is the pressure on the kite, when placed perpendicular to the wind's direction.

17. Forces act at the middle points of the sides of a rigid polygon in the plane of the polygon; the forces act at right angles to the sides, and are respectively proportional to the sides in magnitude: shew that the forces will be in equilibrium if they all act inwards or all act outwards.



18. Shew that it is impossible to arrange six forces along the edges of a tetrahedron so as to form a system in equilibrium.

19. An uniform rod of weight  $W$  is supported in equilibrium by a string of length  $2l$  attached to its ends and passing over a smooth peg. If a weight  $W'$  be now attached to one end of the rod, prove that a length  $\frac{W'}{W+W'}$  of the string will slip over the peg.

20. If four parallel forces balance each other, let their lines of action be intersected by a plane, and let the four points of intersection be joined by six straight lines so as to form four triangles; then prove that each force is proportional to the area of the triangle whose angles are in the lines of action of the other three.

21. Two rings of weight  $P$  and  $Q$  respectively, slide on a string, whose ends are fastened to the extremities of a straight rod inclined at an angle  $\theta$  to the horizon: on the rod slides a light ring through which the string passes so that the heavy rings are on different sides of the light ring. Prove that in the position of equilibrium the inclination  $\phi$  of those parts of the string next the weightless ring, to the rod, is given by the equation  $\tan \phi / \tan \theta = (P + Q) / (P - Q)$ .

22. An elastic string passes round three equal right-circular cylinders so that when each cylinder touches the other two along a generating line, the string is just not stretched: shew that if the system be placed on a smooth horizontal plane, the inclination ( $\theta$ ) of the plane containing the axis of the upper cylinder, and that of either of the lower ones to the horizontal, in the position of equilibrium, is given by the equation  $(\pi + 3)W = 2\lambda(2 \cos \theta - 1) \tan \theta$ . ( $W$  is the weight of the upper cylinder, and  $\lambda$  is the modulus of elasticity.)

23. Two equal circular discs, of radius  $r$ , with smooth edges are placed on their flat sides in the corner between two smooth vertical planes inclined at an angle  $2\alpha$  and touch each other in the line bisecting the angle; the radius of the least disc which may be pressed between them without causing them to separate  $= r(1 - \cos \alpha) / \cos \alpha$ .

24. A rectangular lamina  $ABCD$  is supported with its plane vertical and one edge  $AB$  in contact with a smooth vertical wall, by an endless string which passes through smooth rings, one fixed to the wall at  $A$ , and two others  $P, Q$  fixed in the sides  $AB, CD$  of the lamina respectively

so that  $PQ$  is parallel to  $AD$ . Prove that the string has the least tension consistent with equilibrium when the position of  $Q$  is such that

$$BC/2AD = \tan \frac{1}{2}AQD.$$

25. Forces act through the angular points of a tetrahedron perpendicular to the opposite faces and proportional to them. Prove that they are in equilibrium if they all act either inwards or outwards.

26.  $AC, BD$  are two non-intersecting straight lines of constant length; prove that the effect of forces represented in every respect by  $AB, BC, CD, DA$  is the same, so long as  $AC, BD$  remain parallel to the same plane, and their projections on that plane are inclined at a constant angle to one another.

27. A flat semicircular board with its plane vertical and curved edge upwards rests on a smooth horizontal plane, and is pressed at two given points of its circumference by two beams which slide in smooth vertical tubes: find the ratio of the weights of the beams to one another when the board is in equilibrium.

28. An endless string is placed round two equal cylinders and the system is suspended from a peg so that the line joining the centres of the cylinders is horizontal. If the pressure between the cylinders be equal to twice the weight of either of them; prove that the length of the string : the radius of either cylinder ::  $4(2 + \tan^{-1} 2) : 1$ .

29. A homogeneous circular cylinder rests on two smooth planes inclined to the horizon at angles  $\alpha$  and  $\beta$  in opposite directions, so that its axis is at right angles to the line of intersection of the planes. Prove that the inclination  $\theta$  of the base to the vertical in the position of equilibrium is given by

$$\tan \theta = \frac{a \sin (\alpha - \beta)}{r \sin (\alpha + \beta) + 2a \sin \alpha \sin \beta},$$

where  $r$  is the radius of the base and  $2a$  the length of the cylinder.

30. In a triangular lamina  $ABC$ ,  $AD, BE, CF$  are the perpendiculars on the sides, and forces represented by the lines  $BD, CD, CE, AE, AF, BF$  are applied to the lamina; prove that their resultant will pass through the centre of the circle described about the triangle.

31. An elliptic lamina rests against an inclined plane ( $\alpha$ ) being supported by a string attached to the extremity of its minor axis, so that its major axis is vertical and the plane of the ellipse is perpendicular to the inclined plane. Shew that the inclination of the string to the vertical is  $\tan^{-1} b \sqrt{(a^2 + b^2 \tan^2 \alpha) / (a^2 - b^2)}$ .

32. A uniform bar of length  $a$  rests suspended by two strings of lengths  $l$  and  $l'$  fastened to the ends of the bar and to two fixed points in the same horizontal line at a distance  $c$  apart. If the directions of the strings, being produced, meet at right angles, prove that the ratio of their tensions is  $al + cl' : al' + cl$ .

33. Two weights  $P, P$  are attached to the ends of two strings which pass over the same smooth peg and have their other extremities attached to the ends of a beam  $AB$ , the weight of which is  $W$ ; shew that the inclination of the beam to the horizon  $= \tan^{-1} \left( \frac{a-b}{a+b} \tan \alpha \right)$ ;  $a, b$  being the distances of the centre of gravity of the beam from its ends, and  $\sin \alpha = W/2P$ .

34. A string 9 feet long has one end attached to the extremity of a smooth uniform heavy rod two feet in length, and at the other end carries a ring which slides upon the rod. The rod is suspended by means of the string from a smooth peg: prove that if  $\theta$  be the angle which the rod makes with the horizon, then  $\tan \theta = 3^{-\frac{1}{3}} - 3^{-\frac{2}{3}}$ .

35. A triangle formed of three smooth rods is fixed horizontally, and a homogeneous sphere rests on it. Prove that the pressure on each rod is proportional to its length.

36. A sphere rests on three smooth pegs, which lie in a horizontal plane, and are at distances  $a, b, c$  from one another, prove that the pressures on the pegs are in the ratios

$$a^2 (b^2 + c^2 - a^2) : b^2 (c^2 + a^2 - b^2) : c^2 (a^2 + b^2 - c^2).$$

37.  $ABC, A'B'C'$  are two triangles inscribed in the same circle; and forces proportional to the sides of the triangle act along them, but in opposite directions round the two triangles. Prove that, if  $\alpha, \beta, \gamma$  be the angles subtended at the centre of the circle by the sides of the one triangle, and  $\alpha', \beta', \gamma'$  those subtended by the sides of the other, the forces will be in equilibrium if  $\sin \frac{\alpha}{2} \sin \frac{\beta}{2} \sin \frac{\gamma}{2} = \sin \frac{\alpha'}{2} \sin \frac{\beta'}{2} \sin \frac{\gamma'}{2}$ .

38.  $A, B, C, D$  are four points in space: four forces represented by  $AB, AD, CB$ , and  $CD$  act along these lines: prove that they have a single resultant, the line of action of which is perpendicular to the shortest distance between the lines  $AB, DC$ , and also to that between  $AD, BC$ .

39. Three equal spheres are placed in contact on a smooth horizontal table, and a fourth equal sphere is placed upon them, and then a cone of semi-vertical angle  $\alpha$  is placed over the pile of spheres. Prove that the cone will be lifted if its weight is less than  $\frac{1}{\sqrt{2}} \tan \alpha$  of the weight of a sphere.

40. A cylindrical shell, without a bottom, stands on a horizontal plane, and two smooth spheres are placed within it, whose diameters are each less whilst their sum is greater than that of the interior surface of the shell: shew that the cylinder will not upset if the ratio of its weight to the weight of the upper sphere be greater than  $2c - a - b : c$ , where  $a, b, c$  are the radii of the spheres and cylinder.

41. Three spheres of radius  $c$  are placed on a smooth horizontal table so that their points of contact with it are at the angular points of an equilateral triangle. A fourth sphere of radius  $a$  and weight  $W$  touches the table and each of the other spheres. An elastic string of natural length  $2\pi c$  and modulus of elasticity  $\mu$  is placed symmetrically round the first three spheres. If the fourth sphere is just on the point of ascending, shew that  $2\pi c W = 27\mu (a - c)$ .

42. A uniform rod, length  $c$  and weight  $W$  is suspended from a fixed point by two equal elastic strings, the natural length of each being  $c$  and the modulus  $w$ . A particle of weight  $W$  is placed on the rod at a distance  $x$  from its middle point, and when the system is in equilibrium the rod makes an angle  $\alpha$  with the vertical. If  $\theta, \phi$  are the angles the strings make with the vertical, prove that

$$\frac{x}{c} = \frac{\sin(\theta - \phi) - 2 \cot \alpha \cdot \sin \theta \sin \phi}{\sin(\theta + \phi)} = \frac{\sin \theta - \sin \phi}{\sin \alpha},$$

and obtain another equation connecting  $\theta$  and  $\phi$ .

43. A lamina in the form of an isosceles triangle of vertical angle  $\alpha$  rests with its plane vertical and its two equal sides each in contact with a smooth peg, the pegs being in a horizontal line distant  $c$  apart: prove that the axis of the triangle is vertical or makes with it the angle  $\cos^{-1}(h \sin \alpha / 3c)$ .  $h$  is the length of the axis of the triangle.

44. Two strings of the same length have each of their ends fixed at each of two points in the same horizontal plane. A smooth sphere of radius  $r$  and weight  $W$  is supported upon them at the same distance

from each of the given points. If the plane in which either string lies makes an angle  $\alpha$  with the horizon, prove that the tension of each =  $Wa/8r \sin \alpha$ ;  $a$  being the distance between the points.

45. A smooth semi-circular tube is just filled with  $2n$  equal smooth beads that just fit the tube, and the whole is at rest in a vertical plane with the bounding diameter highest. If  $R_m$  be the pressure between the  $m$ th and  $(m+1)$ th beads from the top, then

$$R_m = W \cdot \sin \frac{m\pi}{2n} / \sin \frac{\pi}{2n},$$

where  $W$  is the weight of a bead.

Hence deduce that when the beads are diminished indefinitely in size, the pressure between any two is proportional to their depth below the top one.

46. A smooth rod passes through a smooth ring at the focus of an ellipse whose major axis is horizontal and rests with its lower end on the quadrant of the curve which is furthest removed from the focus. Shew that its length must be at least  $\frac{3}{4}a + \frac{1}{4}a \sqrt{(1+8e^2)}$ , where  $a$  is the semi-major axis and  $e$  the eccentricity.

47. A rigid bar without weight is suspended in a horizontal position by means of three equal, vertical, and slightly elastic rods to the lower ends of which are attached small rings  $A$ ,  $B$ , and  $C$  through which the bar passes. A weight is then attached to the bar at any point  $G$ . Shew that, on the assumption that the extension or compression of an elastic rod is proportional to the force applied to stretch or compress it, and provided the rods remain vertical, then the rod at  $B$  will be compressed, if  $G$  lie in the direction of the longer of the two arms  $AB$ ,  $BC$ , and be at a greater distance from  $B$  than  $\frac{AB^2 + BC^2}{AB \sim BC}$ .

48. A number  $n$  of equal smooth spheres of weight  $W$  and radius  $r$  is placed within a hollow vertical cylinder of radius  $a$ , less than  $2r$ , open at both ends and resting on a horizontal plane. Prove that the least value of the weight  $W'$  of the cylinder in order that it may not be upset by the balls is given by

$$aW' = (n-1)(a-r)W \text{ or } aW' = n(a-r)W,$$

according as  $n$  is odd or even.

49. Four equal smooth spherical balls of radius  $a$  are piled up within a hollow sphere which is the largest which can retain them in mutual contact, shew that its radius is  $a(1+2\sqrt{11})$ .



50. Four equal weights  $W$  are tied by strings to four equi-distant points of a loop of a string of length  $l$ , which is then placed symmetrically on a smooth sphere of radius  $r$ , all the weights hanging freely down; shew that in the position of equilibrium, the tension of each string is equal to

$$\frac{W}{2} \sqrt{\left\{ \left( 1 + \cos \frac{l}{2r} \right) / \cos \frac{l}{2r} \right\}} .$$

51. A quadrilateral  $ABCD$  has the sides  $DA, AB, BC$  equal and the angles  $DAB, ABC$  right angles, but  $AB$  and  $CD$  are not in the same plane. If forces acting along the four sides can be reduced to a couple, its axis will make with  $AB$  an angle

$$= \cos^{-1} \sqrt{\frac{CD^2 - AB^2}{CD^2 + 3AB^2}} .$$



## CHAPTER III.

### STATICS OF CONSTRAINED BODIES, ETC.

72. THE conditions of equilibrium which we have proved in the last Chapter apply to any rigid bodies whatsoever. If however the body considered be a *constrained* one, i.e. one that is not free to move in every way, as for instance one that can only turn about a fixed axis, we can obtain conditions of equilibrium which do not involve the forces of constraint.

73. *Prop.* If a rigid body under the action of a system of coplanar forces, have *one* point in the plane of the forces fixed, it is a necessary and sufficient condition of equilibrium that the algebraical sum of the moments about the fixed point of the forces, excluding the force of constraint, be zero.

For the force of constraint acts through the fixed point  $A$ , and therefore when there is equilibrium, the resultant of the remaining forces must act through  $A$ . But the algebraical sum of the moments of these remaining forces about any point is equal to the moment of their resultant, and therefore that about  $A$  vanishes. The condition is therefore a *necessary* one.

It is also *sufficient*. For if it hold, it can be shewn as in Art. 52 that  $A$  being a fixed point, the body is in equilibrium.

Ex. 1. A uniform rod which is 12 feet long and which weighs 17 lbs. can turn freely about a point in it, and the rod is in equilibrium when a weight of 7 lbs. is hung at one end. How far from that end is the point about which it can turn? *Ans.* 4 ft. 3 in.

Ex. 2.  $ABCD$  is a square: a force of 1 lb. acts from  $A$  to  $B$ , one of 4 lbs. from  $B$  to  $C$ , and one of 15 lbs. from  $D$  to  $C$ : if the centre of the square is fixed, find the force which, acting along  $DA$ , will maintain equilibrium. *Ans.* 10 lbs.

Ex. 3.  $ABCD$  is a square, of which the point  $A$  is fixed: a force of 2 lbs. acts along  $AB$ , one of 6 lbs. along  $AD$ , one of 10 lbs. along  $BD$ , and one of 3 lbs. along  $BC$ , find the force along  $DC$  which will maintain equilibrium. *Ans.*  $(5\sqrt{2} + 3)$  lbs.

Ex. 4. A lever  $ABC$ , with a fulcrum  $B$ , one-third of its length from  $A$ , is divided into equal parts in  $D$ ,  $E$ , and  $F$ . At  $C$ ,  $D$ , and  $F$ , forces of 12 lbs., 8 lbs., and 6 lbs. respectively act vertically downwards, and at  $E$  a force of 16 lbs. acts vertically upwards. What force applied to  $A$  will cause equilibrium? *Ans.*  $21\frac{1}{2}$  lbs.

Ex. 5. A weightless lamina in the shape of a regular hexagon  $ABCDEF$ , is suspended from the middle point of  $AB$ : shew that it will be in equilibrium with the side  $AB$  horizontal, if weights of 3 lbs., 7 lbs., 3 lbs. and 5 lbs. are hung at  $C$ ,  $D$ ,  $E$ , and  $F$  respectively.

74. *Prop.* If two points of a rigid body be fixed, so that it can only turn about the line joining them, it is a necessary and sufficient condition of equilibrium that the algebraical sum of the moments of the forces, excluding those of constraint, about the fixed line, be zero.

If there is equilibrium, the algebraical sum of the moments of *all* the forces about any line is zero, and the moment of the force of constraint at each of the fixed points about the line joining them is zero: therefore the sum of the moments of the remaining forces, excluding those of constraint, about this line, is zero. It is therefore a *necessary* condition.

It can be proved as in Art. 54 that when the algebraical sum of the moments about any line is zero, there is equilibrium provided two points in the line be fixed. The condition is therefore *sufficient*.

75. *Prop.* If one point of a rigid body be fixed, the necessary and sufficient conditions of equilibrium are, that the algebraical sum of the moments of the forces about each of three lines through the fixed point, but not in the same plane, be zero.

It can be shewn, as in the last proposition, that the conditions are *necessary*.

It can be shewn, as in Art. 55, that they are *sufficient*.

76. To obtain the forces of constraint at the fixed points in any of the cases considered in the last three propositions, we have only to apply the remaining conditions of equilibrium found in Chapter II.

77. As we shall often have to consider the case of bodies, such as rods, which are connected by means of *hinges* or *joints*, it will be well to consider what a *hinge* is. We shall consider *smooth* hinges only.

The connection may be supposed to be made in several ways. A point of one body may be connected with one of the other body by a very short *string*. Or one body may end in a very small *ball* or *pivot*, which works in a corresponding small *socket* or *ring* in the other body, so that there is contact at only one point. Or we may suppose each body to end in a small ball, which works in a corresponding socket of a small separate body. In each of these cases there is no restriction on either body, except that the two ends must be in contact; the action on each at the common point must pass through this point, but will adapt itself in magnitude and direction so as to maintain equilibrium, if possible.

If three or more bodies are connected by one joint, we may suppose the connection to be made by each having a very short string attached to it, and the strings to be knotted together. Or we may suppose each to end in a small smooth ball, which works in a corresponding socket in a small separate body.

78. In the construction of materials it is often desirable to ascertain the internal forces between one portion of a body and the adjacent portion. When all these are known, we are able to adapt the strength of each part to the force it has to sustain. For instance, if we know that the tension at one point of a chain is

always half that at another, the thickness of the chain at the former point need only be half that at the latter; a saving in material and in weight is thus effected.

We have learnt that when a body is in equilibrium, the forces exerted on any portion of it by the adjacent portions counteract the remaining forces acting on the portion in question. As, however, there is an infinite number of systems of forces, each of which counteracts a given system, we cannot as a rule determine which system is the one actually exerted, without going beyond the limits of Elementary Statics. If, for instance, a rope composed of several fibres be taut, though we may know the tension of the rope itself, i.e. the sum of the tensions of the different fibres, we cannot say how it is distributed among them. This can only be ascertained when the elasticity of each fibre is known.

When a beam is merely *stretched*, i.e. when the external forces all act *along* it, the only internal forces called into play will be between particles arranged in lines along the beam. If then the beam be supposed to consist of two parts  $A$  and  $B$ , the action of  $B$  on  $A$  will be the sum of the forces exerted by particles of  $B$  on the adjacent particles of  $A$ , all such forces being in the same direction along the beam. This action is equal to the resultant of the forces acting on the portion  $A$ , and which are also external to the beam. It is clear that the greater this action becomes, the more likely is the beam to be pulled asunder at the point of junction of  $A$  and  $B$ ; the action therefore measures the *tendency* of the beam to *break* at that point.

79. When the external forces on the beam are not all along it, the action of one portion on another is not so simple as in the above case. Take the following case. Let  $ABCD$  be a rectangular beam which is firmly fixed at the end  $AB$  in a vice; along  $DC$  let a force  $S$  be applied: it will of course be perpendicular to the beam. Consider

the equilibrium of the portion  $CDPQ$ , where  $PQ$  is an imaginary section perpendicular to the beam's length.

The forces in action are  $S$  and the innumerable forces due to  $ABQP$ , acting at every point of the section  $PQ$

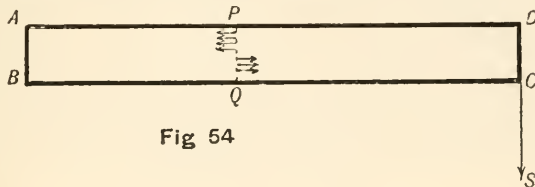


Fig 54

Let the latter be resolved along  $PQ$  and at right angles to it: the sum of the former components must be equal and opposite to  $S$ , and will with it form a couple. The components perpendicular to  $PQ$  must therefore be equivalent to a couple, equal and opposite in sign to the former. This shews that the forces near  $P$  must be in the direction  $PA$ , and those near  $Q$  in the opposite direction: and therefore that the tendency of  $S$  is to stretch the fibres near  $P$  and crush those near  $Q$ . It must follow too, that the magnitudes of the components perpendicular to  $QP$  depend on the moment of  $S$  about  $Q$ , and not on the magnitude of  $S$  simply. Hence the greater the moment of  $S$  about  $Q$  the more likely are the fibres along  $PQ$  to give way and the rod to bend at  $PQ$ .

Since  $PQ$  is supposed small compared with  $QC$ , the numerical sum of the forces along  $PQ$  must be very much greater than  $S$ , i.e. a force is far more likely to bend a rod, when applied at right angles to it, than to pull it asunder when applied along it.

Similar reasoning will apply to a beam under the action of any system of forces. We can shew that the *tendency to bend* at any point is measured by the algebraical sum of the moments about that point, of the forces external to the rod and acting on one of the parts into which the beam is divided by the point. This *tendency to bend* is also termed the *bending moment*.



Ex. 1. A light beam is supported in a horizontal position at its ends, and a weight  $w$  is hung from its middle point. Find the bending moment at a point distant  $x$  from one end. Ans.  $\frac{wx}{2}$ .

Ex. 2. If a heavy uniform rod be supported at its middle point, shew that the bending moment at any point varies as the square of its distance from the nearer end.

Ex. 3. A uniform rod  $AB$  of weight  $w$  and length  $a$  is supported in a horizontal position at  $A$  and  $B$ ; from a point distant  $x$  from  $A$  a weight  $w'$  hangs: find the bending moment at a point distant  $y$  from  $A$ .

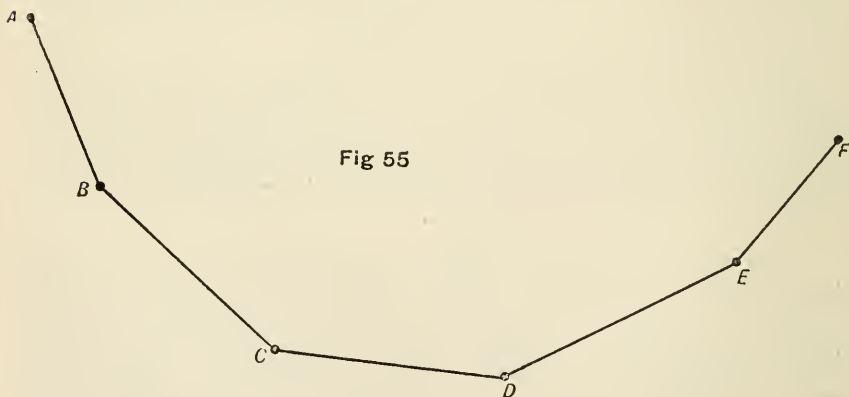
$$\text{Ans. } w \cdot \frac{y(a-y)}{2a} + w' \cdot \frac{(a-x)y}{a}, \text{ if } y \text{ is } < x.$$

$$w \cdot \frac{y(a-y)}{2a} + w' \cdot \frac{(a-y)x}{a}, \text{ if } y \text{ is } > x.$$

Ex. 4. A uniform rod of weight  $w$  and length  $a$ , can turn freely about a hinge at one end, and rests with its other end against a smooth vertical wall, distant  $b$  from the hinge. Prove that the bending moment at a point whose distances from the two ends are  $x$ ,  $y$ , respectively, is

$$\frac{w \cdot xyb}{2a^2}.$$

80. When each of the bodies forming a system in equilibrium is acted on by forces that reduce to three, the problem of finding the position of each of the bodies,



or of ascertaining the different forces, can often be easily solved by constructing a series of triangles each of which



is the *triangle of forces* corresponding to one of the bodies. For instance, let us consider the case of a number of particles of equal weight fastened at intervals along a weightless string, the ends of which are attached to fixed points. Let  $A, B, C, D$  &c. be the positions of the particles, when in equilibrium. Any particle,  $B$  for instance, is kept in equilibrium by three forces, its weight vertically downwards, and the tensions of the strings  $BA, BC$ . Draw a triangle  $obc$ , having its sides  $ba, ao, ob$  respectively parallel to the lines of action of these forces: then by the triangle

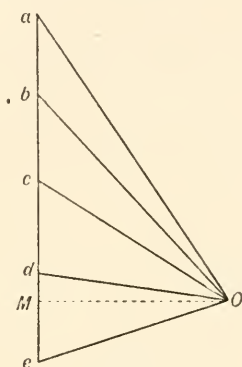


Fig 56

of forces these lines are proportional to the forces, to whose directions they are parallel: i.e. weight of  $A$  : tension of  $AB$  : tension of  $BC = ab : ao : ob$ . Produce  $ab$  downwards, and mark off  $bc, cd, de$  &c., each equal to  $ab$ ; join  $Oc, Od, Oe$  &c. Then  $Ob, bc$  represent in every way the tension of  $BC$ , on  $C$ , and the weight of  $C$  respectively, so that  $co$  must represent the tension of  $CD$ . Similarly  $do$  represents the tension of  $DE$ ,  $eo$  that of  $EF$ , and so on.

Draw  $OM$  perpendicular to  $abc$ : then the tangents of the angles that  $ao, bo, co$  &c. make with the horizon are

$$\frac{aM}{OM}, \frac{bM}{OM}, \frac{cM}{OM}, \dots, \frac{Me}{OM};$$

hence the tangents of the angles which the strings make with the horizon form an arithmetic series. Also the

horizontal resolved part of the tension of each string is represented by  $OM$ , and is therefore the same for all.

Such a figure which is drawn to enable us to solve the problem is called a *Force-Diagram*.

The above results can be obtained very easily by equating to zero the  $A.S$ 's of the resolved parts in a horizontal and vertical direction of the forces that act on each particle separately.

81. This '*Graphic*' method can be applied to prove the following important proposition.

*Prop.* If a weightless string be stretched across a smooth surface, the tension is everywhere the same.

Let  $ABCD$  &c. be the string: then any small portion

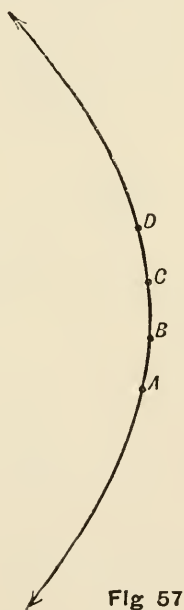


Fig 57

of it  $AB$  is kept in equilibrium by the tensions at its ends, and the resultant of the pressures of the surface on it: as the pressures along  $AB$  all act along the normals to the surface at the corresponding points, their resultant's

direction must lie somewhere between the normals at  $A$  and  $B$ .

Draw  $Oa, Ob, Oc, Od, Oe$  &c. parallel to the tensions at

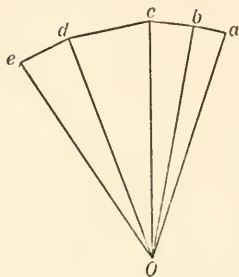


Fig 58

$A, B, C, D$  &c. respectively: and also  $ab, bc, cd,$  &c. parallel to the resultants of the pressures on  $AB, BC, CD$  &c. Then by the triangle of forces, each line represents the magnitude of the force to whose direction it is parallel. Since the resultant pressure on  $AB$  has a direction between the normals at  $A$  and  $B$ , and these ultimately, when  $AB$  is taken indefinitely small, make indefinitely small angles with one another,  $ab$  makes with the normals at  $A$  and  $B$  very small angles, i.e. makes with  $Oa, Ob$ , which are parallel to the tangents at  $A, B$ , angles ultimately equal to right angles. Hence the difference between  $Oa, Ob$  must be of the second order of small quantities, similarly those between  $Ob$  and  $Oc, Oc$  and  $Od$  &c. are of the second order, i.e.  $Oa, Ob, Oc,$  &c. and the tensions they represent, are all equal.

#### ILLUSTRATIVE EXAMPLES.

Ex. 1.  $OA, AB$  are two uniform beams loosely jointed at  $A$ , the former being moveable about a hinge at  $O$ . A string attached to  $B$  passes over a fixed smooth pulley and supports a weight  $P$ . If in the position of equilibrium the beams are equally inclined to the vertical, the string will make an angle  $\cos^{-1} \left( \frac{W + 3W'}{4P} \right)$  with the vertical, where  $W, W'$  are the weights of the beams.

Let  $\alpha$  be the inclination of either of the beams to the vertical, and  $\theta$  that of the string.

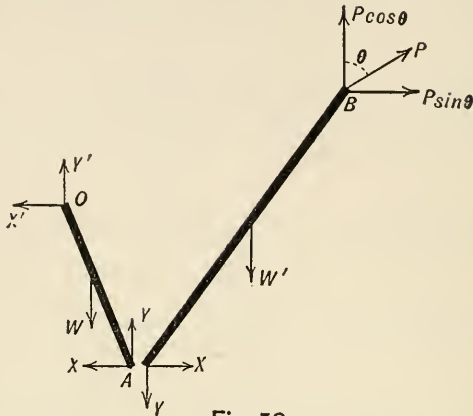


Fig 59

Resolve the tension of the string ( $P$ ) at  $B$  into two forces  $P \cos \theta$  vertically, and  $P \sin \theta$  horizontally.

Let  $2a, 2b$  be the respective lengths of  $OA, AB$ .

From the equilibrium of both rods together by taking moments about  $O$ , we have

$$W \cdot a \sin \alpha + W'' (2a \sin \alpha + b \sin \alpha) - P \cos \theta (2a \sin \alpha + 2b \sin \alpha) + P \sin \theta (2b \cos \alpha - 2a \cos \alpha) = 0 \dots (1).$$

Taking moments about  $A$  for the equilibrium of  $AB$

$$W' \cdot b \sin \alpha + P \sin \theta \cdot 2b \cos \alpha - P \cos \theta \cdot 2b \sin \alpha = 0 \dots (2).$$

Subtracting

$$W \cdot a \sin \alpha + 2W' \cdot a \sin \alpha - 2Pa \sin (\theta + \alpha) = 0,$$

or  $(W + 2W') \sin \alpha = 2P \sin (\theta + \alpha) \dots (3),$

from (2)  $W' \sin \alpha = 2P \cdot \sin (\alpha - \theta) \dots (4).$

Adding equations (3) and (4) we have

$$(W + 3W') \sin \alpha = 4P \sin \alpha \cos \theta,$$

$$\therefore \theta = \cos^{-1} \left( \frac{W + 3W'}{4P} \right).$$

If the stresses at  $O$  and  $A$  be resolved horizontally and vertically, as shewn in the figure, we can determine them as follows:

Resolving horizontally and vertically for the equilibrium of  $OA$

$$X' + X = 0 \dots\dots\dots(5).$$

$$Y' + Y - W = 0 \dots\dots\dots(6).$$

Resolving horizontally and vertically for  $AB$ ,

$$X + P \sin \theta = 0 \dots\dots\dots(7),$$

$$Y + W' - P \cos \theta = 0 \dots\dots\dots(8).$$

Equations (5), (6), (7) and (8) completely determine  $X$ ,  $Y$ ,  $X'$  and  $Y'$ .

Ex. 2. An equilateral pentagon consisting of five freely-jointed rods is hung up with one side horizontal; shew that the inclination ( $\theta$ ) of either of the upper rods to the vertical is given by the equation

$$\sin \theta + 6 \sin^2 \theta + 8 \sin^3 \theta - 8 \sin^4 \theta = \frac{1}{4}.$$

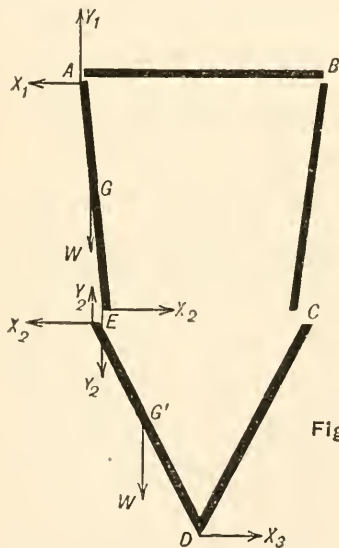


Fig. 60

Let  $AB$  be the fixed rod. Let  $\phi$  be the inclination of  $CD$  and  $DE$  to the vertical.

(The rods are drawn separate to make the figure clearer.)

Let  $W$  be the weight of each rod,  $2a$  its length.

Let the stresses on the different rods at the joints be resolved horizontally and vertically: the magnitude of these stresses are indicated in the figure. The stress at  $D$  is entirely horizontal, as the rods  $CD$ ,  $DE$  are symmetrical with respect to the vertical.

From the equilibrium of  $AE$ , resolving horizontally we have

$$X_1 = X_2 \dots \dots \dots (1).$$

Taking moments about  $A$

$$W \cdot a \sin \theta + Y_2 \cdot 2a \sin \theta - X_2 \cdot 2a \cos \theta = 0 \dots \dots \dots (2).$$

From the equilibrium of  $ED$ , resolving horizontally

$$X_2 = X_3 \dots \dots \dots (3).$$

Resolving vertically

$$Y_2 = W \dots \dots \dots (4).$$

Taking moments about  $E$

$$W \cdot a \sin \phi - X_3 \cdot 2a \cos \phi = 0 \dots \dots \dots (5).$$

Substituting from (1), (3) and (4) in (2) and (5),

$$2X_1 \cdot \cos \theta = 3W \cdot \sin \theta \dots \dots \dots (6).$$

$$W \cdot \sin \phi = 2X_1 \cos \phi \dots \dots \dots (7).$$

$$\therefore \cot \theta = 3 \cot \phi \dots \dots \dots (8).$$

Since the sum of the horizontal projections of  $AE$ ,  $ED$ ,  $DC$ ,  $CB$  is equal to  $AB$ ,

$$4a \sin \theta + 4a \sin \phi = 2a, \\ \therefore \sin \theta + \sin \phi = \frac{1}{2} \dots \dots \dots (9).$$

By eliminating  $(\phi)$  between (8) and (9) we obtained the required result.

By substituting the value of  $\theta$  just obtained in (6), we determine  $X_1$  and by resolving vertically for the equilibrium of  $AE$ , we obtain another equation which determines  $Y_1$ .

The stresses at the angular points are thus completely determined.

Ex. 3. Six equal heavy rods freely jointed at the ends form a regular hexagon  $ABCDEF$ , which when hung up by the point  $A$  is kept from altering its shape by two light rods  $BF$ ,  $CE$ . Prove that the thrusts of the rods  $BF$ ,  $CE$  are as 5 to 1, and find their magnitudes.

We shall suppose that there is a light pivot at  $B$ , to which the three rods  $AB$ ,  $BF$ , and  $BC$  are attached; and that a similar arrangement is made at  $C$ .

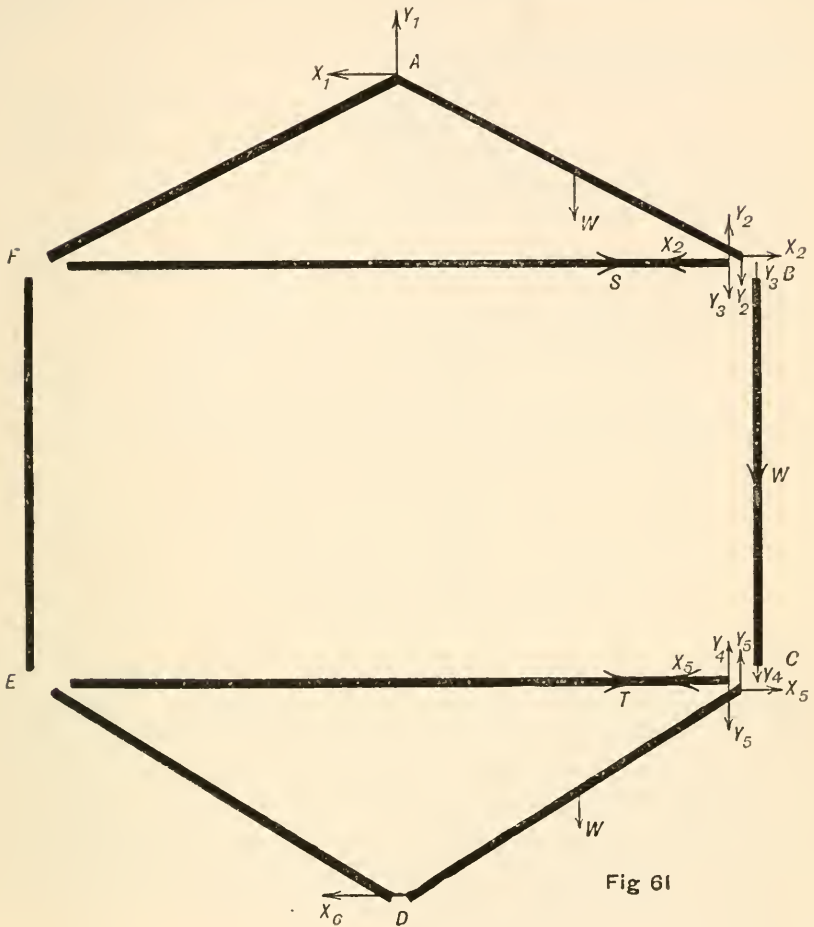
Let  $W$  be the weight of each rod,  $2a$  its length.

Since the rods  $BF$ ,  $CE$  are only acted on by the stresses at their ends, these stresses must be along the rods, i.e. horizontal, let them be  $S$  and  $T$  respectively.

Since the rod  $BC$  is acted on by its weight along its length and the stresses at  $B$  and  $C$ , these latter forces must also act along  $BC$  (Art. 61), i.e. vertically.



From symmetry the stress at *D* on *CD* is horizontal.



Let the stresses resolved horizontally and vertically at *A*, *B*, *C* and *D* be those shewn by the figure.

From the equilibrium of *AB*, by taking moments about *A*,

$$W \cdot a \cdot \frac{\sqrt{3}}{2} + Y_2 \cdot 2a \cdot \frac{\sqrt{3}}{2} - X_2 \cdot 2a \cdot \frac{1}{2} = 0 \dots \dots \dots (1).$$

From the equilibrium of the pivot *B*, resolving horizontally and vertically,

$$S = X_2 \dots \dots \dots (2).$$

and

$$Y_2 = Y_3 \dots \dots \dots (3)$$

From the equilibrium of  $BC$ ,

$$Y_3 - W - Y_4 = 0 \dots\dots\dots(4).$$

From the equilibrium of the pivot  $C$ ,

$$T = X_5 \dots\dots\dots(5).$$

$$Y_4 = Y_5 \dots\dots\dots(6).$$

From the equilibrium of  $CD$ ,

$$X_5 = X_6 \dots\dots\dots(7).$$

$$Y_5 = W \dots\dots\dots(8).$$

By taking moments about  $C$ ,

$$W \cdot a \cdot \frac{\sqrt{3}}{2} - X_6 \cdot 2a \cdot \frac{1}{2} = 0 \dots\dots\dots(9).$$

By substituting from the other equations in (1) and (9), we have

$$W \cdot \frac{\sqrt{3}}{2} + 2W \cdot \sqrt{3} - S = 0,$$

$$W \cdot \sqrt{3} - 2T = 0,$$

$$\therefore S = \frac{5W}{2} \sqrt{3} = 5T.$$

Ex. 4. A gipsy's tripod consists of three uniform straight sticks freely hinged together at one end. From this common end hangs the kettle. The other ends of the sticks rest on a smooth horizontal plane, and are prevented from slipping by a smooth circular hoop which encloses them and is fixed to the plane. Shew that there cannot be equilibrium unless the sticks be of equal length; and if the weights of the sticks be given (equal or unequal) the bending moment of each will be greatest at its middle point, will be independent of its length, and will not be increased on increasing the weight of the kettle.

Let  $OA, OB, OC$  be the three rods,  $P, Q, R$  their respective weights acting at their middle points. Let  $X, Y, Z$  be the vertical stresses at  $A, B$  and  $C$ , and  $X', Y', Z'$  the horizontal stresses.

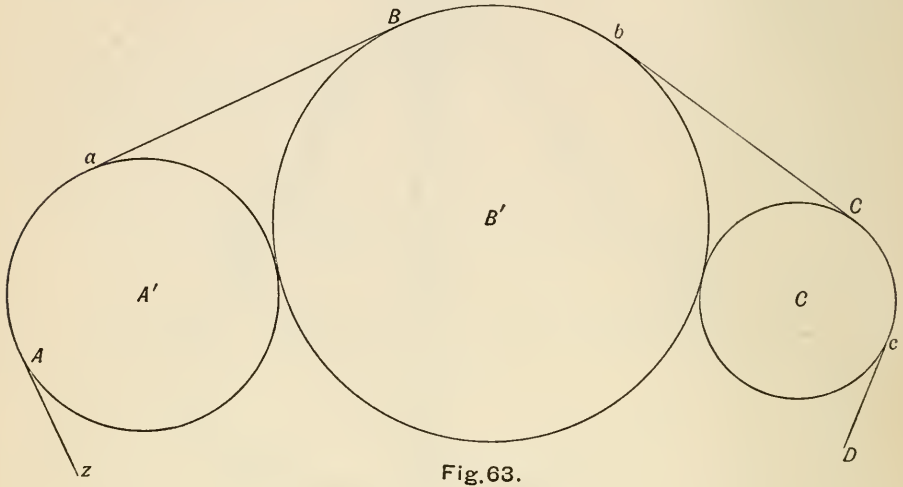
Draw  $OII$  vertically downwards.

The three forces acting on  $OA$ , viz.  $P$  and the resultant stresses at  $O$  and  $A$ , must be in one plane (Art. 61) the vertical plane containing  $OA$ , i.e.  $OAH$ .

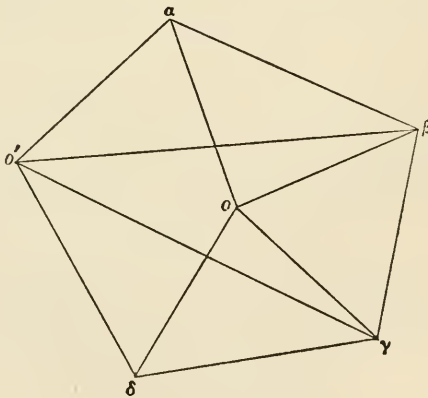
$X'$  the horizontal stress at  $A$  must therefore act along  $AH$ ; similarly  $Y'$  and  $Z'$  act along  $BH$  and  $CH$  respectively.



Ex. 5. An elastic band binds together any number of smooth right cylinders so that each cylinder touches only two others. Prove that if lines be drawn from a point parallel and proportional to the pressures between the cylinders, their extremities will lie on a circle.



Let  $Aa, Bb, Cc, \&c.$  be the portions of the band in contact with the cylinders  $A', B', C', \&c.$



From any point  $O$  draw a number of equal straight lines  $Oa, Ob, Oc, Od, \&c.$  respectively parallel to the portions of the band  $zA, aB, bC, cD, \&c.$  These lines will therefore represent the tensions along the corresponding portions of the band.

Join  $a\beta$ ,  $\beta\gamma$ ,  $\gamma\delta$ , &c.

By the triangle of forces,  $a\beta$  represents the resultant action of  $Aa$  on the cylinder  $A'$ . Similarly  $\beta\gamma$ ,  $\gamma\delta$ , &c. represent the resultant actions of the band on the cylinders  $B'$ ,  $C'$ , &c. respectively.

Through  $\beta$  draw  $\beta O'$  parallel to the normal common to  $A'$  and  $B'$ : through  $\gamma$  draw  $\gamma O'$  parallel to the normal common to  $B'$  and  $C'$ . Join  $\delta O'$ ,  $\epsilon O'$ , &c. By the triangle of forces  $O'\beta$  and  $\gamma O'$  represent the pressures of the cylinders  $A'$  and  $C'$  on  $B'$ .

Therefore  $O'\gamma$ ,  $\gamma\delta$  represent two of the forces on the cylinder  $C'$ , so that  $\delta O'$  must represent the third, which is the pressure due to  $D'$ . Similarly it can be shewn that  $O'a$ , &c. represent the pressures between the other pairs of cylinders.

Hence from  $O'$  straight lines  $O'a$ ,  $O'\beta$ ,  $O'\gamma$ , &c. have been drawn representing in magnitude and direction the pressures between the cylinders, and their extremities  $a$ ,  $\beta$ ,  $\gamma$  lie on a circle whose centre is  $O$ , since,  $Oa$ ,  $O\beta$ ,  $O\gamma$  &c. are all equal.

(The cylinders are not necessarily circular.)

### EXAMPLES.

1. Two uniform heavy rods, each of length  $a$  and jointed together by a smooth hinge, are placed symmetrically over two pegs at a given distance  $b$  apart in a horizontal line; find the position of equilibrium of the rods.

Each rod is inclined to the horizon at an angle  $\cos^{-1} (b/a)^{\frac{1}{2}}$ .

2. Three equal uniform rods,  $AB$ ,  $BC$ ,  $CD$ , of the same material and thickness, are jointed at  $B$  and  $C$ . If they are supported in a horizontal plane by smooth pegs placed under  $AB$  and  $CD$ , shew that the distance between either peg and the nearest joint is one-third the length of a rod.

3. A uniform heavy rod of length  $2b$  and weight  $W$  can turn freely about one end. To this end is attached a string of length  $l$  ( $< 2b$ ), which supports a sphere of radius  $a$  and weight  $W'$ . When the system is in equilibrium with the rod resting against the sphere, the rod makes an angle  $\theta$  with the horizontal; shew that  $\tan \theta - \tan \alpha = W'b/W'a$ , where  $l = a(\sec \alpha - 1)$ , and  $l^2 + 2al$  is  $< 4b^2$ .

4. A uniform heavy rod hangs by light inextensible strings, attached to its ends, and also to the ends of another uniform rod, which can turn about a pivot at its middle point. Prove that, when there is equilibrium, either the rods or the strings are parallel.

5. Prove that the angular points of a funicular polygon, in which the weights are equal and also the horizontal distances between them, lie on a parabola.

6. Two rods  $AC, BC$ , of equal uniform thickness are jointed at  $C$ , and the ends  $A$  and  $B$  are fixed at two points in the same vertical line. Prove that the direction of the action at the point  $C$  bisects the angle  $ACB$ : and if  $AB^2 = 4AC \cdot BC$ , shew that its magnitude is equal to a quarter of the difference of the weights of the rods.

7. A chain formed of rods of equal weight jointed together is hung up by its two ends and rests under the action of gravity. Shew that, if lines be drawn from a point representing the actions at the hinges, their ends lie on a straight line.

8. A rhombus is formed of four similar uniform rods connected by smooth hinges at their extremities, and two of these rods rest upon two smooth pegs in the same horizontal line: determine the position in which the rhombus will rest with one of its diagonals vertical.

9. Two uniform rods  $AB, AC$ , of lengths  $a, b$  respectively, are of the same material and thickness and smoothly jointed at  $A$ . A rigid weightless rod of length  $l$  is jointed at  $B$  to  $AB$  and its other end  $D$  is fastened to a smooth ring sliding on  $AC$ . The system is hung over a smooth peg at  $A$ : shew that  $AC$  makes with the vertical an angle

$$\tan^{-1} \frac{al}{b^2 + a\sqrt{(a^2 - l^2)}}.$$

10. A regular tetrahedron consists of six rigid bars without weight. It is suspended from one angular point, and from the other three equal weights  $W$  are hung: find the strain on each of the horizontal edges.

11. A beam  $AB$  of length  $a$  and weight  $w$  rests horizontally on two smooth pegs, whose distances from  $A$  and  $B$  respectively are  $a/3$  and  $a/4$ : if from  $A$  a weight  $5w$  is hung, and from  $B$   $\frac{7}{2}w$ , shew that the bending moment is greatest at the peg next  $A$ , and find its magnitude.

12. Two heavy uniform rods  $AB, BC$ , weights  $P$  and  $Q$ , are connected by a smooth joint at  $B$ . The ends  $A$  and  $C$  slide by means of small smooth rings on two fixed rods each inclined at an angle  $\alpha$  to the horizon. If  $\theta$  and  $\phi$  be inclinations of the rods  $AB, BC$  respectively to the horizon, shew that

$$\tan \theta = \frac{Q \cot \alpha}{P + Q}, \quad \tan \phi = \frac{P \cot \alpha}{P + Q}.$$



13. At what distance from the foot of an upright post must a rope of given length be attached, in order that a given force applied to the other end may produce the greatest bending moment at the foot of the post?

14. Four uniform rods  $AB, BC, CD, DA$  freely jointed at their ends so as to form a quadrilateral rest on a smooth horizontal table. They are connected together by an endless elastic string passing through small smooth rings at their middle points. Prove that in the position of equilibrium, the harmonic means of the segments into which each diagonal is divided by the other are equal.

15. A heavy uniform rod of weight  $W$  and length  $2a$  can turn freely about a hinge at one end; a ring of weight  $w$ , which slides along the rod, is connected with a point in the same horizontal plane as the hinge, by means of string whose length  $c$  is equal to the distance between the point and the hinge. Shew that in the position of equilibrium the angle  $\theta$  which the rod makes with the horizon is given by the equation

$$\cos 2\theta + \frac{Wa}{2wc} \cos \theta = 0.$$

16. Two equal uniform ladders of length  $l$ , freely jointed at  $A$ , are connected by a rope  $PG$  and rest equally inclined to it on a smooth horizontal plane; a man of weight  $W$  goes a distance  $b$  up one of the ladders: prove that the tension of the rope is  $\frac{Wb + wl}{2a} \cdot \frac{c}{\sqrt{a^2 - c^2}}$ , if  $w =$  weight of each ladder,  $2c =$  length of the rope, and  $AP = AQ = a$ .

17.  $AB, BC, CD$  are three equal rods freely jointed at  $B$  and  $C$ . The rods  $AB, CD$  rest on two pegs in the same horizontal line so that  $BC$  is horizontal. If  $\alpha$  be the inclination of  $AB$ , and  $\beta$  that of the reaction at  $B$  to the horizon, prove that  $3 \tan \alpha \cdot \tan \beta = 1$ .

18. Two equal rods can move in a vertical plane about an axis through their middle points. The lower ends of the rods are connected by a weightless elastic string, and a circle of weight  $W$  rests between the rods above the joint. The radius of the circle and the unstretched length of the string are each equal to half the length of either rod, and the rods are at right angles when the system is in equilibrium; prove that Young's modulus for the string is  $(\sqrt{2} - 1)$ .

19. Four equal uniform rods, each of weight  $W$ , are jointed so as to form a rhombus  $ABCD$ : the system rests on a horizontal plane, with  $AC$  vertical,  $B, D$  are connected by a light string: shew that its tension is  $2W \tan \frac{1}{2}BAD$ , and find the actions on the rods at  $A$  and  $C$ .

20. A triangular lamina  $ABC$  is moveable in its own plane about a point in itself: forces act on it along and proportional to  $BC$ ,  $CA$ ,  $BA$ . Prove that if these do not move the lamina the point must lie in the straight line which bisects  $BC$  and  $CA$ .

21. Five rods are jointed so as to form a regular pentagon  $ABCDE$  and are suspended from  $A$ . Two strings connect  $C$  with the middle point of  $AE$ , and  $D$  with the middle point of  $AB$ . Determine their tensions.

22. Seven equal and similar uniform rods  $AB$ ,  $BC$ ,  $CD$ ,  $DE$ ,  $EF$ ,  $FG$ ,  $GA$  are freely jointed at their extremities and rest in a vertical plane supported by rings at  $A$  and  $C$ , which are capable of sliding on a smooth horizontal rod: prove that,  $\theta$ ,  $\phi$ ,  $\psi$  being the angles which  $BA$ ,  $AG$ ,  $GF$  make with the vertical,  $\tan \theta = 4 \tan \phi = 2 \tan \psi$ .

23. Four rods jointed at their extremities form a quadrilateral, which may be inscribed in a circle: if they be kept in equilibrium by two strings joining the opposite angular points, shew that the tension of each string is inversely proportional to its length, the weights of the rods being neglected.

24. A series of particles are knotted on an endless string, forming a closed polygon, and are in equilibrium under the action of given forces applied to the particles. Shew that the tensions of the string may be represented in direction and magnitude by means of straight lines drawn from a point to the angular points of the polygon of forces.

25. Three uniform rods  $AB$ ,  $BC$ ,  $CD$ , lengths  $2c$ ,  $2b$ ,  $2c$ , rest symmetrically on a smooth parabolic arc, whose axis is vertical and vertex upwards. There are hinges at  $B$  and  $C$ , and all the rods touch the parabola. If  $W$  be the weight of either slant rod, shew that its pressure against the parabola is  $W \cdot \frac{a^2 c}{(a^2 + b^2) b}$ .  $4a = \text{lat. rec.}$

26. Four equal uniform rods are freely jointed at their extremities so as to form a square, and the middle point of one side is joined by three strings to the middle points of the other three sides.

(1) If the square be laid on a smooth table, prove that the tensions of two of the strings will be equal: and, given the magnitudes of the three tensions, find the actions at the joints.

(2) If the square be hung up by one corner, prove that the difference between two of the tensions will be four times the weight of a rod.

27. Two equal rods  $AB$ ,  $BC$ , of length  $2a$ , are connected by a free hinge at  $B$ : the ends  $A$  and  $C$  are connected by an inextensible string of length  $l$ : the system is suspended from  $A$ : prove that, in order that the angle  $AB$  makes with the verticle may be the greatest possible,  $l$  must be equal to  $4a/\sqrt{3}$ .

28. Six equal and uniform heavy rods are hinged together so as to form a hexagon: it is placed with one side on a horizontal plane and is kept in the shape of a regular hexagon by means of a string fastened to the middle points of the two sides adjacent to the base: find the tension of the string and the stresses at the hinges.

29. A parallelogram formed of four rods of uniform material and thickness, jointed at their ends, is suspended from one point, which is connected with the opposite point by a string of such a length that the figure is rectangular: prove that the tension of the string is half the weight of the four rods, and that the direction of the stress between the rods at either of the joints not connected by the string bisects the angle between them.

30. A heavy uniform rod of length  $2a$  turns freely on a pivot at a point in it, and suspended by a string of length  $l$  fastened to the ends of the rod hangs a bead of equal weight which slides on the string. Prove that the rod cannot rest in an inclined position unless the distance of the pivot from the middle point of the rod be less than  $a^2/l$ .

31. A number of equal weightless rods are freely jointed and assume the form of a regular polygon when subjected to a system of stresses at each joint, all emanating from a point on the circumscribing circle. Shew that, if from a point radii be drawn to represent in magnitude and direction the stresses in the rods, and a polygon constructed so that its sides taken in order represent the system of applied stresses, then the polygon will be equiangular and described about a parabola, and further the angular points of the polygon will all lie on a hyperbola.

32. Two equal beams  $AB$ ,  $AC$ , connected by a hinge at  $A$ , are placed in a vertical plane with their extremities  $B$ ,  $C$  resting on a horizontal plane; they are kept from falling by strings connecting  $B$  and  $C$  with the middle points of the opposite sides; shew that the ratio of the tension of each string to the weight of each beam is  $\frac{1}{3}\sqrt{(8 \cot^2 \theta + \operatorname{cosec}^2 \theta)}$ , where  $\theta$  is the inclination of either beam to the horizon.

33. A trapezium  $ABCD$  is formed of four rods joined by hinges at their extremities:  $BC, AD$  are equal, and the framework is suspended by a string attached to the middle point of  $AB$ . Determine completely the stresses at  $A$  and  $D$ . If

$$AB = AD = BC = \frac{1}{2} CD,$$

$$\text{stress at } A : \text{stress at } D = \sqrt{19} : \sqrt{7}.$$

34. A number of light rigid rods are loosely jointed together at their extremities so as to form a closed polygon, and a force applied to each side perpendicular and proportional to it, their lines of action meeting in a point; prove that, if equilibrium be maintained, the polygon will be inscribable in a circle, and if  $S$  be the point through which the forces act,  $O$  the centre of the circumscribed circle, and  $SO$  be produced to  $S'$  so that  $SS'$  is bisected in  $O$ , the stress at any angular point of the polygon will be perpendicular and proportional to the distance of the point from  $S'$ .

35.  $n$  equal uniform rods, each of weight  $W'$  and length  $l$ , are jointed so as to form symmetrical generators of a cone whose semi-vertical angle is  $\alpha$ , the joint being at the vertex of the cone.

The rods are placed with their other ends in contact with the interior of a sphere whose radius is  $r$ , so that the axis of the cone is vertical, and a weight  $W$  is hung on it at the joint. Shew that

$$\cos \alpha = \frac{\sqrt{r^2 - l^2} \cdot (nW' + 2W)}{l \sqrt{3n^2 W'^2 + 4n W' W}},$$

and find the action at the joint on each rod.

36. A fire-screen holder with any number of unequal weightless arms projects horizontally from a chimney-piece. Shew that, if the ends of the arms all lie on a circle, the axes of the couples at the hinges all pass through one point.

37. A regular octahedron is formed of 12 uniform rods jointed together at the ends. Along the three diagonals are stretched strings whose tensions are  $T_1 T_2 T_3$ . Shew that the thrusts along the rods, joining the ends of diagonals the tensions along which are  $T_1, T_2$ , are

$$\frac{1}{4} \sqrt{2} (T_1 + T_2 - T_3).$$

Prove also that, if the four diagonals of a cube be treated in a similar way, equilibrium is not possible unless the tensions are all equal.

38. Three uniform heavy rods of the same material (lengths  $2a$ ,  $2b$ ,  $2c$ , respectively) hinged together at  $B$  and  $C$  rest on a vertical circle of radius  $r$ , the whole system being in one vertical plane, and such that  $BC$  is horizontal. Find the stresses at the hinges, and prove that

$$\begin{aligned} \cot \frac{1}{2} \theta \cdot (a^2 \cos^2 \theta - c^2 \cos^2 \phi + b^2 + 2bc) \\ = \cot \frac{1}{2} \phi (c^2 \cos^2 \phi - a^2 \cos^2 \theta + b^2 + 2ab) \\ = (a + b + c)r, \end{aligned}$$

where  $\theta$  and  $\phi$  are the acute angles made with the horizon by  $AB$  and  $CD$  respectively.

39. Three equal heavy rods, in the position of the three edges of an inverted triangular pyramid, are in equilibrium with their lower ends attached to a joint about which each rod can turn freely, and their upper ends connected by strings each of length equal to half that of a rod. Prove that the tension of a string is to the weight of a rod as  $1 : \sqrt{11}$ .

40. A rhombus is formed of four rods of length  $a$ , hinged together. Two opposite rods are supported in a vertical plane by two smooth pegs which are separated by a horizontal distance  $h$  and vertical distance  $k$ . Shew that the product of the horizontal distances of either peg from the ends of the nearer unsupported rod is  $\frac{1}{4}(k^2 - 2ah + h^2)$ , and that there is no bending moment round a point in either supported rod, whose distance from its supporting peg is three times the shorter of the distances of that peg from an unsupported rod.

41. Four equal uniform rods are jointed freely together so as to form a rhombus: this is suspended by one of the angular points, and a sphere of weight equal to twice that of the rhombus is balanced inside it so as to prevent it from collapsing; shew that, if the radius of the sphere be to the length of a rod in the ratio  $5 : 8\sqrt{3}$ , the rods will, in equilibrium, make each an angle  $\pi/6$  with the vertical.

42.  $ABCD$  is a quadrilateral formed by four uniform rods of equal weight loosely jointed together. If the system be in equilibrium in a vertical plane with the rod  $AB$  supported in a horizontal position, prove that  $2 \tan \theta = \tan \alpha \sim \tan \beta$ , where  $\alpha$ ,  $\beta$  are the angles at  $A$  and  $B$ , and  $\theta$  is the inclination of  $CD$  to the horizon: also find the stresses at  $C$  and  $D$ , and prove that their directions are inclined to the horizon at the angles  $\tan^{-1} \frac{1}{2} (\tan \beta - \tan \theta)$  and  $\tan^{-1} \frac{1}{2} (\tan \alpha + \tan \theta)$  respectively.



43. Four equal rods are joined together so as to form a rhombus  $ABCD$ , lying upon a smooth horizontal plane, and elastic strings  $AC$ ,  $BD$  of the same substance are stretched along the diagonals: if  $a$  be the length of a side of the rhombus, and if the natural lengths of the strings be  $\frac{a}{2}$  and  $\frac{a}{2(1+\sqrt{2})}$ , find the angles of the rhombus when there is equilibrium.

44. Seven rods are freely jointed together to form a regular heptagon  $ABCDEFG$ . Two equal strings connect  $G$  with  $D$  and  $B$  with  $E$ , and the whole system is suspended by the point  $A$ . Find the tension of the strings.

45. Three beams  $AB$ ,  $BC$ ,  $CA$  are joined together at  $A$ ,  $B$ ,  $C$ ;  $B$  being an obtuse angle, and are placed with  $AB$  vertical, and  $A$  fixed to the ground, so as to form the framework of a crane. There is a pulley at  $C$ , and the rope is fastened to  $AB$  near  $B$ , and passes along  $BC$ , and over the pulley. If it support a weight  $W$  large in comparison with the weights of the framework and rope, find the couples which tend to break the crane at  $A$  and at  $B$ .

46. A door is moveable about its line of hinges which is inclined at an angle  $\alpha$  to the vertical; shew that the couple necessary to keep it in a position inclined at an angle  $\beta$  to its position of equilibrium is proportional to  $\sin \alpha \sin \beta$ .

47. Three equal heavy rods  $AB$ ,  $BC$ ,  $CD$  are jointed to each other at  $B$  and  $C$  and to fixed points at  $A$  and  $D$ , where  $AD$  is horizontal and equal to the length of a rod. Shew that the horizontal couple required to turn the rod  $BC$  through an angle  $\theta$  is  $BC \cdot W \cdot \sin \frac{1}{2}\theta$ , where  $W$  is the weight of each rod.

48. The lid  $ABCD$  of a cubical box, moveable about hinges at  $A$  and  $B$ , is held at a given angle to the horizon by a horizontal string connecting  $C$  with a point vertically over  $A$ : find the pressure on each hinge.



## CHAPTER IV.

### CENTRES OF MASS.

82. WE have seen (Art. 59) that the resultant of *two* parallel forces  $P$ ,  $Q$ , acting at fixed points  $A$ ,  $B$  respectively, is equal to their algebraical sum, and acts along a line parallel to the line of action of either: also that its line of action cuts  $AB$  at a fixed point, whose position depends solely on the relative magnitude of  $P$  and  $Q$  and not on their direction. So too, if we have *a number of* parallel forces acting at fixed points, their resultant is equal to their algebraical sum, and its line of action is parallel to that of any of them, and passes through a point whose position depends solely on the positions of the fixed points and the relative magnitude of the forces. For two of the forces are equivalent to their sum acting parallel to them and through a fixed point: this resultant and a third force of the system are also equivalent to the algebraical sum of the three acting parallel to them through a fixed point; in this way we can go on reducing the number of the forces until we arrive at the final resultant acting through a fixed point. We shall necessarily arrive at the same fixed point, whatever be the order in which we compound the forces: for if by compounding them in different orders we obtain two points, at either of which the resultant may act, its line of action must be the line joining the two points (Art. 53), which is inconsistent with its being always parallel to the directions of the original forces.

It is assumed above that the algebraical sum of the forces is not zero, otherwise, if they are not in equilibrium, they will not reduce to a single force, but to a couple.

83. *Def.* The *centre* of a number of *parallel forces* acting at fixed points, is the point at which their resultant always acts, however their direction alters, so long as their relative magnitudes remain the same.

If the points at which the parallel forces act lie in *one* plane, we can find an expression for the distance of the centre of the forces from any straight line in the plane.

Let  $A_1, A_2, A_3, \&c.$  be the points of application of the parallel forces,  $P_1, P_2, P_3, \&c.$ , and let  $C$  be their centre.

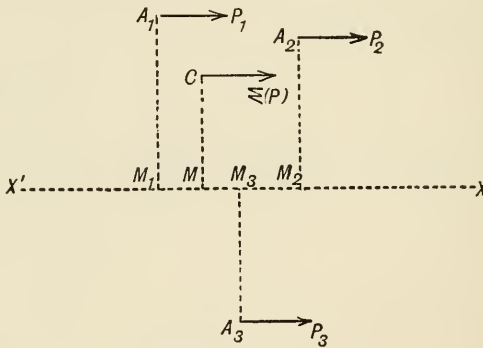


Fig. 65

Let  $X'X$  be any straight line in the plane containing the points of application. Draw  $A_1M_1, A_2M_2, \&c., CM$  perpendicular to  $X'X$ . Let  $x_1, x_2, \dots, \bar{x}$  be the lengths of these perpendiculars, which are reckoned positive or negative according to the side of the line on which the corresponding point of application lies.

As the position of  $C$  is independent of the direction of the forces, it will not be affected by supposing  $P_1, P_2, \dots$  to act parallel to  $X'X$ : since the algebraical sum of  $P_1, P_2, \&c.$  acting at  $C$ , is the resultant of these parallel forces, the algebraical sum of the moments of  $P_1, P_2, \&c.$  about

any point in  $X'X$  is equal to the moment of their algebraical sum at  $C$ , about the same point in  $X'X$ .

$$\therefore P_1x_1 + P_2x_2 + \dots = (P_1 + P_2 + \dots)\bar{x};$$

$$\therefore \bar{x} = \frac{P_1x_1 + P_2x_2 + \dots}{P_1 + P_2 + \dots} = \frac{\Sigma(Px)}{\Sigma(P)}.$$

As we can find in this way the distance of the centre of a number of parallel forces acting at fixed points in one plane, from *two* intersecting straight lines in that plane, its position is completely determined.

84\*. When the points of application of the parallel forces are not in one plane, we can find an expression for the distance of the centre from any given *plane*.

Let  $A_1, A_2, \&c.$  be the points at which the forces  $P_1, P_2, \&c.$  respectively act: let  $C$  be the centre. Draw  $A_1M_1, A_2M_2,$

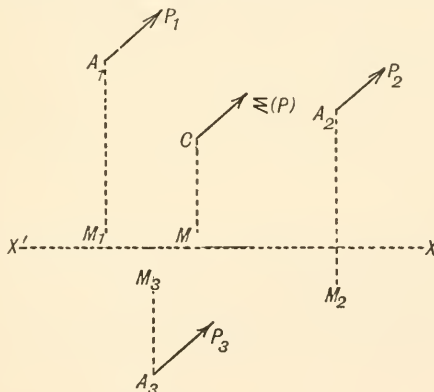


Fig. 66

$\&c.$ ,  $CM$  perpendicular to the given plane; let  $x_1, x_2 \dots \bar{x}$  be these respective distances, which are reckoned positive or negative according to which side of the plane the corresponding points lie. Let  $X'X$  be any straight line in the plane.

Since the position of  $C$  is independent of the direction of the forces, it will not be affected by supposing this

direction to be parallel to the plane and at right angles to  $X'X$ .

As the resultant of  $P_1, P_2$ , &c. is their algebraical sum acting at  $C$ , the algebraical sum of the moments of  $P_1, P_2$ , &c. about  $X'X$  is equal to the moment of their algebraical sum acting at  $C$  about  $X'X$ .

$$\therefore P_1 \cdot A_1 M_1 + P_2 \cdot A_2 M_2 + \&c. = (P_1 + P_2 + \dots) CM;$$

$$\therefore P_1 x_1 + P_2 x_2 + \&c. = (P_1 + P_2 + \dots) \bar{x};$$

$$\therefore \bar{x} = \frac{P_1 x_1 + P_2 x_2 + \dots}{P_1 + P_2 + \dots} = \frac{\Sigma(Px)}{\Sigma(P)}.$$

When we have found the distance of  $C$  from *three* planes which have only one point in common, its position is completely determined.

Ex. 1.  $O$  is the intersection of the diagonals of a square  $ABCD$ , whose side is 1 foot long: find the position of the centre of like parallel forces acting at  $A, B, C, D$  and  $O$ , respectively proportional to 4, 3, 4, 6 and 9.

Ans. In  $DB$ , distant  $5\frac{4}{3}$  inches from  $AD$ .

Ex. 2. At the angular points  $A, B, C$  of an equilateral triangle, forces of 1, 2, and 3 lbs. respectively act: find the distance of their centre from  $C$ .

Ans.  $\frac{1}{3} \sqrt{7} \cdot AB$ .

Ex. 3. At four of the angles of a regular hexagon taken in order, parallel forces proportional to 3, -2, 7 and -5 act: find the magnitude of the forces that must act at the remaining angles, in order that the centre of the six parallel forces may be the centre of the hexagon. Ans. 6, -1.

85. *Def.* Let  $A_1, A_2, A_3$ , &c. be a number of particles of masses  $m_1, m_2, m_3$ , &c. respectively; then if a point  $C_1$  be taken in  $A_1 A_2$ , so that

$$m_1 \cdot C_1 A_1 = m_2 \cdot C_1 A_2,$$

this point is called the *centre of mass* or the *centre of inertia* of the particles  $A_1$  and  $A_2$ . The centre of mass of  $A_3$  and a particle of mass  $(m_1 + m_2)$  situate at  $C_1$  is the centre of mass of  $A_1, A_2$  and  $A_3$ . That of  $A_4$  and a particle of mass  $(m_1 + m_2 + m_3)$  situate at the centre of mass of

$A_1, A_2$  and  $A_3$  is the centre of mass of  $A_1, A_2, A_3$  and  $A_4$ . Continuing this process we obtain the centre of mass of any number of particles.

From this definition of the centre of mass of a number of particles it is clear that its position is the same as that of the centre of a number of like parallel forces acting one on each of the particles, each force being proportional to the mass of the particle on which it acts. Hence if the particles of masses  $m_1, m_2 \dots$  be at distances  $x_1, x_2 \dots$  respectively from a given plane, the distance of their centre of mass from that plane is  $\Sigma(mx)/\Sigma(m)$ ; or, in other words, the distance from a given plane of the centre of mass of a number of particles is obtained by multiplying the mass of each by its distance from the plane, and dividing the algebraical sum of the products by that of the masses.

If the particles are not fixed in position, but move so that the configuration formed by them is unaltered in shape, their centre of mass will be a point moving with the configuration, but occupying a position fixed relatively to it.

*Def.* The product of a mass into the distance of its centre of mass from any plane or line is termed its *moment about that plane or line*.

We see from the above, that the algebraical sum of the moments of a number of masses about any plane, and if they are coplanar, about any line, is equal to the moment of the whole mass collected at the centre of mass about the same plane or line.

86. Let us suppose that the above system is acted on by a number of like parallel forces, one on each particle, their magnitudes being proportional to the masses of the particles on which they respectively act: now, no matter how much the direction of the forces varies, or to what extent the particles move, so long as the configuration formed by them remains the same, the resultant of these forces will always pass through the centre of mass, which is fixed re-



latively to the configuration. Since the magnitude of a particle's weight is proportional to its mass and its direction is towards the earth's centre, the weights of a system of particles which are not far from one another in comparison with their distance from the earth's centre, are forces approximately parallel, and also proportional to the masses of the particles on which they act. The line of action of their resultant then will approximately always pass through a point fixed relatively to the configuration formed by the particles, if that configuration does not alter, though it move as a whole. This point, which we have called the centre of mass of the system, is on this account often called its *centre of gravity*.

We may define the centre of gravity thus: the centre of gravity of a body is the point, fixed relatively to the body and through which the resultant of the weights of the particles composing it always acts, however the body move, provided it always moves as if it were rigid.

Strictly speaking, there is no such point of necessity for every body, because the weights of the particles composing the body are not accurately parallel, but they are so nearly so that their resultant will pass very close to the centre of mass, if it does not pass through it.

It is not assumed in the definition of the centre of gravity that the body is a rigid one: any body whatsoever, a flexible string for instance, or a mass of liquid, will have a centre of gravity corresponding to every definite shape of the body, though its position in the body will generally alter with an alteration of the body's shape.

If a body be such that the action of gravity on it can always be reduced to a single force passing through a point fixed relatively to the body, whatever be its position relatively to the earth, the body is termed a *centrobaric body*, and the point its *centre of gravity*, in a stricter sense than is usually attached to the term.

87. *Def.* When a substance is such that the mass of any volume of it is proportional to that volume, it



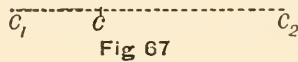
is said to be *homogeneous*, or of *uniform density*: when this is not the case, it is said to be *heterogeneous*, or of *variable density*.

When a substance is homogeneous its density is measured by the numerical measure of the mass in a unit of volume.

When the density of a substance *varies*, the *average* density of any volume is measured by the ratio of the numerical measure of its mass to that of its volume. The density *at any point* is measured by the limit of the average density of an indefinitely small volume containing the point in question.

88. *Prop.* Having given the centres of mass of a body and of one part of it, to find that of the remaining part.

Let  $m_1, m_2$  be the masses of the two parts forming the body,  $C_1, C_2$  their respective centres of mass. Join  $C_1C_2$ ,



and take  $C$  between  $C_1$  and  $C_2$  such that  $m_1 \cdot CC_1 = m_2 \cdot CC_2$ : then  $C$  is the centre of mass of the whole.

Since  $C_1, C, C_2$  are connected in this way, it is perfectly clear that if  $C_1$  and  $C$  are given,  $C_2$  is the point obtained by producing  $C_1C$  to a distance  $= (m_1/m_2) \cdot CC_1$ .

*Cor.* In a similar way we can obtain the centre of one part of a system of parallel forces when the centres of the whole system and of the remaining part are known.

89. *Prop.* If the mass of each of a series of particles be multiplied by the square of its distance from any given point, the sum of the products so obtained is equal to the sum of the products obtained by multiplying the mass of each particle by the square of its distance from the centre of mass of all the particles, together with the product of the whole mass into the square of the distance of the given point from the centre of mass.

Let  $A_1, A_2, \&c., A_n$  be  $n$  particles of mass  $m_1, m_2 \dots m_n$ ; let  $G$  be their centre of mass, and  $O$  any point whatsoever.

Join  $GO$ , and draw  $A_1M_1, A_2M_2, \&c.$  perpendicular to  $GO$ .

$$\text{Then } AO^2 = AG^2 + OG^2 - 2OG \cdot GM.$$

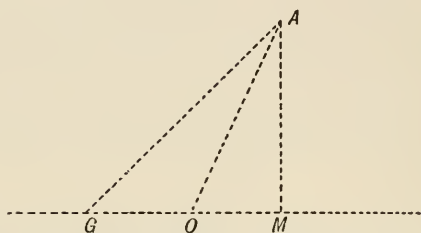


Fig 68

The  $-$  sign in this equation refers to the above figure where  $M$  and  $O$  are on the same side of  $G$ , but if we agree that  $GM$  shall be reckoned positive when  $M$  is on the same side of  $G$  as  $O$ , and negative when on the other, the equation holds for all figures.

Hence

$$\begin{aligned} \Sigma (m \cdot AO^2) &= \Sigma (m \cdot AG^2) + \Sigma (m \cdot OG^2) - 2\Sigma (m \cdot OG \cdot GM) \\ &= \Sigma (m \cdot AG^2) + OG^2 \cdot \Sigma (m) - 2OG \cdot \Sigma (m \cdot GM), \end{aligned}$$

But since  $G$  is the centre of mass of the  $n$  particles,  $\Sigma (m \cdot GM)$  is zero (Art. 85), and we have

$$\Sigma (m \cdot AO^2) = \Sigma (m \cdot AG^2) + OG^2 \cdot \Sigma (m).$$

(In the above proof, it is not assumed that  $A_1, A_2, \&c.$  are in one plane.)

*Cor.* If the mass of each of a series of particles be multiplied by the square of its distance from any given point, the product so obtained is least when the given point is the centre of mass of the system of particles.

90. We will now investigate the positions of the centres of mass of some of the simpler geometric figures.

*Prop.* If a body consists entirely of pairs of particles, such that those forming each pair are of equal mass and at equal distances from, but on opposite sides of, a certain point, that point is the centre of mass of the body.

For this point is clearly the centre of mass of each pair, and therefore of all the pairs, i.e. of the whole body.

Hence the centre of mass of a thin rod, uniform in density and sectional area, is its middle point: that of a lamina, uniform in thickness and density, and in shape, a circle, ellipse, or parallelogram, is its centre of figure. Also the centre of figure of a homogeneous sphere, ellipsoid, or parallelepiped is its centre of mass. The centres of mass of many other figures can be thus determined.

91. *Prop.* If a body consists entirely of pairs of particles, those forming each pair being of equal mass and such that the middle point of the line joining them is on a certain straight line or plane, the centre of mass of the body lies in that straight line or plane.

For this straight line or plane contains the centre of mass of every pair of particles and therefore that of the whole body.

Hence any straight line or plane which divides a homogeneous body symmetrically, contains its centre of mass. For instance the centre of mass of the volume of surface of a right circular cone, with its base at right angles to its axis, lies in the axis: that of a segment of an ellipse or parabola lies in the diameter conjugate to the chord cutting off the segment.

When we speak of the centre of mass of a surface or plane figure, we suppose the figure to be of very small uniform thickness. Similarly a line or curve is supposed to be of very small uniform sectional area.

92. To find the centre of mass of a plane triangle.

Let  $ABC$  be the triangle. Bisect  $BC$  in  $D$ , and join  $AD$ . Draw  $bdc$  parallel to  $BC$ , meeting  $AD$  in  $d$ .

Then  $bd : BD = Ad : AD = dc : DC$ ;  
 $\therefore bd = dc$ .

Similarly it may be shewn that  $AD$  bisects any other line parallel to  $BC$ . Hence the triangle consists entirely of

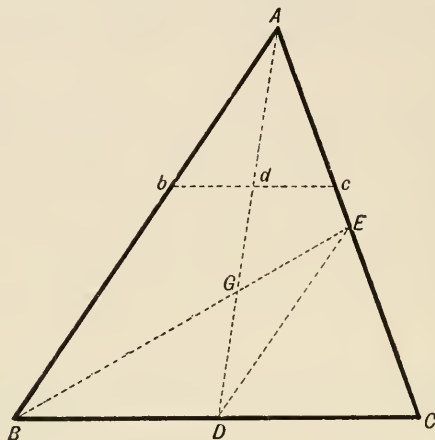


Fig 69

pairs of particles, those forming each pair being of equal mass, and such that  $AD$  bisects the line joining them: the centre of mass of the triangle is therefore in  $AD$ . (Art. 91.)

Bisect  $AC$  in  $E$ , and join  $BE$  meeting  $AD$  in  $G$ .

Then we can prove as before that the centre of mass of the triangle lies in  $BE$ , as well as in  $AD$ : it must therefore be  $G$ , their point of intersection.

Join  $DE$ : since  $D, E$  are the middle points of  $BC, AC$  respectively,  $DE$  is parallel to  $AB$ , and

$$DE = \frac{1}{2} AB;$$

$$\therefore AG : GD = AB : DE = 2 : 1;$$

$$\therefore AG = \frac{2}{3} AD.$$

Hence the centre of mass of a triangle is obtained by joining the vertex with the middle point of the base and taking the point two-thirds the way down this line from the vertex.

The centre of mass of the triangle  $ABC$  coincides with that of three equal particles placed at  $A$ ,  $B$ , and  $C$ . For the centre of mass of those at  $B$  and  $C$  is at  $D$ , half-way between them: and that of all three will be in  $AD$  at a point  $g$ , such that

$$Dg : gA = 1 : 2, \text{ or } Dg = \frac{1}{3}DA.$$

Hence  $G$  and  $g$  are the same point.

*Cor.* By drawing an indefinitely large number of lines parallel to  $BC$  and at equal distances from one another, the triangle  $ABC$  may be divided into an infinitely large number of indefinitely narrow strips, of equal breadth, and having their centres of mass in  $AD$ . Now the mass of each strip is proportional to its area, i.e. to its length, and therefore to its distance from  $A$  measured along  $AD$ : also for the purpose of finding the centre of mass of the whole we may suppose the mass of each portion collected at its centre of mass. The problem therefore of finding the centre of mass of all these strips, i.e. of the triangle, is the same as that of finding the centre of mass of an infinite number of masses arranged along  $AD$  at equal, but indefinitely small distances, each mass being proportional to its distance from  $A$ . The centre of mass in the latter case, then, is at a distance from  $A$  equal to two-thirds of  $AD$ . Hence the centre of mass of a thin rod, of uniform sectional area, but such that the density at any point varies as its distance from one end, is distant from that end two-thirds the length of the rod.

Also the centre of mass of the portion of a paraboloid of revolution, cut off by a plane perpendicular to the axis, is at a distance from the vertex equal to two-thirds the length of the axis cut off.

For let the paraboloid be divided into an indefinitely large number of thin slices of equal thickness by planes perpendicular to the axis. Then the volume of any slice is proportional ultimately to the square of its radius, i.e. to



its distance from the vertex, whence the result given above follows at once by the preceding corollary.

Ex. 1. Weights of 1, 4, 2, 3 lbs. are placed at the corners taken in order of a parallelogram  $ABCD$ ; a weight of 10 lbs. is also placed at  $O$ , the intersection of diagonals; find the position of their centre of mass.

*Ans.* If  $E$  be the middle point of  $BC$ , the point required is in  $OE$ , at a distance from  $O$  equal to one-tenth of  $OE$ .

Ex. 2. A line  $AB$  is bisected in  $C_1$ ,  $C_1B$  in  $C_2$ ,  $C_2B$  in  $C_3$ , and so on *ad infinitum*, and weights equal to  $P, \frac{P}{2}, \frac{P}{2^2}, \&c.$  are placed at the points  $C_1, C_2, C_3, \&c.$  Prove that the distance of the centre of mass of the whole system from  $B$  is equal to one-third of  $AB$ .

Ex. 3. Find the centre of mass of seven equal particles placed at the angular points of a regular octagon.

*Ans.* If  $A$  be the unoccupied angular point and  $O$  the centre of the octagon, the required point is in  $AO$  produced, at a distance from  $O$  equal to  $\frac{1}{7}AO$ .

Ex. 4. A square  $ABCD$  is divided into four equal triangles, by its diagonals, which intersect in  $O$ : if the triangle  $OAB$  be removed, find  $G$ , the centre of mass of the remaining three. Prove that if  $E$  be the middle point of  $CD$ ,  $G$  is in  $OE$ , and  $OG = \frac{1}{5}AB$ .

Ex. 5. The sides of a square  $ABCD$  are bisected, and the points of bisection of the opposite sides joined. If the small square, having the angle  $A$ , be removed, find  $G$  the centre of mass of the remaining three.

*Ans.*  $G$  is in  $AC$  and  $CG = \frac{5}{12}AC$ .

Ex. 6. Out of a circular lamina of radius  $r$  is cut a circle, whose diameter coincides with a radius of the lamina: find the position of the centre of mass of the remainder.

*Ans.* The c. m. is at a distance from the centre of the lamina equal to  $r/6$ .

Ex. 7. A figure consists of a square and an isosceles triangle, whose base is one of the sides of the square: if the side of the square be 6 inches, and the height of the triangle be 6 inches, find the centre of mass of the figure.

*Ans.* Within the square,  $\frac{4}{3}$  of an inch from the base of the triangle.



Ex. 8. A uniform rod, 18 inches long, is bent so that the two parts, 8 and 10 inches long respectively, are at right angles to one another. Find the distance between the centres of mass of the new shape and the original.

*Ans.*  $\frac{16}{9}\sqrt{2}$  inches.

Ex. 9. Equal weights are placed at  $\overline{n-2}$  of the corners of a regular  $n$ -sided polygon: find their centre of mass.

*Ans.* If  $A, B$  be the unoccupied corners,  $C$  the middle point of  $AB$ , and  $O$  the centre of the polygon, the centre of mass is in  $CO$  produced at a distance from  $O$  equal to  $\frac{2}{n-2}OA$ .

Ex. 10. Having given the position of the centre of mass of two particles  $A$  and  $B$ , and also that of  $A$  and  $C$ , find that of  $B$  and  $C$ .

*Ans.* Join  $B$  with  $E$ , the c. m. of  $A$  and  $C$ , and  $C$  with  $D$ , the c. m. of  $A$  and  $B$ ; let these two lines meet in  $G$ . The point where  $AG$  meets  $BC$  is the c. m. of  $B$  and  $C$ .

Ex. 11. Assuming that the pressure on an indefinitely small area below the surface of a liquid is perpendicular to the area and varies as the area and its depth below the surface conjointly: find where the resultant pressure on a parallelogram, one of whose sides is in the surface of the liquid, acts.

*Ans.* At a point whose depth below the surface is two-thirds that of the lowest side.

Ex. 12. With the same assumption as in the last example, shew that the resultant pressure on any plane area below the surface of a liquid is proportional to the area and the depth of its centre of mass below the surface conjointly.

Ex. 13. Find the centre of mass of a quadrilateral, two of whose sides are parallel to one another, and respectively 6 inches and 14 inches long, while the other sides are each 8 inches long.

*Ans.* In the line joining the middle points of the two parallel sides, at a distance of  $\frac{26\sqrt{3}}{15}$  inches from the longer side.

Ex. 14. Find also the centre of mass of the perimeter of the above quadrilateral.

*Ans.* In the line joining the middle points of the parallel sides, at a distance from the greater equal to  $\frac{14}{9}\sqrt{3}$  inches.

93. To find the centre of mass of a triangular pyramid.

Let  $ABCD$  be the pyramid. Bisect  $BC$  in  $E$ , join  $AE$ , and take  $H$  in it, so that

$$AH = \frac{2}{3} AE.$$

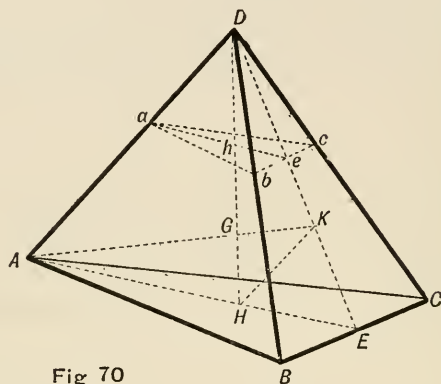


Fig 70

Let  $abc$  be a section of the pyramid, made by a plane parallel to  $ABC$ , and let  $ae$  be its intersection with the plane  $ADE$ .

Since the planes  $ABC$ ,  $abc$  are parallel,  $bc$ ,  $BC$  are also parallel;

$$\therefore be : ec = BE : EC;$$

$$\therefore be = ec,$$

and  $e$  is the middle point of  $bc$ .

Similarly  $ae$ ,  $AE$  are parallel, and

$$ah : ae = AH : AE = 2 : 3,$$

i.e.  $h$  is the centre of mass of the triangle  $abc$ .

Hence, if we suppose the pyramid divided into an infinitely large number of indefinitely thin triangular slices made by planes parallel to  $ABC$ , the centre of mass of each slice will lie in the line  $DH$ , which must therefore contain the centre of mass of the pyramid. Join  $DE$ , and take  $K$  in it so that  $DK = \frac{2}{3} DE$ ; join  $AK$  intersecting  $DH$  in  $G$ . Then, as before, we can shew that the centre of

mass of the pyramid lies in  $AK$ , as well as in  $DH$ ; the point of intersection  $G$  of these two lines must be the required centre of mass, then. Join  $HK$ .

$$AH = \frac{2}{3}AE, \text{ and } DK = \frac{2}{3}DE;$$

$\therefore HK$  is parallel to  $AD$ ,

and  $DG : GH = AD : HK = AE : HE = 3 : 1$ ,

$$\therefore DG = \frac{3}{4}DH.$$

Hence the centre of mass of the pyramid is in the line drawn from any vertex to the centre of mass of the opposite face, and is such that its distance from the former point is three times its distance from the latter.

*Cor.* The centre of mass of a triangular pyramid coincides with that of four particles of equal mass placed at its angular points.

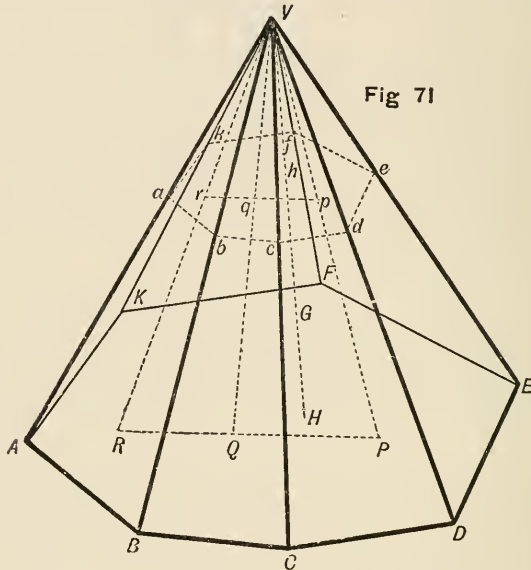
For the centre of mass of the particles at  $A$ ,  $B$  and  $C$  is  $H$ , and therefore that of the four is in  $HD$ , and at a distance from  $D$  equal to three times its distance from  $H$ ; it is therefore  $G$ , the centre of mass of the pyramid.

94. If the above pyramid be divided into an indefinitely large number of indefinitely thin slices, such as  $abc$ , of the same thickness, we may suppose the mass of each slice to be collected at its centre of mass  $h$ , which lies in  $DH$ : also the mass of any slice  $abc$  is proportional to its area, since they are of equal thickness, and therefore to the square on  $Dh$ . Hence finding the centre of mass of a triangular pyramid is the same problem as finding that of an indefinitely large number of masses arranged at equal but indefinitely small intervals along a straight line, each mass being proportional to the square of its distance from one end of the line. We infer then that the centre of mass in the latter case is at a distance from this end equal to three-quarters the length of the line. For instance, the centre of mass of a thin rod of uniform thickness, but whose density varies as the square of the distance from one end, is the point whose distance from this end is three-quarters the length of the rod.

95\*: To find the centre of mass of a pyramid having any given rectilinear plane figure for its base.

Let  $V$  be the vertex of the pyramid,  $ABCDE$  the perimeter of its base.

Let  $abcde$  be a section of the pyramid made by a plane parallel to the base. Let  $PQR$  be any straight



line in the plane of the base; join  $VP, VQ, VR$ , cutting the plane  $abcd$  in  $p, q, r$  respectively;  $p, q, r$  may be said to be the *corresponding points* to  $P, Q, R$  respectively. Since  $pqr, PQR$  are the sections of parallel planes made by the plane  $PVQ$ , they are parallel;

$$\begin{aligned} \therefore PQ : pq &= VQ : Vq = QR : qr, \\ \therefore pq : qr &= PQ : QR. \end{aligned}$$

Hence, if  $Q$  be the centre of mass of two given particles at  $P$  and  $R$ ,  $q$  will be that of particles at  $p$  and  $r$ , provided the masses of the latter particles have the same ratio to one another as those of the former have. Similarly, if we have any number of particles at different points of the base and also another set of particles at the corresponding

points of the parallel section, the mass of each particle of one set bearing a constant ratio to that of the corresponding particle of the other set, we could shew in the same way as we have done for two, that the centres of mass of the two sets are corresponding points, i.e. that they both lie in a straight line passing through the vertex. But we may suppose the two sections  $ABCD$ ,  $abcd$  to be made up each of a number of equal particles, the positions of the particles forming one set corresponding to the positions of those forming the other set. Hence, if  $H$  be the centre of mass of the base, the point  $h$ , where  $VH$  cuts the section  $abcd$ , is the centre of mass of the latter. Dividing then the pyramid up into an infinitely large number of indefinitely thin slices cut off by planes parallel to the base, we see that the centre of mass of each slice and therefore that of the whole pyramid lies in  $VH$ . But the pyramid may be divided into a number of triangular pyramids  $VHAB$ ,  $VHBC$ , &c. and the centre of mass of each of these will lie in a plane parallel to the base and at a distance from it one quarter the distance of the vertex from it. The centre of mass of the pyramid must therefore be at  $G$ , the point where this plane cuts  $VH$ ; i.e. the centre of mass is found by joining the vertex with the centre of mass of the base, and taking a point in the joining line at a distance from the former point three times its distance from the latter.

*Cor.* Since a cone or pyramid with a curvilinear base may be regarded as the limiting case of a pyramid with a rectilinear base, when the number of sides is indefinitely large, we can find the centre of mass of a cone in exactly the same way as we find that of a pyramid with a rectilinear base.

96\*. To find the centre of mass of the surface of a pyramid with a rectilinear base.

If the pyramid be the one in fig. 71, its surface may be divided into a number of triangles having the common vertex  $V$ : the centre of mass of each triangle and there-



fore that of the whole surface will lie in a plane parallel to the base and at a distance from the vertex two-thirds that of the base. Also, as in the case of the solid pyramid, the centre of mass of the surface may be shewn to lie in the line joining the vertex with the centre of mass of the perimeter of the base. Hence the point where this line meets the plane mentioned above, is the centre of mass required. The centre of mass then is in the line joining the vertex of the pyramid with the centre of mass of the perimeter of the base, and its distance from the latter point is half its distance from the former.

*Cor.* The centre of mass of the surface of a cone may be found by the same rule, as a cone is the limiting case of a pyramid, when the number of sides of the base is indefinitely increased.

97\*. To find the centre of mass of an arc of a circle.

Let  $ABC$  be the arc, subtending an angle  $2\alpha$  at the centre  $O$ .

Draw  $OB$  bisecting the angle  $AOC$ : it is clear from the principle of symmetry of Art. 91 that the centre

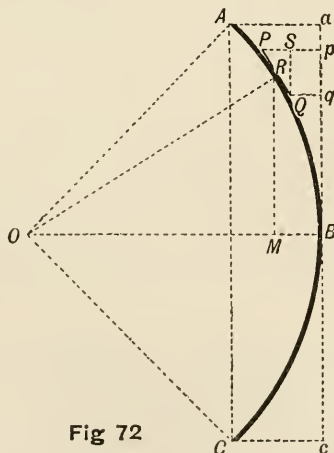


Fig 72

of mass is in  $OB$ . Construct a regular polygon circum-



scribing the arc; let  $PQ$  be one side of it, touching the circle at  $R$ . Draw  $Aa, Pp, Qq, Cc$  perpendicular to the tangent  $aBc$  at  $B$ ,  $RM$  perpendicular to  $OB$ , and  $QS$  to  $Pp$ .

The right-angled triangles  $PSQ, ORM$  are similar, since  $QS, PQ$  are respectively perpendicular to  $OM, OR$ .

$$\therefore PQ : QS = OR : OM;$$

$$\therefore PQ \cdot OM = OR \cdot QS = OB \cdot pq;$$

$$\therefore \Sigma (PQ \cdot OM) = \Sigma (OB \cdot pq) = OB \cdot \Sigma (pq);$$

$$\therefore OG \cdot \text{perimeter of polygon} = OB \cdot ac = OB \cdot \text{chord } AC$$

(Art. 85);

where  $G$  is the centre of mass of the polygon.

Also, when the sides of the polygon are taken indefinitely small, the limit of the perimeter of the polygon is that of the arc, and their centres of mass are also coincident. Hence the distance of the centre of mass of the arc  $ABC$  from  $O$  is

$$\frac{\text{radius } OB \cdot \text{chord } AC}{\text{arc } ABC} = \frac{r \sin \alpha}{\alpha}.$$

98\*. To find the centre of mass of the sector of a circle.

Let  $ABC$  be the sector: from  $O$ , the centre of the circle, draw  $OB$  bisecting the angle  $AOC$ . Then (Art. 91) the centre of mass of the sector is clearly in  $OB$ . In the arc  $ABC$  inscribe a regular polygon; let  $PQ$  be one of its sides,  $R$  the middle point of  $PQ$ : join  $OR$ , and take  $r$  in  $OR$  such that  $Or$  is equal to  $\frac{2}{3} OR$ . Then the centre of mass of the triangle  $OPQ$  is  $r$ , and the centres of mass of all such triangles are arranged at equal angular intervals along the arc of a circle of radius  $Or$ , and whose angle is  $AOC$ . But when the number of the sides of the polygon is increased indefinitely,  $Or$  becomes equal to  $\frac{2}{3} OB$  ultimately, the sum of the triangles of which  $OPQ$  is a type becomes the sector  $AOC$ , and the centre of

mass of the latter is that of an infinite number of equal masses arranged at equal angular intervals along an arc

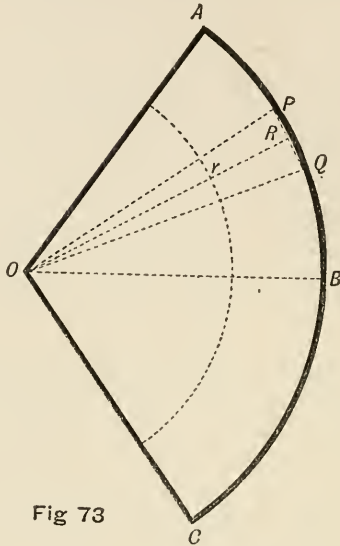


Fig 73

of a circle of radius  $\frac{2}{3}OB$ , and whose angle is equal to  $AOB$ . But the centre of mass of the masses arranged along this arc is that of the arc itself. Therefore the distance of the centre of mass of the sector from  $O$

$$= \frac{2}{3} \cdot \frac{OB \times \text{chord } AC}{\text{arc } AC}.$$

*Cor.* As the segment of a circle is the difference between a sector and a triangle, its centre of mass can be found by the method of Art. 88.

The centre of mass of the portion of a circle cut off by two parallel lines can also be obtained, since the figure consists of the difference of two segments.

99. To find the centre of mass of the belt of a sphere cut off by two parallel planes.

Let  $AB$  be the arc of a circle, which by revolving about  $OE$  generates the belt  $ABCD$  of a sphere in question. Then (Art. 91) the centre of mass of the belt lies in  $OE$ .

Let  $PQ$  be the side of a regular polygon, circumscribing the arc  $AB$ ; let  $R$  be the middle point of  $PQ$ ,

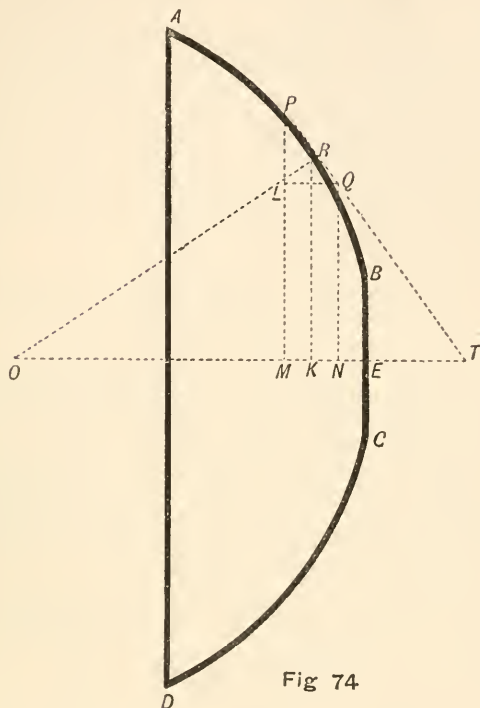


Fig 74

where it touches the circle. Produce  $PQ$  to meet  $OE$  in  $T$ , and draw  $PM$ ,  $RK$ ,  $QN$  perpendicular to  $OE$ , and  $QL$  perpendicular to  $PM$ . The area of the frustum of the cone, generated by the revolution of  $PQ$  about  $OE$

$$= PT \cdot \pi PM - QT \cdot \pi QN$$

$$= \pi \cdot (PR + RT) PM - \pi (RT - RQ) \cdot QN$$

$$= \pi \cdot RT \cdot PL + 2\pi PR \cdot RK$$

$$= 2\pi \cdot PQ \cdot RK, \text{ by similar triangles } PQL, RKT$$

$$= 2\pi OR \cdot MN \text{ by similar triangles } PQL, ORK$$

= the area of the belt cut off by the planes  $PM$ ,  $QN$  from the cylinder circumscribing the sphere and having its axis along  $OE$ .

Hence the sum of the areas of any number of frusta of cones, of which the one considered is a type, is equal to the sum of the areas of the corresponding belts of the circumscribing cylinder. But ultimately, when the number of the sides of the circumscribing polygon is taken indefinitely large, the sum of the areas of the frusta of the cones becomes the area of the belt of the sphere. Hence the area of the belt of a sphere, cut off by parallel planes, is equal to that of the coaxial circumscribing cylinder cut off by the same planes.

Let  $G$  be the centre of mass of the belt of  $ABCD$  of the sphere,  $G'$  of the corresponding belt of the cylinder. Then

$$\begin{aligned}
 OG \cdot \text{area of } ABCD &= \text{moment of } ABCD \text{ about the plane} \\
 &\quad \text{through } O \text{ perpendicular to } OE \\
 &= \Sigma (2\pi \cdot OA \cdot MN \cdot OK) \quad (\text{Art. 85}) \\
 &= \text{moment about the same plane of the belt cor-} \\
 &\quad \text{responding to } ABCD \text{ of the cylinder} \\
 &= OG' \cdot \text{area of the belt of the cylinder;} \\
 \therefore OG &= OG'.
 \end{aligned}$$

Therefore  $G, G'$  are coincident, i.e.  $G$  is in  $OE$ , half-way between the planes which cut off the belt. (Art. 90.)

100. We can easily deduce from the above the position of the centre of mass of the volume of a sector of a sphere, the figure generated by the revolution of a circular sector about one of the bounding radii.

Let  $OAC$  be the spherical sector generated by the revolution of the circular sector  $AOB$  about  $OB$ . The centre of mass is in  $OB$  (Art. 91).

Imagine the sector to be divided into an infinite number of indefinitely small pyramids having the common vertex  $O$ . The centre of mass of each of these pyramids will lie on a spherical cap  $abc$ , generated by the revolution of  $ab$ , the arc of a circle, of radius three-quarters that of

$ABC$ , and the same vertical angle  $AOB$ . Supposing the

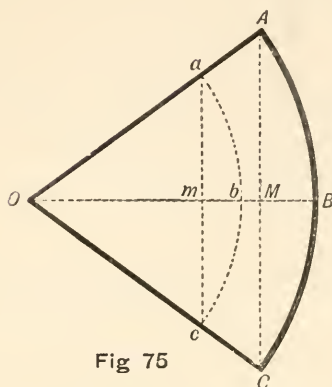


Fig 75

mass of each pyramid to be collected at its centre of mass, the centre of mass of the sector  $AOC$  is clearly the same as that of the spherical cap  $abc$ : its distance from  $O$  therefore is equal to  $\frac{1}{2}(Om + Ob)$  or  $\frac{2}{3}(OM + OB)$ . If the sector be a hemisphere,  $OM$  vanishes, and the distance from the centre of the centre of mass of the volume of the hemisphere is  $\frac{3}{8}$  of the radius.

*Cor.* As a spherical segment, the solid figure cut off a sphere by a plane, is the difference between a spherical sector and a right circular cone, its centre of mass can be found by the method of Art. 88.

The centre of mass of the solid cut off a sphere by two parallel planes can also be obtained, since the figure is the difference of two spherical segments.

Ex. 1. With the same assumption as in Ex. 11, p. 135, find where the resultant pressure acts on a triangle whose vertex is in the surface of a liquid and whose base is parallel to the surface, but below it.

*Ans.* At a point whose depth below the surface is three-quarters that of the base.

Ex. 2. Find the centre of mass of a segment of a circle.

*Ans.* It is in the diameter bisecting the segment, at a distance from the centre,  $\frac{4}{3} \cdot \frac{r \sin^3 \alpha}{2\alpha - \sin 2\alpha}$ , where  $r$  is the radius, and  $2\alpha$  the angle the segment subtends at the centre.

Ex. 3. If a figure consist of a cone and a hemisphere on the same base, find the height of the cone in order that the centre of mass of the whole may be the centre of the hemisphere.

*Ans.*  $\sqrt{3}$  times the radius of the hemisphere.

Ex. 4. Find the position of the centre of mass of a frustum of a cone, when the radii of the faces are 4 inches and 8 inches respectively, and the distance between them 7 inches.

*Ans.* In the line joining the centres of the faces at a distance of  $4\frac{1}{4}$  inches from that of the smaller face.

Ex. 5. Find also the position of the centre of mass of the surface of the above figure.

*Ans.* At a distance of  $3\frac{8}{9}$  inches from the centre of the smaller face.

Ex. 6. From a cube is cut a tetrahedron, three of whose edges are the edges of the cube which meet in one of the corners. Find the centre of mass of the remainder.

*Ans.* The c.m. is in the diagonal of the cube through that corner from which the tetrahedron is cut off, and at a distance from that corner equal to  $\frac{11}{20}$  of the diagonal.

Ex. 7. Find the centre of mass of a segment of a sphere.

*Ans.* It is in the diameter of the sphere at right angles to the base of the segment and at a distance from the centre of the sphere equal to  $\frac{3}{4} \cdot \frac{(r + h)^2}{2r + h}$ , where  $r$  is the radius of the sphere and  $h$  is the distance from the centre of the sphere of the plane cutting off the segment.

101. The centre of mass of a segment of a parabola.

Let  $BAB'$  be the segment,  $AC$  being the diameter conjugate to the base  $BB'$ .

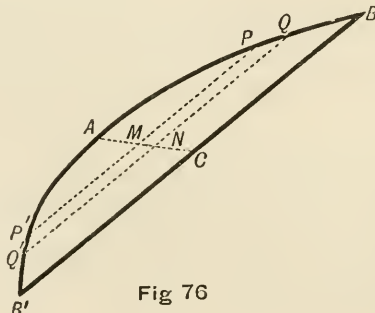


Fig 76



Divide  $AC$  into an infinite number  $n$  of indefinitely small equal parts of which  $MN$  is a typical one, the  $r$ th. Draw  $PMP'$ ,  $QMQ'$  chords parallel to  $BB'$ .

Let  $S$  be the focus; then

$$PM^2 = 4AS \cdot AM.$$

The centre of mass of the strip  $PP'Q'Q$  is in  $MN$ . (Art. 91.)

The area  $PP'Q'Q$  lies between  $PP' \cdot MN \sin BCA$ , and  $QQ' \cdot MN \cdot \sin BCA$ , and the distance of its c.m. from  $A$  lies between  $AM$  and  $AN$ ; therefore the sum of the moments of all the strips about a line through  $A$  perpendicular to  $AC$  lies between

$\Sigma(PP' \cdot MN \cdot AM \sin BCA)$ , and  $\Sigma(QQ' \cdot MN \cdot AN \cdot \sin BCA)$ ,

i. e. between  $4AS^{\frac{1}{2}} \cdot \sin BCA \cdot \Sigma(AM^{\frac{3}{2}} \cdot MN)$ ,

and  $4AS^{\frac{1}{2}} \cdot \sin BCA \cdot \Sigma(AN^{\frac{3}{2}} \cdot MN)$ .

But  $AM = \frac{r}{n} AC$ ,  $AN = \frac{r+1}{n} AC$ , and  $MN = \frac{AC}{n}$ ; therefore the moment of the mass of the parabola lies between

$$4AS^{\frac{1}{2}} \cdot AC^{\frac{5}{2}} \cdot \sin BCA \cdot \frac{1^{\frac{3}{2}} + 2^{\frac{3}{2}} + \dots (n-1)^{\frac{3}{2}}}{n^{\frac{5}{2}}},$$

and  $4AS^{\frac{1}{2}} \cdot AC^{\frac{5}{2}} \cdot \sin BCA \cdot \frac{1^{\frac{3}{2}} + 2^{\frac{3}{2}} + \dots n^{\frac{3}{2}}}{n^{\frac{5}{2}}}$ ,

i. e.,  $= \frac{4AS^{\frac{1}{2}} \cdot AC^{\frac{5}{2}} \cdot \sin BCA}{\frac{5}{2}}$ . (Appendix.)

Similarly it can be shewn that the area of the segment

$$= \frac{4AS^{\frac{1}{2}} \cdot AC^{\frac{3}{2}} \cdot \sin BCA}{\frac{3}{2}}.$$

Hence the distance of the c.m. of the parabola from  $A$

$$= \frac{8AS^{\frac{1}{2}} \cdot AC^{\frac{5}{2}} \cdot \sin BCA}{5} \div \frac{8AS^{\frac{1}{2}} \cdot AC^{\frac{3}{2}} \cdot \sin BCA}{3} = \frac{3}{5}AC.$$

Also the c.m. is in  $AC$ . (Art. 91.)

102. The centre of mass of a rod of uniform thickness, and whose density varies as the  $m$ th power of the distance from one end.

Let  $AB$  be the rod, such that the density at any point  $P$  varies as  $(AP)^m$ .



Fig 77

Divide the rod into an infinite number  $n$  of indefinitely small equal parts, of which  $PQ$  is a typical one, the  $r$ th.

The mass of  $PQ$  lies between

$$\kappa \cdot PQ \cdot AP^m \text{ and } \kappa \cdot PQ \cdot AQ^m,$$

where  $\kappa$  is a constant; therefore the moment of the whole rod about  $A$  lies between

$$\Sigma (\kappa PQ \cdot AP^m \cdot AP) \text{ and } \Sigma (\kappa PQ \cdot AQ^m \cdot AQ),$$

i.e. between

$$\kappa (AB)^{m+2} \cdot \frac{1^{m+1} + 2^{m+1} + \dots + (n-1)^{m+1}}{n^{m+2}},$$

and

$$\kappa AB^{m+2} \cdot \frac{1^{m+1} + 2^{m+1} + \dots + n^{m+1}}{n^{m+2}}.$$

$$\text{i.e.} = \frac{\kappa AB^{m+2}}{m+2}.$$

Similarly it can be shewn that the mass of the rod

$$= \frac{\kappa \cdot AB^{m+1}}{m+1}.$$

Hence the distance from  $A$  of the c.m.

$$= \frac{\kappa AB^{m+2}}{m+2} \div \frac{\kappa AB^{m+1}}{m+1} = \frac{m+1}{m+2} \cdot AB.$$

The centres of mass of a triangle, pyramid and paraboloid of revolution might have been obtained by methods similar to those employed in the last two articles.

Ex. 1. Find the c. m. of a tetrahedron  $ABCD$ , which is such that the density at all points in a plane parallel to  $BCD$  is the same and proportional to the distance of the plane from  $A$ .

*Ans.* If  $G$  is the c. m. of  $BCD$ , the required point is in  $AG$ , at a distance from  $A = \frac{4}{5} AG$ .

Ex. 2. Find the c. m. of a triangular lamina  $ABC$ , when the density at any point varies as its distance from  $BC$ .

*Ans.* The middle point of  $AD$ , where  $D$  bisects  $BC$ .

Ex. 3. Find the c. m. of a tetrahedron  $ABCD$ , when the density at any point is proportional to its distance from the face  $BCD$ .

*Ans.* In  $AG$ , at a distance from  $A$  equal to  $\frac{3}{5} \cdot AG$ , when  $G$  is the c. m. of the face  $ABC$ .

Ex. 4. The density of a conical shell standing on a plane horizontal base varies as the depth below the vertex: find the depth of the centre of mass.

*Ans.*  $\frac{3}{4}$  the height of the cone.

103. PROP. When a body or any system of bodies is in equilibrium under the action of gravity, mutual actions, and the action of one external supporting point, the centre of mass of the whole system, and the supporting point lie in a vertical line.

For considering the equilibrium of the whole system, the only external forces acting on it are, its weight acting vertically at its centre of mass and the action of the supporting point: but these two forces cannot maintain equilibrium, unless their lines of action are the same, which will not be the case, unless the centre of mass and the supporting point are in a vertical line.

104. PROP. If a rigid body be placed in contact with a smooth horizontal plane, it will be in equilibrium or not, according as the vertical line drawn through its centre of mass meets the horizontal plane within the base or not.

(N.B. By the base is meant the polygon, without re-entering angles, formed by joining the extreme points of the body in contact with the plane.)

Let  $ABCDE$  be the base,  $O$  the point where the vertical through  $G$ , the centre of mass, meets the plane.

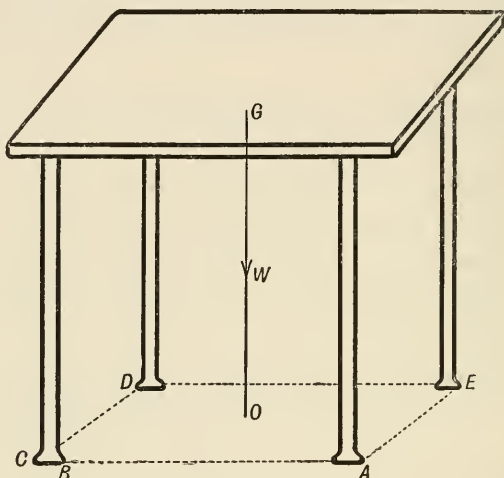


Fig 78

(i) When  $O$  lies *within* the base.

It is obvious that the direction, in which the weight of the body acting along  $GO$  tends to turn it about the side  $AB$  of the base, is such that the points  $C$ ,  $D$ ,  $E$ , &c. would move *downwards* if the plane were not there to resist such motion. As the plane is there such motion is prevented.

The same remark applies to motion about every other side of the base. Hence the weight will not produce any motion: and the resistances of the plane on the base are *passive* forces which can only resist motion and not produce it. The body is therefore in equilibrium.

(ii) When  $O$  lies *outside* the base.

In this case, the base and the point  $O$  must lie on opposite sides of one or more sides of the base.

Let  $AB$  be such a side of the base.

Now the reaction exerted by the plane on any point of the body touching it can only be vertically *upwards*,

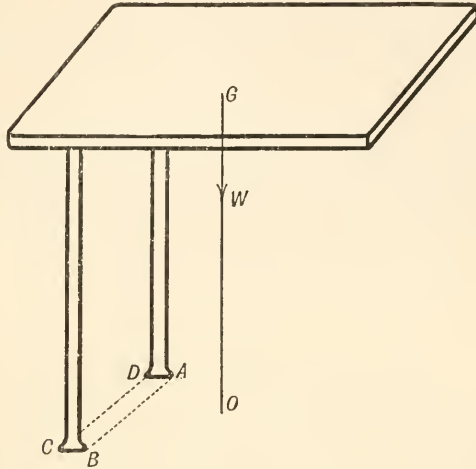


Fig 79

and its moment about  $AB$  is therefore of the same sign as that of the weight. The algebraical sum of the moments of all the forces about  $AB$  cannot therefore be zero, and equilibrium is therefore impossible.

If a curvilinear base be regarded as the limit of a polygonal one, with an infinite number of sides, the above reasoning applies to it.

In a similar way it can be shewn that a body placed on an *inclined* plane, sufficiently rough to prevent *sliding*, will be in equilibrium, provided the vertical through the centre of mass passes through the base, and that if it does not, the body will topple over.

It will be seen hereafter that these propositions are merely particular cases of more general propositions. (Art. 123.)

Ex. 1. A right-angled triangle  $ABC$ , whose sides  $AB, BC$  are respectively 5 and 6 feet long, is hung from the point  $A$ . Find the inclination of  $BC$  to the horizon.

Ans.  $\tan^{-1}(\frac{3}{5})$ .

Ex. 2. A plane triangle is hung with its plane horizontal by three vertical chains from the middle points of its edges. How heavy must it be that a 12-stone man may walk anywhere over it without tilting it?

*Ans.* 36 st.

Ex. 3. A circular table of weight 20 lbs. rests on three legs, which are on the circumference, and at the corners of an equilateral triangle. Find the greatest weight that can be placed on any part of the table without upsetting it.

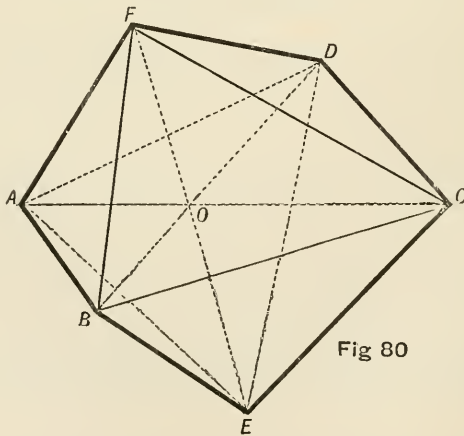
*Ans.* 20 lbs.

Ex. 4. A metal lamina, composed of a semicircle and an isosceles triangle (vertical angle  $2\alpha$ ) on the same base, is placed in a vertical plane with its curved rim resting on a horizontal plane; prove that the lamina will rest in any position, provided  $\tan \alpha = 1/\sqrt{2}$ .

ILLUSTRATIVE EXAMPLES.

Ex. 1. If the three diagonals of an octahedron intersect in a point  $O$ , the centre of inertia of the octahedron coincides with that of seven particles, one at  $O$  and one at each of the angular points: the mass of the particle at  $O$  being unity, and of that at each angular point the ratio of its distance from  $O$  to the diagonal through the point.

Let  $ABCD$  be the plane containing two diagonals  $AOC, BOD$ : let  $EOF$



be the other diagonal. Let us find the distance of the centre of inertia of the octahedron from the plane  $ABCD$ . Let  $h_1$  be the height of the





and produce it to meet  $DE$  in  $T$ .  $T$  is in  $CA$  produced. Draw two ordinates  $PP'$ ,  $QQ'$  of the ellipse indefinitely near to one another, and let them meet  $DE$  in  $M$ ,  $N$  respectively. Produce them to meet  $de$  in  $m$ ,  $n$ , and the circle in  $p$ ,  $q$  respectively.

$$PP' : pP' = CB : CA = MP' : mP';$$

$$\therefore MP : mp = CB : CA;$$

$$\therefore \text{the area } PQNM : \text{area } pqnm = CB : CA.$$

Both elliptic and circular segments may be divided up into the same infinite number of strips, of which  $PQNM$ ,  $pqnm$  are types. Let  $G$  be the c. m. of  $DPE$ , and  $g$  that of  $dpe$ .

The distance of  $G$  from  $CB$

$$\begin{aligned} &= \frac{\text{moment of } DPE \text{ about } CB}{\text{mass of } DPE} \\ &= \frac{\Sigma (PQNM \cdot CP')}{\Sigma (PQNM)} = \frac{\frac{CB}{CA} \Sigma (pqnm \cdot CP')}{\frac{CB}{CA} \Sigma (pqnm)} \\ &= \frac{\Sigma (pqnm \cdot CP')}{\Sigma (pqnm)} = \frac{\text{moment of } dpe \text{ about } CB}{\text{mass of } dpe} \\ &= \text{distance of } g \text{ from } CB. \end{aligned}$$

The distance of  $G$  from  $CA$

$$\begin{aligned} &= \frac{\Sigma \left( PQNM \cdot \frac{PP' + MP'}{2} \right)}{\Sigma (PQNM)} = \frac{\frac{CB^2}{CA^2} \cdot \Sigma \left( pqnm \cdot \frac{pP' + mP'}{2} \right)}{\frac{CB}{CA} \cdot \Sigma (pqnm)} \\ &= \frac{CB}{CA} \times \text{distance of } g \text{ from } CA. \end{aligned}$$

But the position of  $g$  is known (Art. 98), and therefore its distances from  $CA$  and  $CB$ : hence the position of  $G$  is determined.

Ex. 3. Find the centre of gravity of a spherical surface, over which the density at any point varies as the  $n^{\text{th}}$  power of the distance from a fixed point on the surface.

Let  $A$  be the fixed point on the surface:  $AOB$  the diameter through it. Divide  $AB$  into an infinite number  $m$  of equal parts, of which  $MN$  is

a typical one, the  $r^{\text{th}}$ . Let  $PP'Q'Q$  be a small belt cut off the spherical surface by planes through  $M, N$ , perpendicular to  $AB$ .

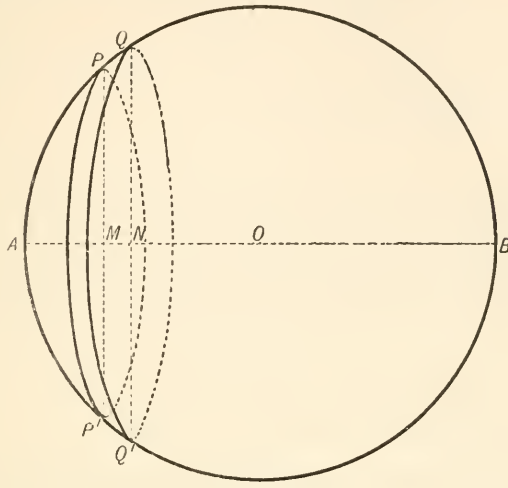


Fig 82

Area of  $PP'Q'Q = 2\pi \cdot AO \cdot MN$  (Art. 99), and mass of area  $PP'Q'Q = 2\pi AO \cdot MN \cdot \kappa AP^n$ , ultimately (where  $\kappa$  is a constant),

$$= 2\pi \cdot AO \cdot MN \cdot \kappa \cdot AB^{\frac{n}{2}} \cdot AM^{\frac{n}{2}} = \pi \kappa \cdot (AB)^{n+2} \frac{r^{\frac{n}{2}}}{m^{\frac{n}{2}+1}}.$$

$\therefore$  whole mass of the surface

$$= \pi \kappa \cdot AB^{n+2} \frac{1^{\frac{n}{2}} + 2^{\frac{n}{2}} + 3^{\frac{n}{2}} + \dots m^{\frac{n}{2}}}{m^{\frac{n}{2}+1}} = \frac{\pi \kappa \cdot AB^{n+2}}{\frac{n}{2} + 1}.$$

Also the moment of the mass of  $PP'Q'Q$  about the tangent plane at  $A$

$$= \pi \kappa \cdot AB^{n+2} \cdot \frac{r^{\frac{n}{2}}}{m^{\frac{n}{2}+1}} \cdot AM = \pi \kappa \cdot AB^{n+3} \cdot \frac{r^{\frac{n}{2}+1}}{m^{\frac{n}{2}+2}};$$

$\therefore$  the moment of the whole mass

$$\begin{aligned} &= \pi \kappa \cdot AB^{n+3} \cdot \frac{1^{\frac{n}{2}+1} + 2^{\frac{n}{2}+1} + \dots m^{\frac{n}{2}+1}}{m^{\frac{n}{2}+2}} \\ &= \pi \kappa \cdot \frac{AB^{n+3}}{\frac{n}{2} + 2}; \end{aligned}$$

∴ the distance of the centre of gravity from  $A$

$$\begin{aligned}
 &= \pi \kappa \cdot \frac{AB^{n+3}}{\frac{n}{2} + 2} \div \pi \kappa \cdot \frac{AB^{n+2}}{\frac{n}{2} + 1} \\
 &= \frac{n+2}{n+4} \cdot AB.
 \end{aligned}$$

Ex. 4. A bowl of uniform thin material in the form of a segment of a sphere is closed by a circular lid of the same material and thickness which is hinged across a diameter. If it be placed on a smooth horizontal plane with one half of the lid turned back over the other half, shew that the plane of the lid will make with the horizontal plane an angle  $\tan^{-1} \left( \frac{4}{3\pi} \tan \frac{\alpha}{2} \right)$ ;  $\alpha$  being the angle any radius of the lid subtends at the centre of the sphere of which the bowl is part.

Let  $EOC$  be the diameter about which the lid turns:  $BO$  the radius at right angles to it. Let  $O'$  be the centre of the sphere, and let  $O'O$

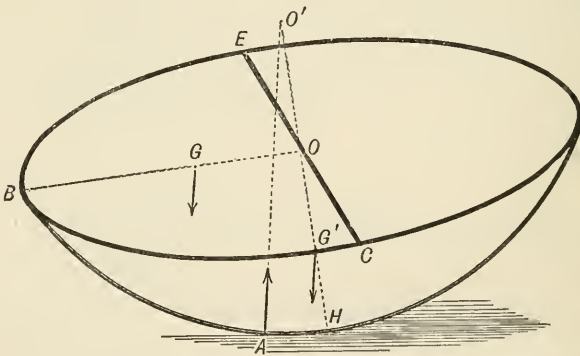


Fig. 83

meet the surface of the bowl in  $H$ . The centre of mass of the bowl is at  $G'$  in  $OH$ , such that  $OG' = G'H$ ; that of the doubled lid is at  $G$  in  $OB$ , such that  $OG = \frac{4OB}{3\pi}$ . Draw  $O'A$  vertically downwards, let  $\theta$  be the angle  $HO'A$ , which is the inclination of the lid to the horizontal.  $A$  is the point where the bowl touches the horizontal plane. Let  $r$  = the radius of the bowl. The centre of mass of the whole body must be vertically above  $A$ . (Art. 103.)



that all parts of the string except those in contact with the pulley are vertical. If the string become gradually contracted by dampness and tend to lift the cone, shew that the end of the shortest generator will remain on the table provided the diameter of the pulley be less than three times the semi-axis major of the elliptic base.

Let  $AOB$  be the major axis of the base,  $O$  the centre : let  $VA$  be the longest generator,  $VB$  the shortest. Join  $VO$ , and take  $VG = \frac{3}{4}VO$ .  $G$  is the c.m. of the cone. Let  $C$  be the middle point of  $VA$ . Draw  $CK$ ,  $GN$ ,  $VM$  perpendicular to the plane. The forces acting on the cone are its weight  $W$  vertically downwards at  $G$ , the tensions  $T, T$  of the string vertically upwards at  $V$  and  $A$ , and the reaction of the plane on the base. We may replace the tensions by  $2T$  upwards at  $C$ .

Now the motion is produced by  $2T$  and  $W$ , the resistance of the plane being a *passive* force only resists motion. It is obvious then that the cone will tend to turn about  $A$  or  $B$  according as  $C$  is to *right* or *left* of  $G$ ,

i. e. according as  $AK$  is  $>$  or  $<$   $AN$ ,

i. e.       ,,        $\frac{AM}{2}$  is  $>$  or  $<$   $AO + \frac{OM}{4}$ ,

i. e.       ,,        $\frac{AM}{2}$  is  $>$  or  $<$   $AO + \frac{AM - AO}{4}$ ,

i. e.       ,,        $AM$  is  $>$  or  $<$   $3AO$ .

### EXAMPLES.

1.  $ABC$  is a triangle,  $D, E, F$  are the middle points of its sides, shew that the centre of gravity of the perimeter of  $ABC$  coincides with the centre of the circle inscribed in  $DEF$ .

2.  $ABCD$  is any plane quadrilateral figure, and  $a, b, c, d$  are respectively the centres of gravity of the triangles  $BCD, CDA, DAB, ABC$ ; shew that the quadrilateral  $abcd$  is similar to  $ABCD$ .

3. Prove that the centre of gravity of a wedge, bounded by two similar, equal, and parallel triangular faces and three rectangular faces, coincides with that of six equal particles placed at its angular points.

4. A thin uniform wire is bent into the form of a triangle  $ABC$ , and heavy particles of weight  $P, Q, R$  are placed at the angular points: prove that if the centre of mass of the particles coincides with that of the wire

$$P : Q : R = b + c : c + a : a + b.$$



5. The perpendiculars from the angles  $A, B, C$  meet the sides of a triangle in  $P, Q, R$ : prove that the centre of gravity of six particles proportional respectively to  $\sin^2 A, \sin^2 B, \sin^2 C, \cos^2 A, \cos^2 B, \cos^2 C$ , placed at  $A, B, C, P, Q, R$ , coincides with that of the triangle  $PQR$ .

6. A plane quadrilateral  $ABCD$  is bisected by the diagonal  $AC$ , and the other diagonal divides  $AC$  into two parts in the ratio  $p : q$ ; shew that the centre of gravity of the quadrilateral lies in  $AC$  and divides it into two parts in the ratio  $2p + q : p + 2q$ .

7. A heavy elliptical ring, whose eccentricity is  $\frac{1}{3}$ , is suspended with its plane horizontal by three vertical strings, one of which is attached to the end of the minor axis, one to the end of the major axis, and one to the end of a latus rectum. Prove that the tensions respectively are  $\frac{1}{4}$ ,  $\frac{1}{3}$ , and  $\frac{5}{12}$  of the weight of the ring.

8. A triangular table is supported by three legs at the middle points of its sides. A given weight is placed upon it in any position. If weights  $P, Q, R$  placed in succession at its angular points will just upset it, prove that  $P + Q + R$  is constant.

9. A uniform wire is bent into the form of a circular arc and its two bounding radii, the arc being greater than a semicircle. Shew that if the acute angle between these bounding radii be  $\tan^{-1} \frac{4}{3}$ , the centre of gravity of the whole wire is at the centre.

10. A triangular lamina is supported at its three angular points and a weight equal to that of the triangle is placed upon it; find the position of the weight if the pressures on the points of support are proportional to  $4a + b + c, a + 4b + c, a + b + 4c$ , where  $a, b, c$  are the lengths of the sides of the triangle.

11. Particles are placed at the corners of a tetrahedron respectively proportional to the opposite faces: prove that their centre of gravity is at the centre of the sphere inscribed in the tetrahedron.

12.  $ABCD$  is a quadrilateral whose diagonals intersect in  $O$ . Parallel forces act at the middle points of  $AB, BC, CD, DA$  respectively proportional to the areas  $AOB, BOC, COD, DOA$ . Prove that the centre of parallel forces is at the fourth angular point of the parallelogram described on  $OE, OF$  as adjacent sides, where  $E, F$  are the middle points of the diagonals of the quadrilateral.

13. A solid, consisting of a hemisphere and a right circular cone on opposite sides of the same circular base, is in equilibrium, when placed with any point of the hemisphere on a horizontal plane. If the whole solid can just be included in the sphere of which the hemisphere in question is half, prove that the density of the cone is three times that of the hemisphere.

14. If three uniform rods of the same material but of different thicknesses be formed into a triangle  $ABC$ , and if their centre of gravity be at the orthocentre of this triangle, prove that their thicknesses must be proportional to

$$\cos(B - C) - 3 \cos A, \quad \cos(C - A) - 3 \cos B, \quad \cos(A - B) - 3 \cos C.$$

15. The corners of a pyramid are cut off by planes parallel to the opposite sides: if the pieces cut off be of equal weight, prove that the centre of gravity of the remainder will coincide with that of the pyramid.

16. Two uniform heavy rods,  $AB$ ,  $BC$  are rigidly united at  $B$ , the rods are then hung up by the end  $A$ ; shew that  $BC$  will be horizontal if

$$\sin C = \sqrt{2} \cdot \sin \frac{1}{2}B.$$

17. A uniform triangular lamina of weight  $W$  is suspended from a fixed point by means of strings attached to its angular points: shew that, unless its plane be vertical, the tensions of the strings are

$$\frac{W \cdot l_1}{\sqrt{\{3(l_1^2 + l_2^2 + l_3^2) - a^2 - b^2 - c^2\}}},$$

and similar expressions;  $l_1, l_2, l_3$  being the lengths of the strings, and  $a, b, c$  the sides of the triangle.

18. Find the centre of gravity of a solid sector of a sphere, in which the density at any point varies as the cube of its distance from the centre.

19. A horizontal rod, the ends of which are on two inclined planes, is in equilibrium: if  $\alpha, \beta$  be the inclinations of the planes, prove that the centre of gravity of the rod divides it into two parts in the ratio of  $\tan \alpha$  to  $\tan \beta$ .

20. Find the centre of mass of the segment of a spheroid cut off by a plane perpendicular to the axis.

21. Shew how to determine the position of the centre of gravity of the area contained between two concentric, similar, and similarly situated ellipses and two straight lines drawn from the common centre.

22. If from a triangle  $ABC$  three equal triangles  $ARQ$ ,  $BPR$ ,  $CQP$  be cut off, the centres of inertia of the triangles  $ABC$ ,  $PQR$  will be coincident.

23. From a uniform circular disc, radius  $a$ , are cut two circular holes, radii  $b$  and  $c$ , and centres at distances  $\beta$ ,  $\gamma$  from that of the disc, and distance  $\delta$  from one another. Find where to cut the hole of radius  $\sqrt{bc}$ , so that the centre of mass of the remainder may be the centre of the disc: if the distance of the centre of this hole from that of the disc be  $r$ , shew that

$$r^2 + \delta^2 = (b^2 + c^2) \left( \frac{\beta^2}{c^2} + \frac{\gamma^2}{b^2} \right).$$

24. A rectangular sheet of stiff paper, whose length is to its breadth as  $\sqrt{2}$  is to 1, lies on a horizontal table with its longer sides perpendicular to the edge and projecting over it. The corners on the table are then doubled over symmetrically so that the creases pass through the middle point of the side joining the corners and make angles of  $45^\circ$  with it. The paper is then on the point of falling over; shew that it had originally  $\frac{2.5}{4.8}$  of its length on the table.

25.  $ABC$  is a triangle;  $APD$ ,  $BPE$ ,  $CPF$  the perpendiculars from it on opposite sides. Prove that the resultant of six equal parallel forces, acting at the middle points of the sides of the triangle and of lines  $PA$ ,  $PB$ ,  $PC$ , passes through the centre of the circle which goes through all of these middle points.

26. The inscribed circle of a triangle  $ABC$  touches the sides in  $D$ ,  $E$ ,  $F$ . Prove that the centre of gravity of weights proportional to  $BC$ ,  $CA$ ,  $AB$ , placed at  $A$ ,  $B$ ,  $C$  respectively, coincides with the centre of gravity of the same weights placed at  $D$ ,  $E$ ,  $F$  respectively.

27. Find the centre of gravity of that part of the circumscribing circle of a triangle which lies outside the nine-points circle; and shew that its distance from the centre of the circumscribing circle is nine times that of the centre of gravity of the triangle.

28.  $A$ ,  $B$ ,  $C$ ,  $D$ ,  $E$ ,  $F$  are six equal particles at the angles of any plane hexagon, and  $a$ ,  $b$ ,  $c$ ,  $d$ ,  $e$ ,  $f$  are the centres of gravity respectively of  $ABC$ ,  $BCD$ ,  $CDE$ ,  $DEF$ ,  $EFA$ , and  $FAB$ . Shew that the opposite sides and angles of the hexagon  $abcdef$  are equal, and that the lines joining opposite angles pass through one point which is the centre of gravity of the particles  $A$ ,  $B$ ,  $C$ ,  $D$ ,  $E$ ,  $F$ .

29. Find the centre of mass of a solid hemisphere whose density varies inversely as the distance from the centre.

30. A circle whose diameter is equal to the latus rectum of a parabola has double contact with it. Find the position of the centre of mass of the area bounded by the two curves.

31. A triangular lamina  $ABC$  hangs at rest from the point  $A$ : if  $AB=c$ ,  $AC=b$ , and  $S$  represent the area of the lamina, prove that the tangent of the inclination of  $BC$  to the vertical is equal to  $4S/(b^2 \sim c^2)$ .

32. A smooth solid hemisphere rests with its flat base against a vertical wall and is supported by a string, one end of which is fastened to the vertex of the hemisphere and the other to a point in the wall. Prove that the inclination of the string to the vertical lies between

$$\tan^{-1}\left(\frac{5}{4}\frac{5}{8}\right) \text{ and } \cos^{-1}\left(\frac{3}{8}\right).$$

33. Find the centre of gravity of the surface of the octant of a sphere.

34. From considerations of symmetry and from the fact that the centre of gravity of the whole lies in the line joining those of any two parts, deduce the position of the centre of gravity of a circular arc.

35. If the opposite edges of a tetrahedron are equal, prove that the centre of gravity of its six edges and the centre of gravity of its four faces both coincide with the centre of gravity of its volume.

36. If  $A, B, C$  be three fixed points, and  $P$  any point on a circle whose centre is  $O$ , shew that

$$AP^2 \cdot \Delta BOC + BP^2 \cdot \Delta COA + CP^2 \cdot \Delta AOB = \text{constant}.$$

37. From an external point an enveloping cone is drawn to a sphere; prove that the centre of gravity of a uniform solid bounded by the sphere and cone is at a distance  $AN^2/4CN$  from the centre of the sphere, where  $CA$  is the radius of the sphere from the centre  $C$  drawn towards the outer point and cutting the plane of contact in  $N$ .

38. The centre of gravity of a solid hexahedron whose faces are triangles is the same as that of five equal weights placed at the corners, and of an equal negative weight placed at the point where the line forming the two trihedral angles cuts the plane of the other three angles.

39. A pack of cards is laid on a table and each projects in direction of the length of the pack beyond the one below it: if each projects as far as possible, prove that the distance between the extremities of successive cards will form a harmonical progression.

40. Prove that the sum of the squares of the sides of the triangle, formed by joining the feet of the perpendiculars, let fall from a point inside a given triangle on the sides, has its least possible value, when the point is the centre of mass of three particles, at the angles of the given triangle, whose masses are proportional to the squares of the opposite sides.

41. A uniform circular disc of weight  $nW$  has a heavy particle of weight  $W$  attached to a point on its rim. If the disc be suspended from a point  $A$  on its rim,  $B$  is the lowest point: and if suspended from  $B$ ,  $A$  is the lowest point. Shew that the angle subtended by  $AB$  at the centre is  $2 \sec^{-1} 2(n+1)$ .

42. A thin shell is bounded by two similar surfaces; any closed curve being drawn on the surface, prove that the centre of inertia of the included portion of the shell, and the centre of inertia of the solid formed by drawing lines to the boundary from the centre of similitude, are in a line with the centre of similitude and at distances from it which are in the ratio 4 : 3.

43. A frustum is cut from a right cone by a plane bisecting the axis and parallel to the base. Shew that it will rest with its slant side on a horizontal table if the height of the cone bear to the diameter of the base a greater ratio than  $\sqrt{7} : \sqrt{17}$ .

44. Four weights are placed at four fixed points in space, the sum of two of the weights being given and also the sum of the other two; prove that their centre of mass lies on a fixed plane, and within a certain parallelogram in that plane.

45. A sphere, radius ( $r$ ), rests on three points at equal distances ( $a$ ) on a horizontal plane. If one of those points be depressed so that the plane containing the three points is inclined at an angle ( $\theta$ ) to the horizon, the sphere will roll off if  $\theta$  exceed  $\sin^{-1}(a/r\sqrt{3})$ , but if the point be raised the sphere will roll off if  $\theta$  exceed  $\sin^{-1}\{a/\sqrt{3(4r^2 - a^2)}\}$ .

46. A hemispherical bowl of radius  $r$  rests on a smooth horizontal table, and partly inside it rests a rod of length  $2l$ , of weight equal that of the bowl. Shew that the position of equilibrium is given by

$$l \sin(\alpha + \beta) = r \sin \alpha = -2r \cos(\alpha + 2\beta),$$



where  $\alpha$  is the inclination of the base of the hemisphere to the horizon, and  $2\beta$  is the angle subtended at the centre by the part of the rod within the bowl.

47. Two equal segments are cut from a hollow sphere, and are hung up from a point by two equal strings attached to their rims, so that their convexities are outwards. Prove that, if the lengths of the strings be equal to the diameter of either rim, they are inclined to each other at an angle  $= 2 \tan^{-1} \left( \frac{1}{3} \tan \frac{1}{2} \alpha \right)$ , where  $2\alpha$  is the angle subtended by either segment at the centre of the sphere.

48. A cone of vertical angle  $2\alpha$  is supported by a string passing over two smooth pullies in the same horizontal line, the string being attached to the vertex and to a point in the circumference of the base. Prove that in the position of equilibrium  $\sin(\alpha + \theta + \phi) = \frac{3}{2} \cos \alpha \sin \theta \cos \phi$ , where  $\theta$  is the inclination of either portion of the string to the horizon, and  $\phi$  is the angle the base of the cone makes with the vertical.

49. The top of a right cone, semi-vertical angle  $\alpha$ , cut off by a plane making an angle  $\beta$  with the axis, is placed on a perfectly rough inclined plane with the major axis of the base along a line of greatest slope of the plane; in this position the cone is on the point of toppling over: prove that the tangent of the inclination of the plane to the horizon has one of the values

$$\frac{4 \sin 2\alpha \pm \sin 2\beta}{\cos 2\alpha - \cos 2\beta}.$$

50. A ring is made up of three arcs,  $BC$ ,  $CA$ ,  $AB$ , of uniform section, but of different metals: uniform rods  $OA$ ,  $OB$ ,  $OC$ , made of the same metals as  $BC$ ,  $CA$ ,  $AB$  respectively, but with sectional area double that of the arcs, connect the points  $A$ ,  $B$ ,  $C$  with the centre  $O$ . Find the angles  $\alpha$ ,  $\beta$ ,  $\gamma$  which  $BC$ ,  $CA$ ,  $AB$  subtend at  $O$ , in order that the centre of gravity of the whole may be at  $O$ , and shew that, if  $\omega_1$ ,  $\omega_2$ ,  $\omega_3$  be the weights per unit length of  $BC$ ,  $CA$ , and  $AB$  respectively,

$$(\omega_1 - \omega_2) \tan \frac{\alpha}{2} \tan \frac{\beta}{2} + (\omega_2 - \omega_3) \tan \frac{\beta}{2} \tan \frac{\gamma}{2} + (\omega_3 - \omega_1) \tan \frac{\gamma}{2} \tan \frac{\alpha}{2} = 0.$$



## CHAPTER V.

### FRICTION.

105. WE have hitherto supposed, that the action exerted by one surface in contact with another is necessarily *along* the common normal at the point of contact, in other words that the surfaces are *perfectly smooth*. We have however no experience of bodies except such as do, in certain cases, exert on other bodies forces *inclined* to the common normal at the point of contact, in other words all bodies we are acquainted with are more or less *rough*.

Suppose the following experiment to be made. Take a mass of some material having a plane surface, and fix it so that this surface is horizontal: on it place a portion of some solid material. Now it will be found that, whatever be the materials used, and however highly their surfaces in contact may be polished and lubricated, it is always possible to turn the horizontal surface through a finite angle without the upper body *slipping*, though it may *topple over*.

Let  $W$  be the weight of the upper body,  $\alpha$  the inclination to the horizon of the plane on which it rests: then

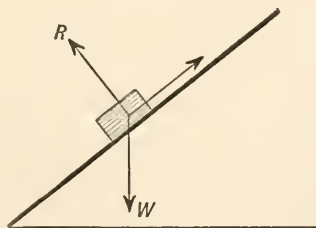


Fig.85

resolving  $W$  into  $W \cos \alpha$  perpendicular to the plane and  $W \sin \alpha$  along the plane, we infer that as  $W$  is counteracted by the action of the plane on the body, this action must consist of two components  $R (= W \cos \alpha)$  along the common normal, and  $F (= W \sin \alpha)$  along the plane. The latter force is called the *friction*. We see also that  $F/R = \tan \alpha$ . When the body is just about to slide the friction exerted is said to be the *limiting* friction.

106. The laws relating to statical friction are :

(i) *Friction always acts in the direction opposite to that, in which the point of the surface acted upon, would move, relatively to the other surface, if there were no friction.*

(ii) *The magnitude is always the least possible required for preserving equilibrium, provided this amount does not exceed the limiting friction.*

These laws are *axiomatic* and are particular cases of the general axiom that a *Passive force, being entirely due to the tendency to motion caused by Active forces, only resists such tendency: its direction therefore is always directly opposite to the motion resisted and its magnitude never exceeds the minimum required for preserving equilibrium, and is if possible equal to this minimum.*

107. Let us now make another experiment. As before take a plane surface of some material or other, and on it place blocks of different weights, shapes and sizes, but all made of the same material. If now the plane be gradually inclined in *any* direction more and more to the horizon, it will be found that each and every block, no matter what face it has in contact with the plane, begins to slide as soon as a certain inclination of the plane to the horizon is exceeded, but not before; also, that when it does slide, the increase per second in its velocity is constant. This angle though constant for the same pair of materials varies considerably for different pairs. Any block may topple over before the others slide.

Let us see what inferences can be drawn from this experiment.

Let  $\alpha$  be the inclination of the plane to the horizon, when all the blocks are just about to slide: the friction exerted is in each case limiting, and since  $F/R = \tan \alpha$ , (Art. 105), the ratio of the limiting friction to the normal pressure is the same for all the blocks. Also since the weights and therefore the normal pressures differ, this ratio is independent of the normal pressure. Since  $\alpha$  is the same whatever face of a block rests on the plane, the ratio  $F:R$  is independent of the area of the surfaces in contact. Since the increase per second in the velocity of a block is constant, the force on it is constant, i.e. the friction is independent of the velocity.

The above experiment confirms the so-called Laws of *limiting* and *dynamical* friction.

These laws are

(i) *So long as the substances in contact are unaltered, the ratio of the limiting or dynamical friction to the normal pressure is independent of the magnitude of the latter.*

(ii) *So long as the substances in contact are unaltered, the friction is independent of the area of the surfaces in contact.*

(iii) *When motion takes place, the dynamical friction is independent of the relative velocity of the points in contact.*

108. These laws must not be regarded as rigorously true in all circumstances, but only as more or less approximate expressions of the results obtained from the experiments of Coulomb and Morin, who enunciated them. More recent investigations would seem to shew, that in certain circumstances they are very far indeed from expressing the amount of friction exerted.

According to a report, read before the Institution of Mechanical Engineers by Captain Douglas Galton, on experiments made by him on the application of brakes to locomotive-wheels, the friction diminishes as the velocity increases beyond a certain limit, and is also less after it has been exerted for some time than when first applied. In the experiments of

Morin and Galton the surfaces in contact were not lubricated in any way. Before the same Institution in 1883, Mr Beauchamp Tower read a report on some experiments made by himself on a thoroughly lubricated journal revolving in bearings. These experiments shewed that in certain circumstances the friction per square inch was nearly independent of the normal pressure and that it increased with the velocity of revolution. A rise in temperature was accompanied by a reduction in the friction, though this might be caused by the lubricant becoming more efficient. Professor Thurston states that from his own experiments, he inferred that the friction at first diminished as the velocity increased and then increased again.

As however we are only concerned with statical friction we may take laws (i) and (ii) as giving fairly accurately the friction in the cases which we shall have to consider.

109. *Def.* The ratio of the limiting friction to the normal pressure, which ratio we see by laws (i) and (ii) is constant, is called the *coefficient of friction* for the pair of materials in contact. The angle the total action makes with the common normal at the point of contact is termed the *angle of friction*, provided the limiting friction is exerted.

Hence (Art. 105) the coefficient of friction is equal to the tangent of the angle of friction.

The *coefficient of dynamical friction* is the ratio of the friction to the normal pressure when motion is actually taking place. It is found by experiment to be less than the corresponding coefficient of statical friction, in other words, there is more resistance when motion is just about to take place than when it is actually taking place.

Ex. 1. If the smallest force which will move a given block weighing 3 lbs. along a given horizontal plane be  $\sqrt{3}$  lbs.; find the greatest angle at which the plane may be inclined to the horizon without the block sliding. *Ans.*  $30^\circ$ .

Ex. 2. If a weight of 14 lbs., when placed on a rough plane inclined at an angle of  $60^\circ$  to the horizon, slides down, unless a force of at least 7 lbs. acts on it up the plane, what is the coefficient of friction? *Ans.*  $\cdot 73$ .

Ex. 3. If a weight of 4 lbs. is just on the point of slipping down a rough plane, inclined at an angle of  $45^\circ$  to the horizon, when a force of 2 lbs. acts up the plane, find the least force which will move the weight up the plane, when the inclination is  $30^\circ$  to the horizon. *Ans.* 3·01 lbs.

Ex. 4. Weights of 4 and 5 lbs. respectively, connected by a light rigid rod, are placed on a rough inclined plane, with the rod parallel to a line of greatest slope. If the coefficient of friction between the 4 lb. weight and the plane be  $\cdot 6$  and that between the other weight and the plane  $\cdot 42$ , find the greatest inclination of the plane to the horizon, consistent with equilibrium. *Ans.*  $\tan^{-1} \cdot 5$ .

Ex. 5. Find the greatest angle at which a plane may be inclined to the horizon so that three equal weights whose coefficients of friction are  $\cdot 5$ ,  $\cdot 6$ ,  $\cdot 7$ , respectively, may when connected by strings rest on it without sliding. The weights are supposed placed along a line of greatest slope so that each is rougher than the one next below it. *Ans.*  $\tan^{-1} (\cdot 6)$ .

Ex. 6. A uniform ladder rests in limiting equilibrium, with its lower end in contact with a rough horizontal plane and its upper end with a smooth vertical wall. If  $\lambda$  be the angle of friction and  $\alpha$  the angle the ladder makes with the vertical, prove that  $\tan \alpha = 2 \tan \lambda$ .

Ex. 7. If everything is as in Ex. 6, except that the wall is as rough as the ground, prove that  $\alpha = 2\lambda$ .

Ex. 8. Two particles of equal weight and connected by a light string rest in limiting equilibrium on the arc of a rough vertical circle; prove that the angle the line joining them makes with the horizontal is equal to the angle of friction.

Ex. 9. A body is resting on a rough inclined plane of inclination  $\alpha$ , the angle of friction being  $\phi$  which is greater than  $\alpha$ . Shew that the ratio of the least force which will drag the body up the plane to the least force which will drag it down is  $\sin (\phi + \alpha) : \sin (\phi - \alpha)$ .

Ex. 10. One end of a uniform rod is on a rough inclined plane to which the rod is perpendicular: at the other end is applied a force parallel to the plane: if the rod be in equilibrium, prove that the coefficient of friction cannot be less than half the tangent of the plane's inclination.

110. *Def.* Let a cone be described, having its vertex at the point of contact of the two surfaces, the common



normal for axis, and the angle of friction as semi-vertical angle. This cone is called the *Cone of Friction*.

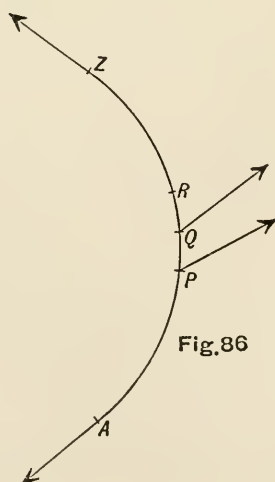
The Laws of statical friction, given in Arts. 106, 7, are all included in the following statement. *If all the other forces, external and internal, acting on the point of contact be compounded into a single resultant  $R$ , the action of the surface in contact will be equal and opposite to  $R$ , whatever be the latter's magnitude or direction, provided its line of action does not lie without the cone of friction.*

Hence a body in contact with rough surfaces will be in equilibrium, provided that to insure its being so, it is not necessary to assume that the total action at any point of contact lies outside the corresponding cone of friction.

It should be noticed that the cone of friction is always drawn so that its concavity is *towards* the body, the action on which we are considering.

111.\* To find the relation between the tensions at the ends of a light string stretched over a rough surface, and on the point of slipping.

Let  $APQRZ$  be the string, which is on the point of slipping from  $Z$  to  $A$ .



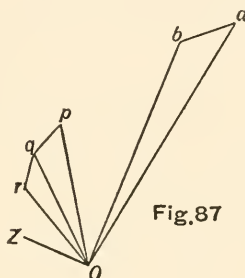


Let  $\lambda$  be the angle of friction,  $\mu$  the coefficient of friction.

Let the points  $A, B, \dots P, Q, R, \dots Y, Z$  be taken on the string so that the ultimately indefinitely small angles between the tangents at consecutive points are each equal to  $\theta$ .

Let us consider a small portion,  $PQ$ , of the string. It is kept in equilibrium by the tensions at  $P$  and  $Q$  and the resultant action of the surface.

As in Art. 81, construct a force-diagram  $Oab \dots pqr \dots yz$ , such that  $Oa, Ob, \dots Op, Oq, Or, \dots Oy, Oz$  represent the



tensions at  $A, B, \dots P, Q, R, \dots Y, Z$  respectively. Join  $ab, bc, \dots pq, qr, \dots yz$ . These last will represent the resultant actions of the surface on  $AB, BC, \dots PQ, QR, \dots ZY$  respectively.

As the portion  $PQ$  is on the point of slipping from  $Q$  to  $P$ , the resultant action on it makes with the normal at either  $P$  or  $Q$  an angle differing from  $\lambda$  by an indefinitely small quantity, and on that side of the normal by which it will most assist the tension at  $Q$ .

Hence in each of the triangles  $Oab, Opq$ , &c. the angles at  $O$  are equal, and the angles  $Oab, Opq$ , &c. are each equal to  $\pi/2 - \lambda$  ultimately; the triangles therefore are all similar to one another.

Let  $n$  be the infinitely large number of portions  $AB$ , &c. of the string. Let  $n\theta = \alpha$ , a finite angle.

Then

$$Oa = Ob \cdot \frac{\cos(\lambda - \theta)}{\cos \lambda},$$

$$op = oq \frac{\cos(\lambda - \theta)}{\cos \lambda},$$

&c. &c.

$$\therefore Oa = Oz \left( \frac{\cos(\lambda - \theta)}{\cos \lambda} \right)^n = Oz (\cos \theta + \sin \theta \tan \lambda)^n;$$

$$\therefore \log Oa = \log Oz + \frac{n}{2} \log(1 - \sin^2 \theta) + n \log(1 + \mu \tan \theta)$$

$$= \log Oz - \frac{1}{2} \left( n \sin^2 \theta + \frac{n}{2} \sin^4 \theta + \&c. \right)$$

$$+ \mu n \tan \theta - \frac{\mu^2 n \tan^2 \theta}{2} + \&c.$$

$$= \log Oz + \mu x \text{ ultimately};$$

$$\therefore Oa = Oz \cdot \epsilon^{\mu x};$$

$$\therefore \text{tension at } A = \epsilon^{\mu x} \cdot \text{tension at } Z.$$

If the string be in one plane, the curve  $abcd\dots z$  will be a plane one, and as the tangent at every point makes a constant angle with the line joining the point with  $O$ , the curve is an equiangular spiral. The ratio of  $Oa$  to  $Oz$  might therefore be obtained from the known properties of that curve.

If the string be not in one plane, the curve  $abc\dots$  will not be a plane one; it can however be made so, without altering the distance of any point from  $O$ , by turning each of the triangles  $Oab$ ,  $Obc$ , &c. about a side terminating in  $O$ , until they are all in one plane, when the curve becomes an equiangular spiral, and the ratio of  $Oa$  to  $Oz$  can be obtained as suggested above.

112.\* We shall sometimes be required to solve problems of the following kind. A system of bodies is in equilibrium

under certain conditions : a gradual change occurs in one or more of these conditions—e.g. the coefficient of friction at one or more points of contact of the bodies is gradually diminished, some external force is gradually altered in magnitude or direction, or the position of one of the bodies is gradually altered. When this gradual change reaches a certain stage equilibrium is no longer possible, and it is required to ascertain the way in which equilibrium is broken, in other words, the nature of the initial motion of the different bodies. The actual way in which equilibrium is broken must satisfy the following conditions. The various forces acting on the different bodies, when such a motion is about to take place, must be able to adapt themselves so as to satisfy the necessary conditions of equilibrium, without in any way violating the laws relating to passive forces : they must also be incapable of satisfying the necessary conditions of equilibrium, if the change in the initial conditions increase still further.

We shall generally proceed by considering the different ways in which it is conceivable equilibrium might be broken, without violating the geometrical conditions. If only one of these satisfies the above conditions, it is the way required ; if more than one satisfy it, it is beyond the limits of this treatise to obtain a solution of the problem.

The following rule will often enable us to solve such problems. *If it is inconceivable that equilibrium can be broken, except by one of the bodies either turning about or sliding past a point of contact with another body, the former motion will actually take place, provided it does not involve the assumption that the total action at the point in question lies outside the cone of friction.*

This rule is a deduction from the axiomatic law relating to passive forces (Art. 106). For if we suppose the body connected with the other body at the point of contact by a smooth joint, it can only *turn about* that point. If now motion be on the point of taking place, the first body will be about to turn about the joint, which will

exert some action on it. If this action does not necessarily lie outside the cone of friction, it could be exerted at the point of contact if no joint existed, i.e. the motion is the same without the joint as with. On the other hand, if the action at the joint be outside the cone of friction there, it could not be exerted without the joint, i.e. equilibrium is about to be broken by the body *sliding past* the point of contact in question. When it is necessary to assume that the action at the joint actually lies *along* a generator of the friction-cone, the question cannot be solved by the above rule, as it shews that slipping is about to occur at the point at the same instant as rolling.

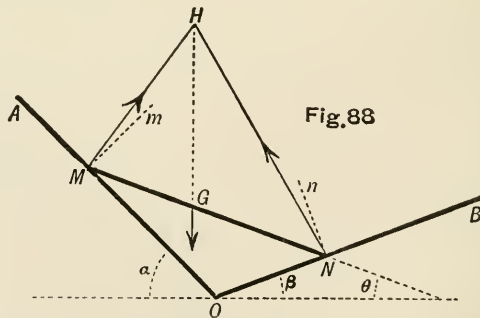
Exs. 5—8, 10—12 are illustrative of this principle and should be studied attentively.

ILLUSTRATIVE EXAMPLES.

Ex. 1. A uniform rod  $MN$  rests with its ends in two fixed straight grooves  $OA$ ,  $OB$ , in the same vertical plane, and making angles  $\alpha$ ,  $\beta$  with the horizon: prove that, when the end  $M$  is on the point of slipping down  $AO$ , the tangent of the inclination of  $MN$  to the horizon is

$$\frac{\sin(\alpha - \beta - 2\epsilon)}{2 \sin(\beta + \epsilon) \sin(\alpha - \epsilon)}$$

Let  $\theta$  be the inclination of  $MN$  to the horizon, when  $M$  is on the point of slipping down  $AO$ .



Draw  $Mm$ ,  $Nn$ , normals to  $OA$ ,  $OB$ , respectively. Since the point  $M$  is on the point of moving down  $AO$ , the limiting friction is exerted at  $M$  in the direction  $MA$ , and the direction of the total action of  $OA$  on the rod makes the angle  $\epsilon$  with  $Mm$ , on the side towards  $A$ .

Similarly, because  $N$  is on the point of slipping up  $OB$ , the total action of  $OB$  on the rod makes the angle  $\epsilon$  with  $Nn$  on the side towards  $O$ .

Let the lines of action of the forces on  $MN$  at  $M$  and  $N$  meet in  $H$  then, (Art. 61),  $H$  is vertically above  $G$ , the middle point of the rod.

Join  $HG$ .

$$MG : GH = \sin MHG : \sin HMG = \sin (\alpha - \epsilon) : \sin \left( \frac{\pi}{2} + \theta - \alpha + \epsilon \right);$$

$$\text{also } NG : GH = \sin NHG : \sin GNH = \sin (\beta + \epsilon) : \sin \left( \frac{\pi}{2} - \theta - \beta + \epsilon \right);$$

$$\therefore \sin (\alpha - \epsilon) : \cos (\alpha - \epsilon - \theta) = \sin (\beta + \epsilon) : \cos (\beta + \epsilon + \theta).$$

$$\text{Hence we obtain } \tan \theta = \frac{\sin (\alpha - \beta - 2\epsilon)}{2 \sin (\alpha - \epsilon) \cdot \sin (\beta + \epsilon)}.$$

Ex. 2. A glass rod is balanced partly in and partly out of a cylindrical tumbler with the lower end resting against the vertical side of the tumbler. If  $\alpha$  and  $\beta$  are the greatest and least angles which the rod can make with the vertical, prove that the angle of friction,  $\lambda$ , is

$$\frac{1}{2} \tan^{-1} \frac{\sin^3 \alpha - \sin^3 \beta}{\sin^2 \alpha \cos \alpha + \sin^2 \beta \cos \beta}.$$

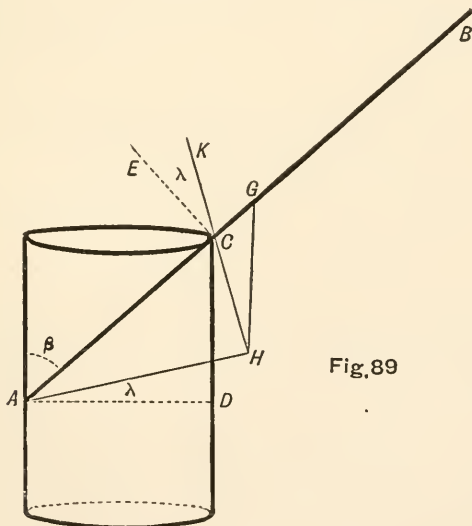


Fig. 89

Let  $AB$  be the rod,  $G$  its centre of mass. Let  $C$  be the point of the edge of the tumbler on which  $AB$  rests. Draw  $AD$  normal to the tumbler at  $A$  and  $CE$  perpendicular to the rod at  $C$ .

(i) When  $AB$  makes the *smallest* possible angle with the vertical, and is therefore on the point of slipping *into* the tumbler.

Since  $A$  is on the point of slipping down, the action there on  $AB$  is in the direction  $AH$ , which makes the angle  $\lambda$  with  $AD$  on the side towards  $C$ .

Similarly, the action at  $C$  on the rod is in the direction  $CK$ , which makes the angle  $\lambda$  with  $CE$ , on the side away from  $A$ .

Let  $KC$  and  $AH$  meet in  $H$ , which must therefore be vertically below  $G$ .

Join  $GH$ . Let  $a$  be the diameter of the tumbler, and let  $AG = c$ .

$$AG : AH = \sin AHG : \sin AGH = \cos \lambda : \sin \beta,$$

and  $AH : AC = \sin ACH : \sin AHC = \cos \lambda : \sin (2\lambda + \beta);$

$$\therefore AG : AC = \cos^2 \lambda : \sin \beta \cdot \sin (\beta + 2\lambda),$$

$$\therefore c : a \operatorname{cosec} \beta = \cos^2 \lambda : \sin \beta \cdot \sin (\beta + 2\lambda).$$

(ii) When  $AB$  makes the *greatest* possible angle with the vertical and is therefore on the point of slipping *out* of the tumbler.

By reasoning as before, we should have  $AH$  and  $CK$  on the sides of  $AD$  and  $CE$  respectively, opposite to those they were on in the first case, and we should arrive at the result obtained there, except that for  $\beta$  we must write  $\alpha$ , and for  $\lambda$ ,  $-\lambda$ .

The result would therefore be

$$c : a \operatorname{cosec} \alpha = \cos^2 \lambda : \sin \alpha \cdot \sin (\alpha - 2\lambda);$$

$$\therefore \text{eliminating } c \text{ and } a, \text{ we have}$$

$$\sin^2 \beta \sin (\beta + 2\lambda) = \sin^2 \alpha \sin (\alpha - 2\lambda);$$

$$\therefore \tan 2\lambda = \frac{\sin^3 \alpha - \sin^3 \beta}{\sin^2 \alpha \cos \alpha + \sin^2 \beta \cos \beta}.$$

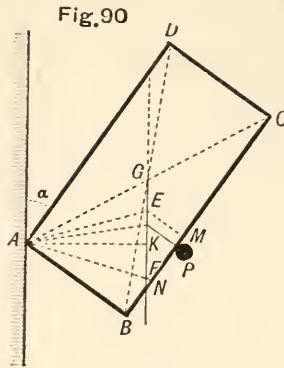
> Ex. 3. A uniform rectangular board  $ABCD$  rests with the corner  $A$  against a rough vertical wall and its side  $BC$  on a smooth peg, the plane of the board being vertical and perpendicular to that of the wall. Shew that, without disturbing the equilibrium, the peg may be moved through a space  $\mu \cos \alpha$  ( $a \cos \alpha + b \sin \alpha$ ) along the side with which it is in contact, provided  $\mu$  do not exceed a certain value:  $\alpha$  being the angle  $BC$  makes with the wall, and  $a, b$  the lengths of  $AB, BC$  respectively.

Let  $G$  be the intersection of diagonals, i. e. the centre of mass of the board.

Let  $P$  be a position of the peg when there is equilibrium.



The forces acting on the board are, its weight vertically downwards



through  $G$ , the reaction of the peg through  $P$  and at right angles to  $BC$ , and the reaction of the wall through  $A$ .

The necessary and sufficient condition of equilibrium is that these three forces should meet in a point, as the magnitudes of the reactions at  $P$  and  $A$  will adapt themselves to secure equilibrium, if the above condition holds.

Let the first two forces meet in  $K$ ; join  $AK$ , which is therefore the direction of the reaction of the wall.

But  $AK$  is not a possible direction of the reaction at  $A$ , if it makes with the normal to the wall an angle greater than  $\tan^{-1} \mu$ .

Draw  $AE$  and  $AF$  making with the normal on either side of it the angle  $\tan^{-1} \mu$ , and meeting  $GK$  in  $E$  and  $F$ . Draw  $EM$ ,  $FN$  perpendicular to  $BC$ .

The condition of equilibrium is then that  $K$  should lie between  $E$  and  $F$ , i. e. that  $P$  should lie between  $M$  and  $N$ . We may therefore, without disturbing the equilibrium of the board, move the peg through the space  $MN$  along  $BC$ .

$$\begin{aligned} \text{And } MN &= EF \cos \alpha = 2\mu \cos \alpha \times \text{horizontal distance of } G \text{ from wall} \\ &= \mu \cos \alpha (a \cos \alpha + b \sin \alpha). \end{aligned}$$

We have assumed above that  $M$  and  $N$  are both between  $B$  and  $C$ : if either lies beyond  $B$  or  $C$ , as the peg cannot be moved off the board without disturbing the equilibrium, it can only be moved along that part of  $MN$  which lies between  $B$  and  $C$ . It is obvious that if  $\mu$  be greater than a certain value, either  $M$  or  $N$  will not lie between  $B$  and  $C$ .

7 Ex. 4. If one cord of a sash window breaks, find the coefficient of friction of the sash in order that the other weight may still support the window.

Let  $ABCD$  be the window,  $W$  its weight acting at  $G$  its centre of mass.

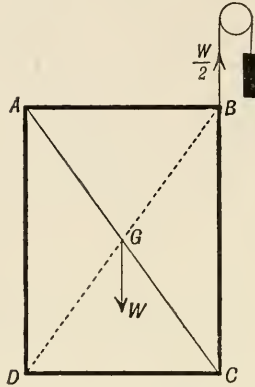


Fig.91

We assume that the window fits *loosely* in the sash, so that there will be contact at only *one* point on each side; these will be  $A$  and  $C$  respectively.

The unbroken cord at  $B$  supplies a force  $\frac{1}{2}W$  vertically upwards; the resultant of this and  $W$  is  $\frac{1}{2}W$  vertically downwards at  $A$ . Hence in order that equilibrium may be possible, the action at  $C$  must be along  $CA$ , i. e. the coefficient of friction at  $C$  must be not less than  $\tan ACD$ .

Ex. 5.\* A right circular cone, vertical angle  $2\alpha$ , rests with its base on a rough horizontal plane: a string is attached to the vertex and pulled in a horizontal direction with a gradually increasing force: determine how the equilibrium will be broken.

Let  $VAB$  be a vertical section of the cone containing the direction of

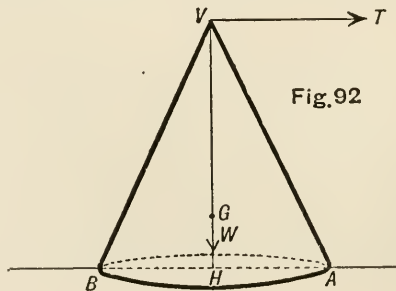


Fig.92

the string. Let  $T$  be the tension of the string when equilibrium is about to be broken, and  $W$  the weight of the cone.

The different ways in which it is conceivable equilibrium may be about to be broken are

- (1) the cone being *lifted bodily* from the plane,
- (2) the cone *tilting*, with one point of the base resting on the plane,
- (3) the cone *sliding* along the plane.

(1) is impossible, as in that case the cone would be in equilibrium under the action of  $W$  and  $T$ .

If (2) take place, the cone is in equilibrium under the action of  $W$ ,  $T$ , and the reaction of the plane at the point of contact, which must therefore be  $A$ ; also the action at  $A$  must pass through  $V$ , i. e. along  $AV$ . This is only possible when the angle  $AV$  makes with the vertical, i. e.  $\alpha$ , is less than the angle of friction ( $\lambda$ ). If, therefore,  $\alpha$  be  $< \lambda$ , (2) takes place, (Art. 112): if  $\alpha$  be  $> \lambda$ , (3) occurs.

Ex. 6.\* A uniform beam  $AB$  lies horizontally upon two others at points  $A$  and  $C$ ; prove that the least horizontal force applied at  $B$ , in a direction perpendicular to  $BA$  which is able to move the beam, is the less of the two forces  $\mu W \cdot \frac{b-a}{2a-b}$  and  $\frac{\mu W}{2}$ , where  $AB=2a$ ,  $AC=b$ ,  $W$ =weight of beam, and  $\mu$ =coefficient of friction.

The vertical pressures at  $A$  and  $C$  are  $W \cdot \frac{b-a}{b}$  and  $W \cdot \frac{a}{b}$  respectively.

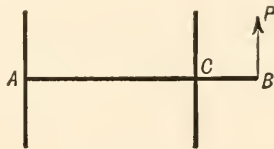


Fig. 93

The maximum frictions that can be exerted at  $A$  and  $C$  are therefore  $\mu W \cdot \frac{b-a}{b}$  and  $\mu W \cdot \frac{a}{b}$  respectively.

The frictions act horizontally and the maximum friction at either point is exerted, only when motion is about to occur at the corresponding point. The horizontal force applied at  $B$  is gradually increased until equilibrium is just about to be broken: it is required to find its maximum value,  $P$ .

Let us suppose that this maximum force  $P$  is exerted, and let us first see whether we obtain consistent results by supposing the rod just about to turn round  $A$ .

In this case as  $C$  is about to move at right angles to  $AB$  in  $P$ 's direction, the friction there is the maximum and acts in the opposite direction to  $P$ , so that the friction at  $A$  must be in the same direction as  $P$ .

Let  $F$  be the friction exerted at  $A$ .

Taking moments about  $A$  and  $C$  for the equilibrium of the rod, we have the equations

$$\begin{aligned} P \cdot 2a &= \mu W \cdot \frac{a}{b} \cdot b, \\ P \cdot (2a - b) &= F \cdot b; \\ \therefore F &= \mu W \cdot \frac{(2a - b)}{2b}. \end{aligned}$$

We have shewn (Art. 112) that the rod will turn about  $A$ , provided it is not necessary to assume the friction there greater than the maximum; therefore the rod turns about  $A$  or not, according as  $F$  or  $\mu W \frac{(2a - b)}{2b}$  is  $< W \cdot \frac{b - a}{b}$ , i.e. as  $\mu W \frac{b - a}{2a - b}$  is  $> \frac{\mu W}{2}$ .

If then  $\mu W \cdot \frac{b - a}{2a - b}$  is  $> \frac{\mu W}{2}$  the rod will turn about  $A$  as soon as  $P$  exceeds  $\frac{\mu W}{2}$ .

If  $\mu W \cdot \frac{b - a}{2a - b}$  is  $< \frac{\mu W}{2}$ , the rod will slip at  $A$  instead of turning about it.

We can shew in a similar way in this case that it will turn about  $C$ , when  $P = \mu W \cdot \frac{b - a}{2a - b}$ .

If  $\mu W \cdot \frac{b - a}{2a - b} = \frac{\mu W}{2}$ , the rod is about to slip at both  $A$  and  $B$  simultaneously when  $P = \frac{1}{2}\mu W$ : the investigation of the point about which the rod will turn in this case is beyond our present scope. It is easily seen that the point lies between  $A$  and  $C$ .

Ex. 7.\* A heavy straight rod, whose sectional area varies as the distance from one end, rests on a rough horizontal plane. At the other end, perpendicularly to its length and in the horizontal plane, a force is applied of gradually increasing magnitude: prove that the distance of the

point about which the rod begins to turn, from the end first mentioned, is given by the equation

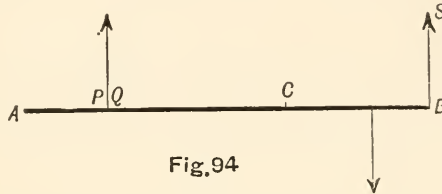
$$4x^3 - 6lx^2 + l^3 = 0,$$

where  $l$  is the length of the rod.

Let  $AB$  be the rod,  $B$  the end at which the force is applied.

Let us investigate whether or no there is a point in  $AB$  about which the rod may be on the point of turning.

If there is such a point, let  $C$  be it, and let  $x$  be its distance from the end  $A$ .



Let  $S$  be the force at  $B$ , when the motion is just about to take place.

The friction then on any point of the rod between  $C$  and  $B$  acts in the opposite direction to  $S$ , and that on any point in  $CA$  in the same direction as  $S$ .

The friction on any small portion  $PQ$  is  $\mu \times$  weight of  $PQ$ , and therefore the total friction on  $AC$  is  $\mu \times$  weight of  $AC$ , and acts at the c. m. of  $AC$ . Also the total friction on  $CB$  is  $\mu \times$  weight of  $CB$ , and acts at the c. m. of  $CB$ .

By Art. 102, the weight of  $AC = \kappa x^2$ , and that of  $AB$  is  $\kappa l^2$ : also the distance from  $A$  of the c. m. of  $AC$  is  $\frac{2}{3}x$ , that of the c. m. of  $AB$  is  $\frac{2}{3}l$ . The weight of the remainder  $CB$  is therefore  $\kappa(l^2 - x^2)$ , and the distance of its c. m. from  $A$  is  $2(l^3 - x^3) / \{3(l^2 - x^2)\}$ .

$\therefore$  taking moments about  $A$  for the equilibrium of the rod, we have

$$\mu\kappa(l^2 - x^2) \cdot \frac{2(l^3 - x^3)}{3(l^2 - x^2)} - \mu\kappa x^2 \cdot \frac{2}{3}x = Sl \dots\dots\dots (1).$$

Also resolving at right angles to the rod, we have

$$\mu\kappa(l^2 - x^2) - \mu\kappa \cdot x^2 = S \dots\dots\dots (2);$$

$\therefore$  eliminating  $S$  from equations (1) and (2)

$$2(l^3 - 2x^3) = 3l(l^2 - 2x^2);$$

$$\therefore 4x^3 - 6lx^2 + l^3 = 0.$$

Since the expression on the left hand is positive when  $x=0$ , and negative when  $x=l$ , the equation has a root between 0 and  $l$ , i.e. it

determines a real point on the rod. This must be the point, round which the rod is about to turn, since the rod will turn about it rather than slide past it (Art. 112).

Ex. 8.\* A square lamina is supported in a horizontal position by means of four rough pegs on which its angles  $A, B, C$  and  $D$  rest. A horizontal force is applied at  $C$  at right angles to  $AC$  and gradually increased until it moves the lamina. Shew that, if the pressures on the pegs be equal, the lamina will begin to turn about the angle  $A$ .

Let  $P$  be the applied force which will cause the lamina to be just on the point of motion.

We know (Art. 112) that the square will be on the point of turning about  $A$ , provided that all the necessary equations of equilibrium can be satisfied on such an assumption, without requiring the friction exerted at  $A$  to be the maximum.

Let  $O$  be the point of intersection of the diagonals of the square. Let

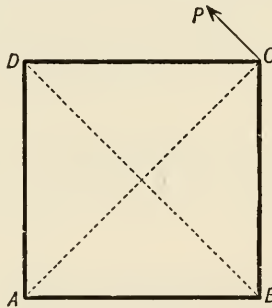


Fig. 95

$Q$  be the maximum friction that can be exerted at any of the corners of the square—then if rotation is about to take place about  $A$ , the force at  $D$  will be  $Q$  along  $DC$ , that at  $C$ ,  $Q$  opposite to  $P$ , and that at  $B$ ,  $Q$  along  $CB$ .

Taking moments about  $A$ , we have

$$P \cdot AC = Q (AD + AC + AB),$$

$$\therefore P = Q (1 + \sqrt{2}).$$

The friction at  $A$  must be equal to the resultant of the other four forces, its magnitude is therefore

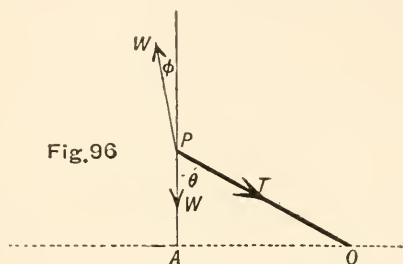
$$\sqrt{\{(P - Q - Q\sqrt{2})^2 + (Q/\sqrt{2} - Q/\sqrt{2})^2\}}, \text{ i. e. zero.}$$

$A$  is the point therefore about which the square will begin to turn.



Ex. 9. A heavy particle is placed on a rough inclined plane whose inclination is equal to the angle of friction: a thread is attached to the particle and passed through a hole in the plane which is lower than the particle, but not in the line of greatest slope: shew that if the thread be very slowly drawn through the hole the particle will describe a straight line and a semi-circle in succession.

Let  $O$  be the hole;  $OA$  the horizontal line in the inclined plane



through  $O$ . Let  $P$  be the particle,  $W$  the resolved part of its weight in the plane. The maximum friction that can be exerted on it is  $W$  therefore.

Let  $\theta$  be the angle the string  $PO$  makes with a line of greatest slope. Let  $\phi$  be the angle the direction of motion at any instant, and therefore the friction, makes with a line of greatest slope. Let  $T$  be the tension of the string.

(1) When  $P$  is above  $OA$ .

The resolved parts of forces down the line of greatest slope

$$= W + T \cos \theta - W \cos \phi.$$

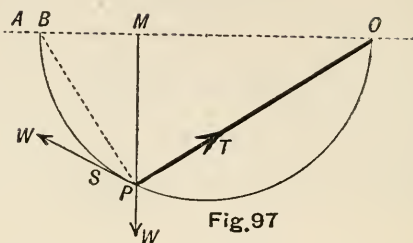
Those perpendicular to the same line  $= T \sin \theta - W \sin \phi$ .

Since the particle is drawn *very slowly*, each of these forces must be indefinitely small. Therefore  $\phi$  and  $T$  are both indefinitely small. Hence the particle moves down a line of greatest slope, until it reaches  $A$ .

(2) When  $P$  is at  $A$ .

The forces now are  $W - W \cos \phi$  and  $T - W \sin \phi$ , whence we infer that  $\phi = 0$ , i.e. the particle moves off initially at right angles to  $OA$ . The particle, however, cannot remain any longer in the same line of greatest slope, and since it must always be approaching  $O$ , it describes a curve, which has a line of greatest slope as tangent at  $A$ , and which passes through  $O$ .

(3) When  $P$  is below  $OA$ .



In this case we deduce, as before, that

$$W(1 - \cos \phi) - T \cos \theta = 0,$$

$$W \sin \phi - T \sin \theta = 0.$$

The solution  $T=0=\phi$  is inadmissible here, since we know that the particle cannot continue to move down a line of greatest slope.

Eliminating  $T$ , we have  $\frac{1 - \cos \phi}{\sin \phi} = \cot \theta$ ,

$$\therefore \tan \frac{\phi}{2} = \cot \theta,$$

$$\therefore \frac{\phi}{2} = \frac{\pi}{2} - \theta.$$

Draw  $PB$  perpendicular to  $OP$ , meeting  $OA$  in  $B$ : describe a semi-circle through  $P$ , on  $OB$  as diameter.

Let  $SP$  be the tangent at  $P$  to this circle. Then

$$\angle SPM = \angle SPB + \angle BPM = \pi - 2MPO = \phi.$$

Therefore the direction of motion at  $P$  is along the tangent to the circle, i.e. the next point to  $P$  in  $P$ 's path is on the circle. Similarly the next consecutive point to that and so on.

Hence the semi-circle is the particle's path, and as this is true always so long as  $P$  is below  $OA$ , the semi-circle must pass through  $A$ , i.e.  $A$  and  $B$  are coincident.

Ex. 10.\* A uniform heavy beam  $AB$  is placed with the end  $A$  upon a rough horizontal plane and a point  $C$  of its length touching a rough heavy sphere whose point of contact with the plane is  $D$ . Prove that if there is equilibrium the magnitude of the friction at each of the three points  $A$ ,  $C$ ,  $D$  will be the same. If the coefficient of friction be the same at each point, the point at which slipping is most likely to take place

will be  $A$  or  $C$ , according as  $A$  and  $D$  lie on the same or opposite sides of the vertical through  $B$ .

Let  $O$  be the centre of the sphere,  $G$  the middle point of the beam.

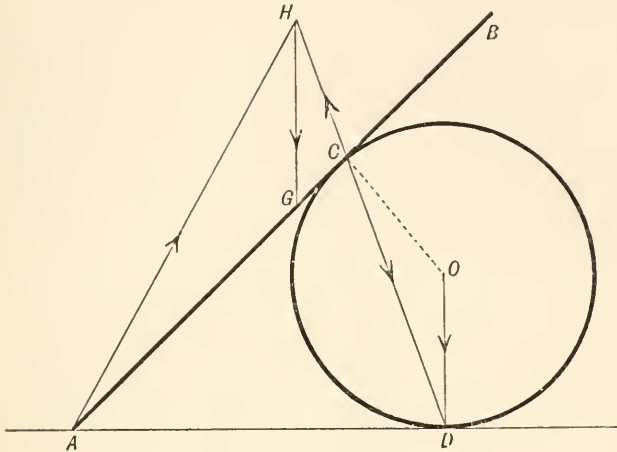


Fig.99

Considering the equilibrium of the sphere and beam together, since the horizontal forces acting on them are the frictions at  $A$  and  $D$  respectively, they must be equal.

Also from the equilibrium of the sphere, by taking moments about  $O$ , we deduce that the friction at  $C$  = that at  $D$  = that at  $A$ .

Let us suppose that the sphere is slowly moved away from  $A$ , until equilibrium is about to be broken; what will be the nature of the motion which is about to happen? Of the three forces acting on the sphere, two, the weight and the reaction at  $D$  act through  $D$ , therefore the third, the action at  $C$ , is along  $CD$ , and the action at  $D$  is within the angle  $CDO$ . Hence slipping cannot be about to occur at  $D$ , as then the angle  $CDO$ , and therefore the angle  $OCD$ , would be greater than the angle of friction, which is impossible, as it is the angle the action at  $C$  makes with the normal.

Let  $DC$  produced meet the vertical through  $G$  in  $H$ : join  $AH$ .  $AH$  is the direction of the action on  $AB$  at  $A$ .

Hence either the angle  $AH$  makes with the vertical, or  $OCD$  must be the angle of friction, as slipping must occur at either  $A$  or  $C$ .

The slipping occurs at  $A$  or  $C$

according as  $\angle AHG$  is  $>$  or  $<$   $\angle OCD$ , i.e.  $\angle ODC$ , i.e.  $\angle GHC$ ,  
according as  $G$  is nearer  $A$  or  $D$ ,

according as  $A$  and  $B$  are on the same or opposite sides of the vertical through  $D$ .

Ex. 11.\* A heavy cube with its vertical face smooth, is placed on a rough horizontal plane, and a ladder is placed with the upper end leaning against it, the vertical plane containing the ladder also containing the centre of mass of the cube. A man now ascends the ladder and when he reaches a certain height the equilibrium ceases. Examine the character of the ensuing disturbance.

Let  $AB$  be the ladder,  $CDEF$  the section of the cube made by the

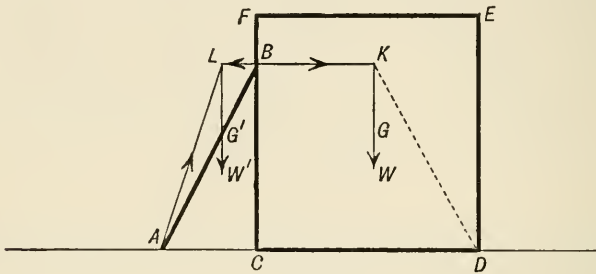


Fig. 100

vertical plane through the ladder. Let  $G'$  be the centre of mass of the ladder and man when motion is about to take place,  $W'$  their weight. Let  $W$  be the weight of the cube,  $G$  its centre of mass. Let  $\lambda$  be the angle of friction at the different points of contact with the ground.

The ways in which we can imagine the equilibrium to be broken are

- (1) the ladder turning about  $A$  and slipping at  $B$ , and the cube turning about  $D$ ,
- (2) the ladder turning about  $A$  and slipping at  $B$ , the cube sliding,
- (3) the ladder slipping at  $A$  and  $B$ , the cube remaining stationary,
- (4) the ladder slipping at  $A$  and  $B$ , and the cube sliding along the plane,
- (5) the ladder slipping at  $A$  and  $B$ , and the cube turning about  $D$ ,
- (6) the ladder slipping at  $A$  but not at  $B$ , and the cube sliding,
- (7) the ladder slipping at  $A$  but not at  $B$ , and the cube turning about  $D$ .

Since the vertical sides of the cube are smooth, the action and reaction ( $R$ ) at  $B$  are horizontal. Draw  $LBK$  horizontally to meet the vertical lines through  $G'$  and  $G$  in  $L$  and  $K$  respectively. Join  $AL$ ,  $DK$ . The action at  $A$  must be along  $AL$ .

By Art. 112, slipping will not occur at  $A$  if the angle  $AL$  makes with the vertical, i.e. the angle  $ALG'$ , be less than  $\lambda$ , but will otherwise.

(a) Let  $\angle ALG'$  be  $< \lambda$ . (1) or (2) must then occur.

If (1) occur, the action of the plane on the cube is along  $DK$ . Hence (Art. 112) (1) occurs if the  $\angle KDE$  is  $< \lambda$ , but (2) occurs otherwise.

(b) Let  $\angle ALG' = \lambda$ . Neither (1) nor (2) can occur in this case.

(6) and (7) are clearly out of the question, as each would involve  $A$  moving in direction  $AC$ , which is impossible as the total action at  $A$  is along  $AL$ .

If (5) occur, the resultant of  $R$  and  $W$  must act along  $KD$ , and we must have the angle  $KDE = \tan^{-1}(R/W)$  and  $< \lambda$ , but  $\lambda = \angle ALG' = \tan^{-1}(R/W')$ . Hence we must have  $W' < W$ , and  $W \tan KDE = W' \tan \lambda$ .

If these conditions hold (5) occurs.

If  $\angle KDE$  be  $> \tan^{-1}(R/W)$ , i.e. if  $W \tan KDE$  be  $> W' \tan \lambda$ , (3) or (4) must occur.

(3) occurs if  $\tan \lambda$  be  $> R/W$ , i.e. if  $W'$  be  $< W$ , and (4) otherwise.

Ex. 12.\* A block in the shape of a rectangular parallelepiped of weight  $W$  rests with one edge horizontal on a rough inclined plane;

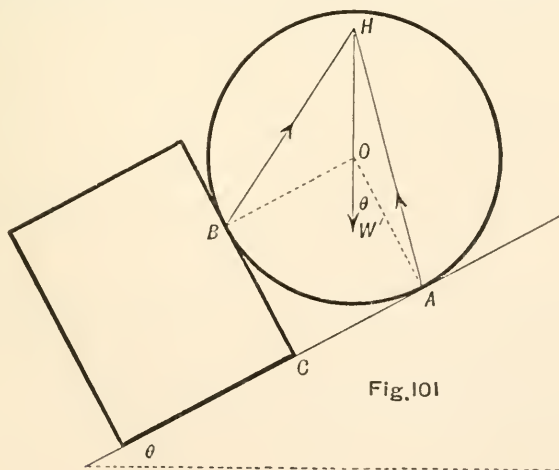


Fig. 101

against the block rests a rough sphere ( $W'$ ) whose radius is less than the thickness of the block. The inclination of the plane is gradually increased

until equilibrium is no longer possible: shew that if the block tilt, the sphere will slide or roll along the plane according as the limiting inclination ( $\theta$ ) of the plane to the horizon is  $>$  or  $<$   $\pi/4$ ; and shew also that if the block slide, the sphere will slide or roll according as  $\lambda$  (the angle of friction) is  $>$  or  $<$   $\pi/4$ , and that in the last case,  $\theta$  is given by the equation  $W \sin(\lambda - \theta) = W' \sin \theta (\cos \lambda - \sin \lambda)$ ,  $\lambda$  being supposed the same everywhere.

Let  $O$  be the centre of the sphere,  $A$  and  $B$  the points where it touches the plane and block respectively:  $C$  the point of the block nearest to  $A$ . Let the inclination of the plane ( $\theta$ ) be such that equilibrium is just on the point of being broken.

There are only two motions of the block conceivable,

- (1) turning about its lowest edge,
- (2) sliding down the plane.

Whichever of these two ways the block moves, the sphere will either

- ( $\alpha$ ) slip at  $B$  and roll at  $A$ , or
- ( $\beta$ ) roll at  $B$  and slip at  $A$ .

The actions at  $A$  and  $B$  on the sphere must meet in the vertical through  $O$ , in the point  $H$  say: join  $AH$ ,  $BH$ , these will be the directions of the respective reactions.

As we have seen either ( $\alpha$ ) or ( $\beta$ ) must occur, one of the angles  $OBH$ ,  $OAH$  must equal  $\lambda$ , and as the other angle must be less than  $\lambda$ , it is the greater angle of the two that is equal to  $\lambda$ .

We shall prove that  $\angle OBH$  is  $>$  or  $<$   $\angle OAH$ , according as  $\theta$  is  $<$  or  $>$   $\pi/4$ .

If  $\theta$  is  $<$   $\pi/4$ ,  $\angle AOH$  is  $>$   $\angle BOH$ ,

$$\therefore AH \text{ is } > BH,$$

and as  $BO = OA$ , and  $OH$  is common to the two triangles  $OBH$ ,  $OHA$ ,

$$\angle OBH \text{ is } > \angle OAH.$$

Similarly it can be shewn that if  $\theta$  is  $>$   $\pi/4$ ,  $\angle OAH$  is  $>$   $\angle OBH$ .

Hence whether (1) or (2) happen to the block the sphere will roll or slide at  $A$ , according as  $\theta$  is  $<$  or  $>$   $\pi/4$ .

If (2) and ( $\beta$ ) happen,  $\theta = \lambda$ , and  $\lambda$  is therefore  $>$   $\pi/4$ .

To find  $\theta$  when (2) and ( $\alpha$ ) happen,

Let  $R$  be the normal reaction at  $B$ , then taking moments about  $A$  for the equilibrium of the sphere,

$$W'a \sin \theta = R(1 + \tan \lambda) a.$$



Resolving along the plane for the equilibrium of the block

$$W' \sin \theta + R = (W \cos \theta + R \tan \lambda) \tan \lambda.$$

$$\therefore W (\sin \theta - \cos \theta \tan \lambda) (1 + \tan \lambda) = W' \sin \theta \cdot (\tan^2 \lambda - 1),$$

$$\therefore W' \sin (\lambda - \theta) = W' \sin \theta \cdot (\cos \lambda - \sin \lambda).$$

Since  $\theta$  cannot be greater than  $\lambda$ , this equation shews that if  $\lambda$  be  $> \pi/4$ , (2) and ( $\alpha$ ) cannot happen.

EXAMPLES.

1. A body is supported on a rough inclined plane by a force acting along it. If the least magnitude of the force, when the plane is inclined at an angle  $\alpha$  to the horizon, be equal to the greatest magnitude when the plane is inclined at an angle  $\beta$ , shew that the angle of friction is  $\frac{1}{2}(\alpha - \beta)$ .

2. Two equal particles on two inclined planes are connected by a string which lies wholly in a vertical plane perpendicular to the line of junction of the planes, and passes over a smooth peg vertically above this line of junction. If, when the particles are on the point of motion, the portions of the string make equal angles with the vertical, shew that the difference between the inclinations of the planes must be twice the angle of friction.

3. A uniform rod is resting on a rough inclined plane, and is moveable on the plane about one end which is fixed: shew that when it is about to slip it makes with the line of greatest slope the angle  $\sin^{-1}(\mu \cot \alpha)$ .

4. Spheres whose weights are  $W$ ,  $W'$  rest on different and differently inclined planes. The highest points of the spheres are connected by a horizontal string perpendicular to the common horizontal edge of the two planes above it. If  $\mu$ ,  $\mu'$  the coefficients of friction are such that each sphere is on the point of slipping down,  $\mu W = \mu' W'$ .

5. Two equal particles rest upon two equally rough inclined planes, being connected by a string passing over a smooth pulley at the common vertex, the vertical plane which contains the string being at right angles to each inclined plane. If the weight of one particle be increased by a certain amount the system is on the point of motion, and if instead the weight of the other particle be decreased by the same amount the system is again on the point of motion in the same direction as before. Prove that the difference of the inclinations of the two planes is double the angle of friction.

6. A lamina is suspended by three strings from a point: if the lamina be rough, and the coefficient of friction between it and a particle placed upon it be constant, shew that the boundary of possible positions of equilibrium of the particle on the lamina is a circle.

7. A uniform heavy rod is in equilibrium in a rough spherical cup; and the length of the rod subtends a right angle at the centre of the sphere; find the greatest angle the rod can make with the horizon in terms of the angle of friction.

8. Two fixed pegs are in a line inclined at a given angle  $\alpha$  to the horizon. A rough thin rod rests on the higher and passes under the lower, the higher peg being lower than the centre of gravity of the rod. The distance of that point from the pegs being  $a$  and  $b$  respectively, shew that when the rod is on the point of motion  $(b+a)\mu = (b-a)\tan\alpha$ .

9. Prove that the direction of the least force required to draw a carriage is inclined at an angle  $\theta$  to the ground, where  $a\sin\theta = b\sin\phi$ ,  $a$  being the radius of the wheels,  $b$  of the axles, and  $\tan\phi$  the coefficient of friction of the axles.

10. A light string is placed over a rough vertical circle, and a uniform heavy rod, whose length is equal to the diameter of the circle, has one end attached to each end of the string, and rests in a horizontal position. Find within what points on the rod a given mass may be placed, without disturbing the equilibrium of the system: and shew that the given mass may be placed anywhere on the rod, provided the ratio of its weight to that of the rod does not exceed  $\frac{1}{2}(e^{\mu\pi} - 1)$ , where  $\mu$  is the coefficient of friction between the string and the circle.

11. Two particles of unequal mass are tied by fine inextensible strings to a third particle. They lie on a rough horizontal plane with the strings stretched at a given angle to each other. Find the magnitude and direction of the least horizontal force which, applied to the third particle, will move all three.

12. An equilateral triangle, of uniform material, rests with one end of its base on a rough horizontal plane and the other against a smooth vertical wall: shew that the least angle its base can make with the horizontal plane is given by the equation  $\cot\theta = 2\mu + 1/\sqrt{3}$ ,  $\mu$  being the coefficient of friction.

13. Two weights  $P$ ,  $Q$  are connected by a string and rest one on each face of a double inclined plane, the string passing over the common vertex, which is smooth: at first  $P$  is about to slip downwards and when

the weights are interchanged, it is found that  $P$  is still just about to slip downwards: shew that if  $\lambda, \lambda'$  are the angles of friction for the two planes and  $\alpha, \beta$  the angles they respectively make with the horizon, then

$$\cos \alpha \cdot \cos \lambda' = \cos \beta \cdot \cos \lambda.$$

14. Two rough spheres, the larger of which is fixed, rest on a rough horizontal plane, and a uniform board rests symmetrically upon the top of them, its centre of gravity being midway between the points of contact: shew that, if  $\tan \lambda'$  and  $\tan \lambda$  be the coefficients of friction between the board and the larger and smaller spheres respectively, and motion be about to take place at both points of contact,  $\tan (\lambda' - \lambda) = \sin^2 \lambda$ .

15. Two rings, each of weight  $w$ , slide upon a vertical semi-circular wire, diameter horizontal and convexity upwards. They are connected by a light string of length  $2l$  (supposed less than the diameter  $2a$ ) on which is slipped a ring of weight  $W$ . Shew that when the two rings are as far apart as possible, the angle  $2\alpha$  subtended by them at the centre is given by  $(W + 2w)^2 \tan^2(\alpha + \epsilon) (l^2 - a^2 \sin^2 \alpha) = W^2 a^2 \sin^2 \alpha$ ,  $\epsilon$  being the angle of friction.

16. An isosceles triangular prism is placed with its edge horizontal and its base on a rough inclined plane, the inclination of which is gradually increased: shew that the prism will tumble or slide according as  $\mu$  is  $>$  or  $<$   $3c/2h$ .  $c$  is the base of a section perpendicular to the edge and  $h$  the height.

17. Two hemispheres, of radii  $a$  and  $b$ , have their bases fixed to a horizontal plane, and a plank rests symmetrically upon them. If  $\mu$  be the coefficient of friction between the plank and either hemisphere, the other being smooth, prove that, when the plank is on the point of slipping, the distance of its centre from its point of contact with the smooth hemisphere is equal to  $(a \sim b)/\mu$ .

18. A disc in the shape of a sector of a circle lies on a rough table ( $\mu$ ) and is fastened at the centre by a peg. Shew that the least force applied along any tangent to the sector necessary to turn it round is to the weight of the disc as  $2\mu : 3$ .

19. A rod rests partly within and partly without a box in the shape of a rectangular parallelepiped, and presses with one end against the rough vertical side of the box and rests in contact with the opposite smooth edge. The weight of the box being four times that of the rod, shew that if the rod be about to slip and the box about to tumble at the

same instant, the angle the rod makes with the vertical is

$$\frac{1}{2}\lambda + \frac{1}{2}\cos^{-1}\left(\frac{1}{3}\cos\lambda\right),$$

where  $\lambda$  is the angle of friction.

20. Three equal heavy rough cylinders are placed in contact along generating lines, lying on a horizontal plane: and two other such cylinders are similarly placed upon them: find the frictions and reactions at the instant when the system is bordering on motion.

21. A sphere (radius  $a$ ) whose centre of gravity is distant  $c$  from its centre, rests in limiting equilibrium on a rough plane, which is inclined at an angle  $\alpha$  to the horizon: shew that the sphere may be turned through the angle  $2\cos^{-1}\left(\frac{a\sin\alpha}{c}\right)$  and still be in limiting equilibrium.

22. Assuming that the limiting friction consists of two parts, one proportional to the pressure, and the other to the surface in contact, shew that if the least force which can support a rectangular parallelepiped, whose edges are  $a$ ,  $b$ , and  $c$  on a given inclined plane be  $P$ ,  $Q$ ,  $R$ , when the faces in contact are  $bc$ ,  $ca$ ,  $ab$  respectively, then

$$(Q - R)bc + (R - P)ac + (P - Q)ab = 0.$$

23. A rough rod rests over a rough sphere, one end of the rod pressing on a rough horizontal plane, on which the sphere rests. Shew that there will be limiting equilibrium for the whole system when the rod makes an angle  $2\lambda_2$  with the plane, if the weight of the sphere is to the weight of the rod in the ratio  $\sin(\lambda_2 - \lambda_1) : \sin(\lambda_2 + \lambda_1)$ , where  $\lambda_1$  is the angle of friction between the rod or sphere and the plane, and  $\lambda_2$  the angle of friction between the rod and sphere.

24. A rectangular lamina rests in a vertical plane with the middle point of one side in contact with a rough peg, the coefficient of friction being 2, and a point in the opposite side in contact with a smooth peg. If the line joining the pegs make an angle  $\alpha$  with the vertical, and the sides in contact with the pegs an angle  $\theta$ , when the lamina is just about to slip, shew that  $\tan(\theta - \alpha) = 1 - 2\tan\theta$ .

25. A heavy rod  $PQ$  is in equilibrium with its ends on a rough parabola whose axis is vertical and vertex downwards: shew that the line joining the intersection of the tangents to the parabola at  $P$ ,  $Q$  to the intersection of the normals makes with the vertical an angle not  $>$  the angle of friction.

26. A pair of equal rods  $AB, AC$  are hinged together at  $A$  and have rings at  $B, C$ : these rings are free to slide along fine rough ( $\mu$ ) straight wires  $OB', OC'$  in the same vertical plane equally inclined at an angle  $\alpha$  to the vertical. Shew that in the limiting positions of equilibrium the angle between the rods is either

$$2 \tan^{-1} 2 \frac{1 + \mu \tan \alpha}{\tan \alpha - \mu} \text{ or } 2 \tan^{-1} 2 \frac{1 - \mu \tan \alpha}{\tan \alpha + \mu}.$$

27. A right-angled isosceles triangular lamina rests with its base angles on the arc of a rough circular wire whose plane is vertical and radius equal to either of the equal sides of the triangle. If the equal sides be horizontal and vertical in the limiting position of equilibrium the coefficient of friction is  $\frac{1}{4} \{ \sqrt{17} - 3 \}$ .

28. Two uniform rods of equal weight, but different lengths, are jointed together and placed in a vertical plane over two rough pegs in the same horizontal line: if  $\alpha, \beta$  be the inclinations of the rods to the horizon,  $\theta$  that of the reaction at the hinge, prove that when the rods are on the point of slipping,  $2 \tan \theta = \cot(\beta + \lambda) - \cot(\alpha - \lambda)$ , where  $\lambda$  is the angle of friction.

29. An ellipse is placed with its plane vertical and major axis horizontal so that one of its vertices  $A$  rests against a rough vertical wall.  $P$  is a point on the wall vertically above  $A$ , and a string of length  $2l$  which has its extremities fastened at the foci  $S, H$  passes through  $P$ . Find the least value of the coefficient of friction consistent with the equilibrium of the ellipse.

30. A uniform ladder (length  $2a$ ) rests at an angle  $\alpha$  to the vertical against a smooth horizontal rail at a height  $h$  from the ground. If  $\lambda$  be the angle of friction, between the ground and the ladder, shew that a man of weight  $n$  times that of the ladder may ascend a distance along the ladder,  $\{ 2(n+1)h \sin \lambda \cdot \sec(\alpha - \lambda) \operatorname{cosec} 2\alpha - a \} / n$ , without the ladder slipping.

31. A uniform rod  $AB$  rests with its ends on a rough circular wire in a vertical plane and the equilibrium is limiting; shew that the vertical through the centre of the rod meets the circle through  $AB$  and the centre of the wire in two points, in one of which the directions of the resultant actions at  $A$  and  $B$  meet.

32. A uniform rod of mass  $M$  rests in a horizontal position with its ends on the circumference of a rough vertical circle and subtends an angle  $2\alpha$  at the centre. An insect of mass  $m$  starts from the middle point of the



rod and crawls gently towards one end. Prove that if the angle  $\epsilon$  of friction be less than  $45^\circ$  it will be able to reach the end of the rod without disturbing the equilibrium provided  $\sin 2\epsilon > m \sin 2a/(M+m)$ .

Examine the case when  $\epsilon > 45^\circ$ .

33. A rod resting with one end on a rough horizontal plane, leans against a rough cylinder, which rests on the plane, with its axis at right angles to the rod. Determine how the equilibrium is broken, when the plane is gradually more and more inclined.

34. A uniform rod, length  $2a \sin \alpha$ , is placed within a rough vertical circle, radius  $a$ , and is on the point of motion, the coefficients of friction at its upper and lower ends are  $\tan \lambda'$ ,  $\tan \lambda$ : prove that if  $\theta$  be the inclination to the vertical of the line joining the centre of the circle to the centre of the rod

$$\tan \theta = \frac{\sin (\lambda + \lambda')}{2 \cos (\lambda + \alpha) \cos (\lambda' - \alpha)}.$$

Examine the case when  $\alpha + \lambda = \pi/2$ .

35. One end of a heavy rod  $AB$  can slide along a rough horizontal rod  $AC$  to which it is attached by a ring;  $B$  and  $C$  are joined by a string: if  $ABC$  be a right angle when the rod is just on the point of slipping,  $\mu$  the coefficient of friction and  $\alpha$  the angle between  $AB$  and the vertical, shew that

$$\mu = \frac{\sin \alpha \cos \alpha}{1 + \cos^2 \alpha}.$$

36. A circular lamina, whose centre of gravity is at an excentric point, rests in a vertical plane supported by the loop of a rough string which is attached to two fixed points. If the lamina be on the point of slipping and the radius containing its centre of gravity be inclined at right angles to the radius bisecting the portion of the string in contact with the circle, the angle of contact  $\phi$ , is given by

$$\frac{1 + \epsilon^{\mu\phi}}{1 - \epsilon^{\mu\phi}} \sin \frac{\phi}{2} = \frac{a}{c},$$

$a$  being the radius of the circle and  $c$  the distance of its centre from its centre of gravity.

37. A rough circular disc of radius  $a$  has its centre of gravity at a distance  $b$  from the centre, and rests in a vertical plane on two pegs placed at a distance apart  $< 2\sqrt{a^2 - b^2}$  and  $> 2b$  in a horizontal line: shew that equilibrium is possible for all positions of the centre of gravity provided the angle of friction be not less than  $\sin^{-1}(b/a)$ .



38. Two equal heavy rods  $AB, BC$ , each of length  $2a$ , joined together at  $B$ , hang with  $AB$  resting on a rough peg  $P$ . If  $\mu$  be the coefficient of friction, and  $2\alpha$  the angle between the rods, shew that  $AB$  will slip on the peg if  $PB < a \cos \alpha (\cos \alpha - \mu \sin \alpha)$  or  $> a \cos \alpha (\cos \alpha + \mu \sin \alpha)$ .

39. A uniform isosceles triangular lamina rests in a limiting position of equilibrium in a vertical plane between two rough pegs in the same horizontal line: prove that  $3c \cos \lambda \cos (\theta + \alpha) = 2p \sin 2\alpha \cdot \sin (2\theta + 2\alpha - \lambda)$ , where  $\theta$  is the inclination of one side to the horizon,  $\lambda$  the angle of friction,  $2\alpha$  the vertical angle of the triangle,  $p$  the perpendicular from the vertex on the base, and  $c$  the distance between the pegs.

40. Three rough particles of masses  $m_1, m_2, m_3$  are rigidly connected by light smooth wires meeting in a point  $O$ , such that the particles are at the vertices of an equilateral triangle whose centre is  $O$ . The system is placed on an inclined plane of slope  $\alpha$ , to which it is attached by a pivot through  $O$ ; prove that it will rest in any position if the coefficient of friction for none of the particles be less than

$$\frac{\tan \alpha}{m_1 + m_2 + m_3} (m_1^2 + m_2^2 + m_3^2 - m_2 m_3 - m_3 m_1 - m_1 m_2)^{\frac{1}{2}}.$$

41. A cylindrical rod with hemispherical ends rests in a vertical plane against two equally rough planes, one horizontal, the other vertical: determine the limiting position of equilibrium, and shew that if the coefficient of friction be not less than the ratio of the length of the straight part of the rod to the total length, it will rest in any position.

42. A uniform heavy rod of given length rests perpendicularly and horizontally across two rough parallel horizontal rails which support the rod at a quarter of its length from each end. One end of the rod is pulled perpendicularly by a string in a downward direction making an angle  $\theta$  with the vertical: shew that the rod will move at both points of support at the same time when  $\theta = \tan^{-1} 2\mu$ ; and in this case find the tension of the string.

43. To the ends of a heavy rod are attached rings which slide on the circumference of a rough vertical circle. Find the force perpendicular to its direction, acting at a given point of it which will just move the rod when in any position: and prove that for all positions it will be greatest when the rod is inclined to the horizon at an angle

$$\tan^{-1} (\cot 2\epsilon + \cos 2\alpha / \sin 2\epsilon),$$

where  $2\alpha$  is the angle subtended by the rod at the centre and  $\tan \epsilon$  the coefficient of friction.

44. A straight uniform rod of length  $2c$  is placed in a horizontal position as high as possible within a hollow rough sphere of radius  $a$ . Prove that the line joining the middle point of the rod to the centre of the sphere makes with the vertical an angle  $\tan^{-1} \mu a / \sqrt{(a^2 - c^2)}$ .

45. A semi-circular arch, composed of an odd number of equal and similar smooth blocks, is constructed upon a rough horizontal plane: prove that the number of blocks must be 3: and that the coefficient of friction must be not  $< 1/\sqrt{3}$ . Also prove that the ratio of the internal to the external arch must not be  $>$  the positive root of the equation

$$2\sqrt{3}(x^2 + x + 1) + \pi(2x^2 - x - 3) = 0.$$

If the blocks, except the key stone, be rough, and if their number be  $n$ , greater than 3, prove that the angle of friction at the  $p$ th joint from the base must be not  $< \cot^{-1} \{(n - 2p) \tan \pi/2n\} - p\pi/n$ .

46. Two particles of equal weight  $w$  connected by a rod without weight rest on a rough plane inclined to the horizontal at an angle  $\alpha$ : the coefficient of friction  $\rho' \tan \alpha$  for one particle is less, and that for the other  $\rho \tan \alpha$  greater, than  $\tan \alpha$ . Prove that, when both are on the point of moving, if in the plane a triangle  $ABP$  be constructed whose sides  $AB$ ,  $BP$ ,  $PA$  are  $2$ ,  $\rho'$ ,  $\rho$ , and  $O$  be the middle point of  $AB$  which is drawn in a line of greatest slope, then  $OP$  is the direction and  $OP \cdot w \sin \alpha$  is the tension of the rod.

47. An elliptical cylinder placed in contact with a vertical wall and a horizontal plane is just on the point of motion when its major axis is inclined at an angle  $\alpha$  to the horizon. Determine the relation between the coefficients of friction of the wall and plane: and shew from your result that if the wall be smooth, and  $\alpha$  be equal to  $45^\circ$ , the coefficient of friction between the plane and cylinder will be equal to  $\frac{1}{2}e^2$ , where  $e$  is the eccentricity of the transverse section of the cylinder.

48. Two equal spheres rest on a rough horizontal plane, the distance between their centres being  $c$ : and a third sphere rests on them: prove that the normal pressure between the two spheres is equal to half the weight of the upper sphere, and that the necessary and sufficient condition of equilibrium is  $a + b > \frac{1}{2}c \cdot \operatorname{cosec} 2\epsilon$ , where  $\epsilon$  is the angle of friction, and  $a$ ,  $b$  the radii of the spheres.

If this condition is not fulfilled how will the lower spheres begin to move?

49. An elliptic lamina of eccentricity  $e$  rests upon a perfectly rough equal and similar lamina, the two bodies being symmetrically situated

with respect to their common tangent at the point of contact. If  $\alpha$  be the inclination of the major axis of the fixed ellipse to the horizon, and  $\theta$  be the inclination, measured in the same direction, of the major axis of the moving ellipse in a position of equilibrium, then

$$\sin \frac{1}{2} (\theta + \alpha) = e^2 \sin \theta \cos \frac{1}{2} (\theta - \alpha).$$

50. A chain is formed by  $2n$  rods, equal in length and weight, smoothly jointed together. The two extremities can move by rings on a rough horizontal rod, coefficient  $\mu$ . Shew that in the limiting position of equilibrium the inclination of either of the upper rods to the vertical is

$$\tan^{-1} \frac{2n\mu}{2n-1}.$$

51. A rough elliptic cylinder rests with its axis horizontal upon the ground and against a vertical wall, the ground and the wall being equally rough; shew that the cylinder will be on the point of slipping when its major axis plane is inclined at an angle of  $\pi/4$  to the vertical if the eccentricity of its principal section be  $\sqrt{\{2 \sin \lambda (\sin \lambda + \cos \lambda)\}}$ , where  $\lambda$  is the angle of friction.

52. An elliptic lamina moveable about its focus in a vertical plane rests against a smooth inclined plane, the major axis of the ellipse being horizontal. The lower surface of the plane is rough and rests just on the point of moving on a horizontal table. If  $a, b$  be the semi-axes of the ellipse, and  $p$  the perpendicular from the centre on the inclined plane, shew that the coefficient of friction is  $\sqrt{\{(p^2 - b^2)/(a^2 - p^2)\}}$ .

53. A circular ring of weight  $W$  hangs in a vertical plane over a rough peg, and to the lowest point of the ring a string is fastened. It is kept always horizontal in the plane of the ring, and its tension is gradually increased from zero. Prove that the ring will slip on the peg when the tension of the string reaches the value  $W \tan \frac{1}{2} \{\sin^{-1} (3 \sin \epsilon) - \epsilon\}$ ,  $\epsilon$  being the angle of friction; and explain what happens if  $3 \sin \epsilon > 1$ .

If the tension be still further increased to a given value  $T$ , find the position of equilibrium.

54. A ring of diameter  $a$  is fixed with its plane making an angle  $\alpha$  with the vertical, and a rough uniform cylinder is supported by being slipped through the ring: prove that the length of the cylinder must be not less than

$$a \cos \theta \cdot \frac{\cos (\theta \pm \alpha - \lambda)}{\sin (\theta \pm \alpha) \sin \lambda},$$

where  $\lambda$  is the angle of friction, and  $\theta$  is the inclination to the axis of the

cylinder of a plane section whose major axis is equal to  $a$ . (The sign to be taken in the above expression depends on whether the cylinder and ring make angles with the vertical on the same or opposite sides.)

55. A cylinder is laid on a rough horizontal plane, and is in contact with a rough vertical wall, the coefficients of friction being equal; a string, coiled round it at right angles to the axis, passes over a fixed pulley and sustains a weight which is gradually increased until equilibrium is broken.

Determine the nature of the initial motion. (Jellett's *Friction*.)

56. Two uniform beams, of the same material and thickness but of different lengths, rest each with one end on a rough horizontal plane, and their other ends connected by a smooth joint. If equilibrium be about to be broken shew in what way it will happen.

57. Two weights,  $P$ ,  $Q$ , whose coefficients of friction are  $\mu_1$ ,  $\mu_2$ , each less than  $\tan \alpha$ , on a rough inclined plane of angle  $\alpha$ , are connected by a string which passes through a fixed pulley  $A$  in the plane. Prove that if the angle  $PAQ$  be the greatest possible the squares of the weights of  $P$ ,  $Q$ , are to one another as  $1 - \mu_2^2 \cot^2 \alpha$  is to  $1 - \mu_1^2 \cot^2 \alpha$ .

58. A rough rod is laid on a horizontal table and is acted on by a horizontal force perpendicular to its length. Find about what point the rod will begin to turn, the point of application of the force trisecting the rod.

59. A cubical uniform block is placed on a rough inclined plane and has two of its faces vertical: it is attached by a string parallel to a line of greatest slope of the plane passing from the middle point of its upper horizontal edge to the middle point of the nearest horizontal edge of another equal similarly situated cube. If  $\mu$  (less than unity) be the coefficient of friction for the lower block, the equilibrium will be broken when the inclination of the plane to the horizon is given by  $2\mu = 3 \sin \theta - \cos \theta$ , by the higher cube tumbling over, provided the friction coefficient for the higher block be great enough.

60. A heavy rod, of length  $2l$ , rests horizontally on the inside rough surface of a hollow circular cone, the axis of which is vertical and the vertex downwards. If  $2\alpha$  is the vertical angle of the cone, and if the coefficient of friction is less than  $\cot \alpha$ , prove that the greatest height of the rod, when in equilibrium, above the vertex of the cone is

$$l \cot \alpha \cdot \left\{ \frac{1 + \cos^2 \alpha + \sin^2 \alpha \sqrt{(\sin^2 \alpha + 4\mu^2)}}{2(1 - \mu^2 \tan^2 \alpha)} \right\}^{\frac{1}{2}}.$$

61. A cubical block, and a cylinder whose diameter is equal to a side of the cube, are laid upon a rough plane, and are attached to each other by a cord coiled round the middle of the cylinder, and fixed to the middle point of one of the edges of the cube which is parallel to the axis of the cylinder. If the plane be then slowly raised (the cube being uppermost) until equilibrium is broken, what will be the nature of the initial motion?

(Jellett's *Friction*.)

62. Two particles  $A$  and  $B$  of weight  $W$  are connected by a thin weightless rod and placed on a rough inclined plane at an inclination to the line of greatest slope, the coefficient of friction for each particle being  $\mu$ . A force  $F$  is applied to  $A$  the lower particle in the direction  $BA$  and its direction gradually turned through an angle  $\theta$  in the plane. Find the nature of the initial motion of the system. If the particles be placed along a line of greatest slope, prove that both will slip when

$$\cos \theta = \frac{F^2 + 4W^2 \sin \alpha (\sin \alpha - \mu \cos \alpha)}{2FW (\mu \cos \alpha - 2 \sin \alpha)},$$

and find the limits between which  $F$  must lie when  $\alpha < \tan^{-1} \frac{1}{2} \mu$ .

63. Two hemispheres (centres  $A, B$  and weights  $W_1$  and  $W_2$ ) are placed with their rims on a rough horizontal table and in contact, and a rough sphere (centre  $C$  and weight  $W$ ) rests on them, of such a radius that  $ACB$  is a right angle. The system is on the point of moving: shew that the sphere will begin to slip over the larger hemisphere, whilst the larger or the smaller hemisphere will begin to slip according as

$$(W_1 - W_2) \sin \epsilon < \text{ or } > W \sqrt{2} \cos (\alpha + \pi/4) \sin (\alpha + \epsilon),$$

where  $\epsilon - \pi/4$  is the angle of friction, and  $\alpha$  is the angle  $CAB$ .

64. A cylindrical rod with hemispherical ends and another cylinder are in contact on a rough plane, the axis of the former is vertical, that of the latter horizontal. The radius of the horizontal cylinder is such that the other touches it at a point in the rim of its upper hemispherical end. The horizontal cylinder is gradually moved along the plane in a direction perpendicular to its axis, the two remaining in contact: shew that equilibrium is no longer possible unless  $\lambda$  be  $> \pi/4$ , and if  $\lambda$  be  $> \pi/4$ , equilibrium is impossible when the rod makes an angle  $> \theta$  with the vertical, where  $\theta$  is given by the equation  $h \cos \theta = h + (h + a) \cos 2\lambda$ .

Explain how the equilibrium is broken in this case.

$a$  = the radius of the hemispherical ends,  $2h$  = the length of the generating lines of the rod, and  $\lambda$  = the angle of friction, supposed the same everywhere.

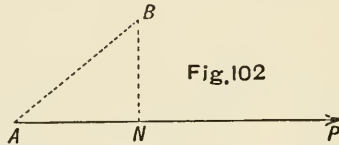


## CHAPTER VI.

### VIRTUAL WORK.

113. *Def.* If the point  $A$  at which a force  $P$  is acting be displaced to any point  $B$ , the distance  $AB$  is called the *displacement* of the point.

If from  $B$ ,  $BN$  be drawn perpendicular to  $P$ 's line of action, the product  $P \cdot AN$  is called the *work* done by



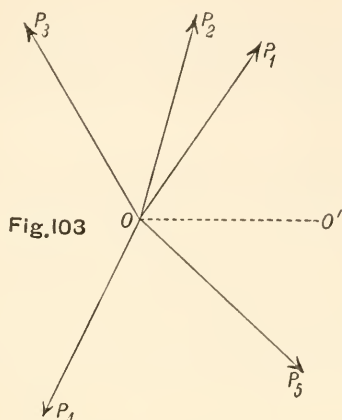
the force  $P$  during the displacement. If  $N$  falls on that side of  $A$  towards which  $P$  acts, the work is said to be positive, if on the other side, negative. We may say then that the product of the force into the projection of the displacement, along the direction of the force, gives the *algebraical* as well as the *numerical* value of the work done during the displacement.

If the displacement does not really take place but is only *imagined* to do so, it is said to be a *virtual displacement*, and the work which would be done during such a displacement is called the *virtual work*.

114. *Prop.* If a particle acted on by any system of forces receive any virtual displacement whatever, the algebraical sum of the virtual work done by the different forces during the displacement is equal to the virtual work done by the resultant.



Let  $O$  represent the actual position of the particle,  $O'$  the position to which it is supposed displaced ; let  $P_1, P_2,$



$P_3,$  &c., be the forces acting on the particle ;  $\theta_1, \theta_2, \theta_3,$  &c., the angles their directions make with  $OO'$ .

The A. S. of the virtual work done by  $P_1, P_2, P_3,$  &c.  
 $= P_1 \cdot OO' \cos \theta_1 + P_2 \cdot OO' \cos \theta_2 + P_3 \cdot OO' \cos \theta_3 + \dots$   
 $= OO' \cdot (P_1 \cos \theta_1 + P_2 \cos \theta_2 + \dots)$   
 $= OO' \times$  A. S. of the resolved parts of the forces in direction  $OO'$   
 $= OO' \times$  resolved part of the resultant in direction  $OO'$   
 $=$  projection of  $OO'$  along the direction of the resultant  $\times$  the resultant  
 $=$  the virtual work done by the resultant.

It should be observed that in the above proposition the displacement the particle receives is virtual, and entirely unrestricted both as regards magnitude and direction.

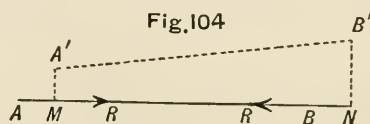
*Cor.* If a particle in equilibrium under the action of any system of forces receive any virtual displacement whatever, the A. S. of the virtual work done by the different forces is zero.

115. If a system of particles be in equilibrium under the action of external and internal forces, and any number of particles of the system receive any virtual displacements whatever, we have seen that the A. S. of the virtual work done by the forces on each particle is zero, and therefore the A. S. of the virtual work done by all the forces, external and internal, is zero.

*Prop.* If a system of particles in equilibrium under the action of any system of external forces together with internal forces, receive any indefinitely small virtual displacement whatever, which does not alter the configuration formed by the particles, the A. S. of the virtual work done by the *external forces alone* is zero, or more strictly speaking, is of an order higher than that of the virtual displacement.

In this proposition the displacements which the particles receive are much more restricted than in the corresponding theorem for a single particle: here the displacement must be indefinitely small, there it was unlimited in extent: the displacements, too, of the different particles are also so connected, that if the particles formed a rigid body, these displacements would not involve any alteration in its shape or size, but only an alteration of its position as a whole.

We shall first prove that if the displacements be of this character, the virtual work done by any internal force (the action exerted by  $B$ ) on the particle  $A$  is equal and opposite in sign to that done by the reaction exerted by  $A$  on the particle  $B$ . Let  $R$  be the action exerted by  $B$  on the particle  $A$ , along  $AB$  in the direction indicated, then



the reaction exerted by  $A$  on  $B$  is in the opposite direction. Let  $A'$ ,  $B'$  be the points to which  $A$ ,  $B$  are supposed dis-

placed, then by the conditions relating to the nature of the displacements, the angle ( $\theta$ ) between  $A'B'$  and  $AB$  is small, and the length  $A'B' = AB$ .

Draw  $A'M$ ,  $B'N$  perpendicular to  $AB$ .

Then  $MN = A'B' \cos \theta = A'B'$  ultimately,  $= AB$

$\therefore AM = BN$ .

The virtual work done by action  $R$  on  $A = R \cdot AM$ :  
that done by reaction  $R$  on  $B = -R \cdot BN = -R \cdot AM$ .

Hence the A.S. of the virtual work done by any action and the corresponding reaction is zero. But the internal forces consist entirely of pairs, each pair being made up of an action and the corresponding reaction: therefore the A.S. of the virtual work done by *all* the internal forces is zero, since that of each pair is so. We have seen too that the A. S. of the virtual work done by *all* the forces, both external and internal, is zero, so that that of the virtual work done by the external forces alone must be zero also.

In obtaining this result we have neglected quantities depending on the powers higher than the first of the displacement, so that strictly speaking the A. S. of the virtual work done by the external forces is not zero, but of an order higher than the first power of the displacement.

*Cor.* If in any system of forces in equilibrium there are two forces equal to one another, and acting in opposite directions along the straight line joining the particles on which they respectively act, the two forces will not enter into the equation of virtual work, provided the virtual displacements of the two particles produce no alteration in the length of the line joining them, or at any rate one of the second order only. Hence, if we have two bodies in contact, and the virtual displacement does not alter the points in contact, the action and reaction between the two bodies will not appear in the equation for the two bodies together. Also, if two particles are connected by an inextensible string or rod, and they receive displacements which do not involve breaking or bending the string

or rod, the tension of the string, or in the case of the rod, the tension or thrust, whichever it exerts, will not enter into the equation of virtual work for both particles. This may easily be extended to the case of two particles connected by an inextensible string which passes round a smooth fixed body: for the distance between them measured along the string is constant, so long as the string neither slackens nor breaks.

116. In applying the above proposition to the case of a rigid body, we may suppose the displacement any slight displacement of the body as a whole not involving any change of shape or size. If we wish to ascertain the internal forces between one portion of a body and another, we may suppose that the first portion is displaced as a whole, without any displacement of the remainder, in which case the actions of this last portion on the first will enter into the equation of virtual work.

In solving problems by the principle of virtual work, it is often convenient to make such a displacement that a force, whose magnitude we do not wish to ascertain, may not enter into the equation of virtual work. In that case the virtual work done by that particular force must be zero, or at any rate of a higher order in small quantities than the displacement. For that to be the case the particle on which the force acts must be virtually displaced in a direction making with the force, either a right angle or an angle differing from a right angle by an indefinitely small quantity.

In the following propositions, it is understood that the displacements are indefinitely small.

117. *Prop.* The work done by the tension of an inextensible string or rod, when one end is fixed and the other attached to a particle which is displaced so that the string or rod is neither broken nor bent, is ultimately of an order higher than the first.

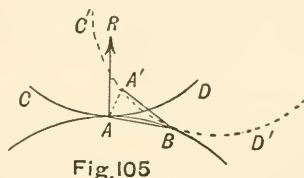
It is obvious that the particle can only move in a direction which is ultimately at right angles to the rod or string, i.e. at right angles to the tension.

*Prop.* If a rigid body resting in contact with any smooth curve or surface, receive a displacement by *sliding* along the curve or surface, the work done by the reaction of the curve or surface on the body is ultimately of an order higher than the first.

In this case the particle situate at the point of the body touching the curve or surface is the one on which the reaction acts, and this point moves along a tangent to the surface or curve, i.e. at right angles to the normal along which the reaction acts.

*Prop.* If a rigid body resting in contact with any surface, not necessarily smooth, receive a displacement by *rolling* along the surface, the work done by the reaction of the surface is ultimately of an order higher than the first.

Let  $A$  be the common point of the rigid body and the surface: let the body be rolled so that the point



originally at  $A$  comes to  $A'$ , and  $B$  becomes the point of contact.

Then the arcs  $AB$ ,  $A'B$  are small, and therefore the corresponding chords; also the angle between these chords is small, so that the base  $AA'$ , which is the displacement of  $A$ , is of a higher order than  $AB$ .

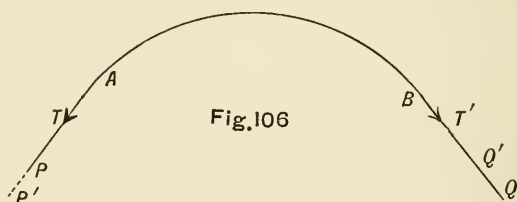
*Cor.* If the rigid body partly roll and partly slide along a smooth surface, it is clear that the displacement is compounded of the two displacements of rolling and sliding, and is therefore of an order higher than the first, since each of the latter is so.



We have already seen that if two bodies in contact receive such virtual displacements that their points of contact remain the same, the action and reaction between the two do not appear in the equation of virtual work for the two bodies: neither will they if in addition to these displacements one rolls along the other, or if the bodies be smooth, one slides or partly slides and partly rolls along the other. For either set of displacements alone will not bring these forces into the equation, therefore a combination will not do so.

118. As an illustration of the application of the principle of virtual work, we will by means of it prove the theorem proved in Art. 81, viz., that the tensions at the ends of a weightless string stretched over a smooth surface are equal.

Let  $A, B$  be the points where the string leaves the surface, and let  $T, T'$  be the tensions at the ends  $P, Q$  respectively.



We shall not interfere with the equilibrium of the string if we suppose it to lie in a groove cut in the surface, so that when pulled at one end, it must move along the groove. Let the virtual displacement which is given to the string be produced by pulling the end  $P$  in the direction  $AP$  to  $P'$ , so that the end  $Q$  must move along  $QB$  to a point  $Q'$  such that  $QQ' = PP'$ . As each portion of the string in contact with the surface moves at right angles to the action of the surface on it, no work is done by the actions of the surface on the string, and the algebraical sum of the virtual work done is  $T \cdot PP' - T' \cdot QQ'$ , which is therefore zero; i. e.  $T = T'$ , since  $PP' = QQ'$ .

Apply the principle of virtual work to the solution of the following examples:

Ex. 1. The algebraical sum of the moments about any point in their plane of a number of coplanar forces in equilibrium is zero.



Ex. 2. Two small rings of equal weight slide on a smooth wire in the shape of a parabola, whose axis is vertical and vertex upwards; they will be in equilibrium if connected by an inextensible string which passes over a smooth peg placed at the focus.

Ex. 3. Two equal uniform rods freely jointed at their ends rest, one on each, of two smooth pegs which are in a horizontal line. Shew that the inclination ( $\theta$ ) of either rod to the vertical is given by the equation

$$a \sin^3 \theta = c,$$

where  $a$  is the length of each rod, and  $c$  the distance between the pegs.

Ex. 4. Shew that in Ex. 27, page 94, the weight of each beam is proportional to the tangent of the angle, which the line joining the centre of the semicircle with the corresponding point of contact of the beam makes with the horizontal.

Ex. 5. Two equal uniform rods of the same material and thickness have two ends connected by a smooth hinge, and their other ends are attached to small rings which slide on a smooth horizontal wire. Find the position of equilibrium when a circular disc whose weight equals that of either rod, is placed between them so that each rod touches its circumference.

*Ans.* Each rod makes with the vertical the angle ( $\theta$ ) given by the equation  $2a \sin^3 \theta = r \cos \theta$ , where  $a$  is the length of a rod and  $r$  the radius of the disc.

Ex. 6. A tripod formed of three equal uniform rods, three ends being connected by a common joint, and the other three connected, each with the other two, by equal strings, rests with the joint uppermost on a smooth horizontal plane. Shew that the tension of each string is  $Wc/3h$ ,  $W$  being the weight of a rod,  $c$  the length of each string, and  $h$  the height of the joint above the plane.

Ex. 7. A heavy elastic string rests in the shape of a necklace round a smooth right circular cone whose axis is vertical: shew that its radius is  $a + wa^2/\lambda \tan \alpha$ , where  $\lambda$  is the modulus of elasticity,  $2\pi a$  the length of the string when unstretched,  $w$  its weight per unit length, and  $\alpha$  the semi-vertical angle of the cone.

119. We will now prove the converse of the principle of virtual work for a single particle, i.e. if the algebraical sum of the virtual work done by a system of forces acting on a particle, be zero for every displacement whatever, the particle is in equilibrium.

For let (fig. 103) the forces be  $P_1, P_2$  &c.,  $O$  the particle,  $OO'$  any virtual displacement,  $\theta_1, \theta_2$  &c., the angles  $P_1, P_2$ , &c. make with  $OO'$ . Then, since the algebraical sum of the virtual work done by the forces = 0,

$$\begin{aligned} P_1 \cdot OO' \cos \theta_1 + P_2 \cdot OO' \cos \theta_2 + \dots &= 0, \\ \therefore OO' (P_1 \cos \theta_1 + P_2 \cos \theta_2 + \dots) &= 0, \\ \therefore P_1 \cos \theta_1 + P_2 \cos \theta_2 + \dots &= 0, \end{aligned}$$

i.e. the algebraical sum of the resolved parts of the forces in any direction is zero, and the particle is therefore in equilibrium.

120.\* The material systems, to which the following propositions refer, are either single rigid bodies, or systems of rigid bodies, connected in such a manner by means of inextensible strings, smooth joints, &c., that the motion of one of them determines that of all of them.

*Prop.* A material system as above, under the action of a system of external and internal forces, such that for every indefinitely small virtual displacement whatever, which does not violate the geometrical conditions, the algebraical sum of the virtual work done by the external forces is of an order higher than the displacement, is in equilibrium.

For if the system be not in equilibrium, its motion is a definite one, which does not break the geometrical conditions: now we can conceive a number of smooth surfaces or inextensible strings so arranged, that they do not interfere with the actual motion of the system, but yet render it the only motion possible. If this be done, the whole system can be fixed by fixing one of the moving points in it, and this can be done by applying to it a force ( $F$ ) of sufficient magnitude, in the direction opposite to the point's motion, since that is the only direction in which the particle can move.

The system is now in equilibrium under the action of the original forces, the new forces of constraint and the

force  $F$ . If then any virtual displacement be given to it, the algebraical sum of the virtual work done by these forces is zero: let the displacement be the one which actually takes place, when  $F$  is not applied. In this case the new forces of constraint do no work, so that the algebraical sum of the virtual work done by the original forces and  $F$  is zero. But we know that the algebraical sum of the virtual work done by the original forces alone is zero; hence the virtual work done by  $F$  is also zero. But as the point on which  $F$  acts is one of the moving points of the system, its displacement is of the first order, so that  $F$  must be zero, i.e. the system is in equilibrium without  $F$ , and without the new forces of constraint.

121.\* *Prop.* A material system as above, under the action of external and internal forces, will, if held in any position, and then let go, move at first so that the algebraical sum of the work done by the external forces is positive, and of the first order of the actual displacement, provided the position is not one of equilibrium.

If the system is not in equilibrium, we can, as before, arrange a system of smooth surfaces, so that the actual motion is the only one possible, and this again can be entirely prevented by applying at one of the moving particles,  $A$ , say, of the system, a force, of sufficient magnitude  $F$ , in a direction opposite to that of  $A$ 's motion. The system being now in equilibrium we see as before, choosing the virtual displacement that which actually takes place, that the algebraical sum of the virtual work done by the original forces and  $F$  is zero.

But it is obvious, since  $A$  moves in the direction opposite to that of the force  $F$ , the work done by  $F$  is negative and of the first order; and therefore the algebraical sum of the virtual work done by the original forces is positive and of the first order of the displacement. The algebraical sum of the work actually done by the

original forces is therefore at first positive and of the first order of the actual displacement.

122. *Def.* The equilibrium of a body is said to be *stable*, when, on moving it slightly from its position of equilibrium, it returns to it; if it moves still further away from this position, its equilibrium is *unstable*. If the body remain in equilibrium, the equilibrium is *neutral*.

If a small ring slide on a smooth circular wire placed in a vertical plane, it will be found by experiment that there are two positions of equilibrium, one, the stable one, at the lowest point of the wire, and towards which it will readily return if moved away from it: the other, the unstable one, at the highest point, away from which it will move if disturbed ever so slightly, and in which it is found practically almost impossible to keep it. A uniform sphere resting on a smooth horizontal plane is an instance of a body in neutral equilibrium; for if it be rolled out of its position along the plane, it will neither return, nor, unless a velocity be given to it, move further away.

The positions of stable and unstable equilibrium of a body succeed one another alternately, i.e. there cannot be two positions of stable equilibrium without one of unstable equilibrium between them, and vice versâ. For a position of stable equilibrium is one to which the body tends to move when placed near it, so that if there are two such positions of a body, there must be a position between them such that, if the body be placed on one side of it, it will tend to move towards one of the above positions, and if placed on the other side, towards the other: i.e. there is a position of unstable equilibrium between them. Similarly we can shew, that there is a position of stable equilibrium between every two positions of unstable equilibrium.

123.\* *Prop.* When the only external forces acting on the material system of the last two propositions are the weights of the different particles which compose it, and the forces due to the geometrical constraints, such as the reactions of smooth surfaces and the tensions of inextensible strings, the system is in a position of stable or unstable



equilibrium, according as its centre of mass is at a maximum or minimum depth consistent with the geometrical conditions of constraint.

For the work done by gravity during any displacement is the algebraical sum of the products of the weight of each particle into its *vertical* displacement (the positive sign being given to the displacement when it is downwards, the negative when upwards): and this again is equal to the product of the weight of the whole system into the *vertical* displacement of its centre of mass. Also, during any displacement of the system, consistent with the geometrical conditions, gravity is the only force which does work. We have seen (Art. 121), that when not in equilibrium the system moves so that the work done by the forces is initially positive, i.e. in this case, so that the centre of mass moves downwards. Hence the system always tends to move initially, so that its centre of mass moves towards the adjacent position at a maximum depth and away from the adjacent position at a minimum depth; these positions succeed one another alternately, and it is clear that the former are positions of stable, and the latter of unstable equilibrium.

124.\* The cases considered above divide themselves into two classes: one, in which the centre of mass of the system is constrained to move along a certain *curve*, so that in any position, it is only free to move in *two* directions, opposite to one another; the other, in which the centre of mass is constrained to move on a certain *surface*, so that in any position, it is free to move in *any* direction in a certain plane, the tangent plane to the surface at the point. A rod with its ends compelled to move along fixed wires is an illustration of the first class, one placed inside a bowl is an illustration of the second class.

If there is a position of the system, such that for all possible small displacements from it, the depth of the centre of mass is *diminished*, that position will be a position of *absolutely* stable equilibrium; on the other hand, a

position, such that for all possible small displacements from it, the depth of the centre of mass is *increased*, is one of absolutely unstable equilibrium. A point then on the locus of the centre of mass, where the tangent line or plane is horizontal and below the adjacent points of the curve or surface, corresponds to a position of the system of absolutely stable equilibrium, when it is above the adjacent points, to one of absolutely unstable equilibrium.

If the locus of the centre of mass be a curve, it may be that there is a point on it, such that the tangent at it is horizontal, and cuts the curve there, i.e. the adjacent part of the curve on one side is above the tangent and that on the other side below it: in other words there may be a point of inflexion at which the tangent is horizontal. Such a position of the centre of mass corresponds to a position of equilibrium of the system, a position from which a displacement in one direction will bring about a tendency to return to it, in the other direction, a tendency to recede still further from it.

Again, when the locus of the centre of mass is a surface, the shape of the latter may be that of a saddle, or that of the ground at the top of a pass between two mountains; in this case a tangent plane to the ground at the top of the pass is horizontal, and has part of the surface above it and part below it. This position of the centre of mass corresponds to a position of equilibrium of the system, which is unstable for displacements of the centre of mass in the plane containing the tangent to the path over the pass, and stable for displacements in the plane at right angles to it.

125.\* A body  $BAC$  rests on a rough fixed body  $DAE$ , the surfaces near the point of contact  $A$  being spherical: it is required to determine whether, for displacements made by *rolling only*,  $BAC$  is in stable or unstable equilibrium.

Let  $o$ ,  $O$  be the centres of the spherical surfaces: we suppose that the common normal  $oAO$  is vertical.  $G$  the centre of mass of  $BAC$  will be situate in  $Ao$ .



Let  $BAC$  be displaced by rolling through a small angle so that it comes into the position  $B'A'C'$ ,  $G'$  and  $o'$  being

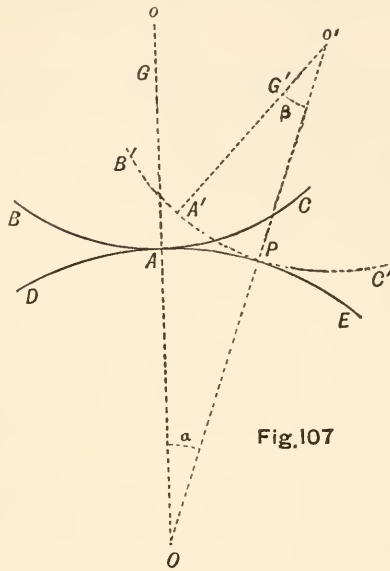


Fig. 107

the new positions of  $G$  and  $o$ ,  $P$  the point of contact of the two surfaces.

Let  $oA = r$ ,  $OA = R$ ,  $AG = h$ ,  $\angle AOP = \alpha$ , and  $A'o'P = \beta$ .

$\therefore$  the arc  $AP =$  the arc  $A'P$ ,  $R\alpha = r\beta$ .

Now the equilibrium is stable or unstable, according as  $G$  was originally at a maximum or minimum depth, i.e. according as  $G'$  is vertically above or below  $G$ ,

according as  $Oo' \cos \alpha - O'G \cos (\alpha + \beta)$  is  $\begin{matrix} > \\ < \end{matrix} OG$ ,

$$\dots\dots\dots (R + r) \cos \alpha - (r - h) \cos (\alpha + \beta) \text{ is } \begin{matrix} > \\ < \end{matrix} R + h,$$

$$\dots\dots\dots h \{1 - \cos (\alpha + \beta)\} \text{ is } \begin{matrix} < \\ > \end{matrix} r \{\cos \alpha - \cos (\alpha + \beta)\} \\ - R (1 - \cos \alpha),$$

according as  $h$  is  $\begin{cases} < \\ > \end{cases} \frac{r \cdot \sin \frac{\beta}{2} \cdot \sin \left( \alpha + \frac{\beta}{2} \right) - R \sin^2 \frac{\alpha}{2}}{\sin^2 \frac{\alpha + \beta}{2}},$

.....  $h$  is  $\begin{cases} < \\ > \end{cases} \frac{r\beta(2\alpha + \beta) - R \cdot \alpha^2}{(\alpha + \beta)^2}$  as  $\alpha$  and  $\beta$  are small,

.....  $h$  is  $\begin{cases} < \\ > \end{cases} \frac{rR(2r + R) - Rr^2}{(R + r)^2},$

.....  $\frac{1}{h}$  is  $\begin{cases} > \\ < \end{cases} \frac{R + r}{Rr}$  or  $\frac{1}{R} + \frac{1}{r}.$

This result is also easily obtained from the consideration, that  $BAC$  will return to its original position or not, according as  $G'$  lies nearer to  $Oo$  than  $P$  or further from it.

If the concavity of either surface be turned the other way we shall obtain the same result as before, except that the sign of the corresponding radius will be changed. If either surface be plane, its radius is of course infinity.

*Cor.* The above results hold for any curved surfaces, if  $R$  and  $r$  represent the radii of curvature of the sections made by the plane of displacement.

If  $\frac{1}{h} = \frac{1}{r} + \frac{1}{R}$ , the equilibrium is said to be *critical*, and we must proceed to a higher degree of approximation in order to determine whether the equilibrium is really *stable* or *unstable*.

Ex. 1. A body made up of a cone and a hemisphere having a common base, rests with the axis vertical on a rough horizontal table: determine the greatest height of the cone in order that the equilibrium may be stable. *Ans.* Height of cone =  $\sqrt{3}$  . radius of base.

Ex. 2. A prolate spheroid rests with its axis horizontal on a rough horizontal plane; shew that for rolling displacements in its equatorial plane the equilibrium is *neutral*, and for displacements in the vertical plane containing the axis, it is *stable*.

Ex. 3. A right circular cylinder of radius  $r$  rests with its axis horizontal on a fixed rough sphere (radius  $R > r$ ): shew that the equilibrium is stable or unstable, according as the plane in which the displacement takes place makes with the vertical one containing the axis of the cylinder an angle  $< \text{or} > \cos^{-1} \sqrt{(r/R)}$ .

Ex. 4. A prolate hemispheroid rests with its vertex on a rough horizontal plane, prove that the equilibrium is stable or unstable according as the eccentricity of the generating ellipse is less or greater than  $\sqrt{(3/8)}$ .

126.\* The material systems for which we have proved the preceding propositions have been either single rigid bodies, or rigid bodies connected in such a way that the position of one determined the positions of the others. We can however easily extend them to include the case of a system of rigid bodies so connected, that it is necessary to know the positions of a number of the bodies in order to know those of all.

*Prop.* If the algebraical sum of the virtual work done by the external forces be zero for all possible small virtual displacements consistent with the geometrical conditions, the above material system is in equilibrium.

For if it is not, it will have a definite motion consistent with the geometrical conditions, and without interfering with the actual motions of the bodies we can so arrange a number of smooth surfaces or inextensible strings, that these actual motions are the only ones possible: they need not however all take place, i.e. several of the bodies may move without all the others doing so, and fixing one of them will not of necessity fix all. In this case we can reduce the whole system to rest by fixing one moving point in each of the bodies, and this can be done by applying forces  $P, Q, R, \&c.$  of sufficient magnitude in the directions opposite to the actual motions of these points respectively. Now the whole system is in equilibrium under the action of the original forces, the new forces introduced by the smooth fixed surfaces &c., and the forces  $P, Q, R, \&c.$ : therefore, if the virtual displacements chosen be the actual

ones, the algebraical sum of the virtual work done by the original forces and  $P, Q, R, \&c.$  will be zero, because the virtual work done by the reactions of the smooth surfaces is zero. But it is obvious that the work done by each of the forces  $P, Q, R, \&c.$  is negative, since the particle on which it acts moves in the direction opposite to that of the force: the algebraical sum of the work done by the original forces is therefore positive, which is inconsistent with its being zero, as it is by supposition. Hence each of the forces  $P, Q, R, \&c.$  is zero, and the system is in equilibrium; and as the smooth surfaces or inextensible strings do not interfere with the actual motion in any way, their removal will not upset the equilibrium of the system.

*Cor.* We see from the foregoing, that when such a material system as the above is not in equilibrium in a particular position, under the action of given external forces, it will, if placed in that position and then released, move so that at first the algebraical sum of the work done by the external forces is positive. By reasoning as in Art. 123 the proposition there proved can be extended to the case of the material systems we have just been considering. Among these systems we can include a mass of liquid, or a heavy inextensible flexible string. In fact the propositions of Arts. 120—123 apply to all systems of bodies the internal forces among which can do no work, so long as the geometrical conditions are not violated: they will not however apply to those systems in which the internal forces are capable of doing work; for instance, systems in which the pressures of compressible fluids, the tensions of elastic strings, and the actions of rough surfaces are included among the internal forces. On the other hand there is no restriction on the nature of the external forces: they may consist of frictions, or the tensions of elastic strings, without affecting the validity of these propositions.

127.\* In a precisely similar way we could prove the much more general proposition still, that if any material

system whatsoever, under the action of any system of forces, be placed in any position and then released, it will, if not in equilibrium, move at first so that the work done by *all* the forces, internal as well as external, is positive.

128.\* *Def.* When the forces, internal as well as external, acting on a material system are such, that the algebraical sum of the work done by them, as the configuration of the system changes, depends only on the initial and final configurations and not on the paths the different bodies take, they are said to form a *conservative* system of forces.

*Def.* If any material system is acted on by a conservative system of forces, the algebraical sum of the work done by these forces, as the configuration of the system changes from any other to some standard configuration, is termed the *Potential Energy* of the system corresponding to the former configuration. It is generally convenient to take the standard configuration such, that the potential energy for every other configuration which is practically considered is positive.

129\*. *Prop.* When any material system is acted on by a conservative system of forces, it is in a position of *stable* equilibrium when its potential energy has a *minimum* value, and in a position of *unstable* equilibrium when its potential energy has a *maximum* value.

We have seen (Art. 127), that when the system is placed in any position, except one of equilibrium, and then released, it will move so that the algebraical sum of the work done by the forces is initially positive, i.e. it will move so as to diminish its potential energy. Hence it will move towards a position of minimum, and away from one of maximum, potential energy. The positions of maximum potential energy then are positions of unstable equilibrium and those of minimum potential energy of stable equilibrium.



The proposition proved in Art. 123 is a particular case of this theorem.

130. *Recapitulation.* We began by shewing that if a particle be in equilibrium, the total virtual work done by the forces acting on it, during any virtual displacement whatever, is zero. The same theorem is therefore true for any system of particles, when the *internal* as well as the *external* forces are taken into consideration; but if the virtual displacement is a small quantity of the first order, and the system of particles form a rigid body, and also in certain other cases; it was shewn that the total virtual work done by the *external forces alone* is a small quantity of the second order.

The converse theorem was then shewn to hold for single rigid bodies, and also for a system of rigid bodies, connected in certain ways. Also such a system will, if placed in any position, and then released, move so that the total virtual work done by the external forces during the initial small displacement is positive, unless the position is one of equilibrium. Hence followed the principle, that such a material system, when gravity is the only *active* force, is in stable or unstable equilibrium, according as its centre of mass is at a maximum or minimum depth consistent with the geometrical conditions. Similarly followed the more general theorem, that for any material system under the action of any *conservative* system of forces, stable positions are positions of minimum, and unstable positions of maximum, potential energy.

#### ILLUSTRATIVE EXAMPLES.

Ex. 1. Find the amount of work done in stretching an elastic string.

Let  $a$  be the natural length of the string,  $\lambda$  its modulus of elasticity; let  $x$  be the extension of the string.

Let the extension  $x$  be divided into  $n$ , an indefinitely large number, equal parts. When the length of the string is  $a + \frac{rx}{n}$ , the tension is

$\lambda \cdot \frac{r}{n} \cdot \frac{x}{a}$ , and therefore the work done in stretching it to  $a + \frac{r+1}{n} x$  lies

between  $\lambda \cdot \frac{r}{n} \cdot \frac{x}{a} \cdot \frac{x}{n}$ , and  $\lambda \cdot \frac{r+1}{n} \cdot \frac{x}{a} \cdot \frac{x}{n}$ ,

i.e. the total work done in stretching the string to the length  $x$

$$= \frac{\lambda x^2}{a} \cdot \sum_{n=1}^t \frac{1+2+3+\dots+(n-1)}{n^2} = \frac{\lambda x^2}{2a}.$$

Hence the work done in increasing the extension from  $y$  to  $x$  is  $\lambda(x^2 - y^2)/2a$ .

Ex. 2. Shew that the power necessary to move a cylinder of radius  $r$  and weight  $W$  up a plane inclined at angle  $\alpha$  to the horizon by a crowbar of length  $l$  inclined at an angle  $\beta$  to the horizon is

$$\frac{Wr}{l} \cdot \frac{\sin \alpha}{1 + \cos(\alpha + \beta)}.$$

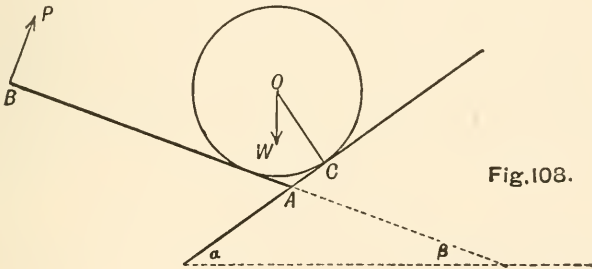


Fig. 108.

Let  $O$  be the point where the axis of the cylinder intersects the vertical plane containing the crowbar  $AB$ ;  $C$  the point where the same plane meets the generating line in contact with the inclined plane.

Let  $P$  be the force, which applied at  $B$  at right angles to  $AB$  will maintain equilibrium.

Let the virtual displacement be for  $AB$  to turn through a small angle  $\theta$ , so that its inclination to the horizon becomes  $\beta + \theta$ .

By Art. 117, the actions between the cylinder and crowbar and between each and the plane do not enter into the equation of virtual work.

The vertical height of  $O$  above  $A$  is  $AC \sin \alpha + OC \cos \alpha$ , i.e.

$$= r \left\{ \sin \alpha \cdot \tan \frac{1}{2} (\alpha + \beta) + \cos \alpha \right\} = r \cos \frac{1}{2} (\alpha - \beta) / \cos \frac{1}{2} (\alpha + \beta).$$

∴ neglecting the weight of the crowbar, the equation of virtual work is

$$P \cdot l \cdot \theta - W \cdot r \left( \frac{\cos \frac{\alpha - \beta - \theta}{2}}{\cos \frac{\alpha + \beta + \theta}{2}} - \frac{\cos \frac{\alpha - \beta}{2}}{\cos \frac{\alpha + \beta}{2}} \right) = 0.$$

$$\begin{aligned} \therefore P &= \frac{Wr}{l} \cdot \frac{\sin \alpha}{\cos \frac{\alpha + \beta}{2} \cdot \cos \frac{\alpha + \beta + \theta}{2}} \cdot \frac{\sin \frac{\theta}{2}}{\theta} \\ &= \frac{Wr}{l} \cdot \frac{\sin \alpha}{2 \cos^2 \frac{\alpha + \beta}{2}} \cdot \frac{\cos \frac{\alpha + \beta}{2}}{\cos \frac{\alpha + \beta + \theta}{2}} \cdot \frac{\sin \frac{\theta}{2}}{\theta} \\ &= \frac{Wr}{l} \cdot \frac{\sin \alpha}{1 + \cos(\alpha + \beta)}, \end{aligned}$$

since  $\theta^2$  and higher powers are neglected.

✂ Ex. 3. A straight uniform rod has smooth small rings attached to its extremities, one of which slides on a fixed vertical straight wire, and the other on a fixed wire in the shape of a parabola whose latus rectum equals twice the length of the rod, and whose axis coincides with the straight wire: prove that in the position of equilibrium (stable when the vertex is upwards) the rod will be inclined at an angle of  $60^\circ$  to the vertical. Which is the position of stable equilibrium when the vertex is downwards?

Let  $PQ$  be the rod,  $P$  being the point on the parabola. Let  $\theta$  be its inclination to the vertical,  $2a$  its length, and  $G$  its middle point.

Draw  $PN$  perpendicular to the axis  $AN$ .

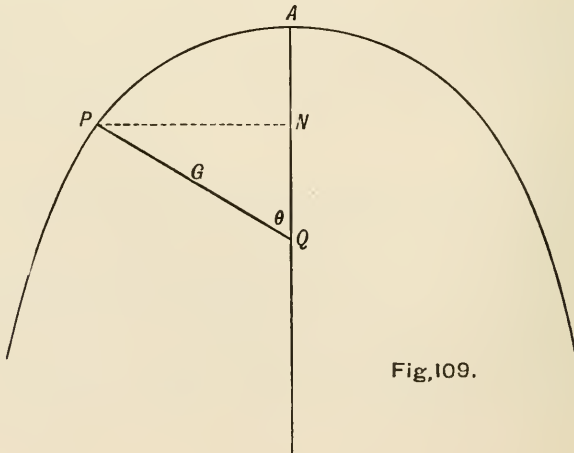


Fig. 109.

(1) When the axis is upwards, the depth of  $G$  below  $A$

$$\begin{aligned} &= AN + PG \cos \theta \\ &= \frac{PN^2}{4a} + a \cos \theta = \frac{4a^2 \sin^2 \theta}{4a} + a \cos \theta \\ &= a (1 + \cos \theta - \cos^2 \theta). \end{aligned}$$

The positions of equilibrium are given by the maximum and minimum values of this expression,

$$1 + \cos \theta - \cos^2 \theta = \frac{5}{4} - (\frac{1}{2} - \cos \theta)^2,$$

i.e. is a maximum when  $\cos \theta = \frac{1}{2}$  or when  $\theta = 60^\circ$ .

It is clearly a minimum when  $\theta = 0$ .

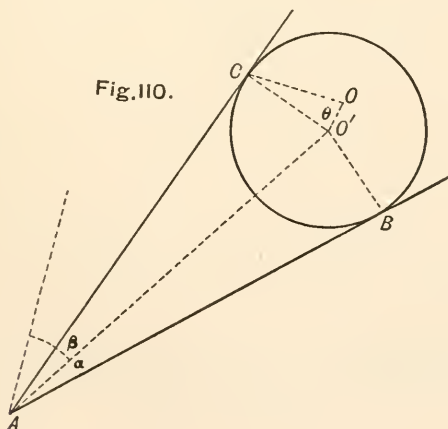
Hence  $\theta = 60^\circ$  corresponds to a position of stable equilibrium, and  $\theta = 0$  to one of unstable equilibrium.

(2) When the vertex is downwards  $\theta = 0$  corresponds to the position of stable, and  $\theta = 60^\circ$  to the position of unstable equilibrium.

Ex. 4. Two smooth rods which intersect at an angle  $2\alpha$  are placed so that they are equally inclined to the vertical, and the line bisecting the angle between them is inclined at an angle  $\beta$  to the vertical. Prove that a spherical ball of radius  $a$  will be in a position of unstable equilibrium, if the distance of its points of contact with the rods from the intersection of the rods be

$$\frac{a \cot \alpha \cos \beta}{\sqrt{(1 - \cos^2 \alpha \sin^2 \beta)}}.$$

Let  $O$  be the centre of the sphere,  $O'$  of the circle in which it is inter-



sected by the plane of the rods. Let  $B, C$  be the points where the rods  $AB, AC$  touch the sphere:  $\theta$  the angle  $CO'$  or  $BO'$  subtends at  $O$ .

Then  $OO' = a \cos \theta$ ,  $CO' = a \sin \theta$ ,  $AO' = a \sin \theta \cdot \operatorname{cosec} \alpha$ .

The vertical height ( $h$ ) of  $O$  above  $A$

$$\begin{aligned} &= AO' \cos \beta + OO' \sin \beta, \\ &= a (\sin \theta \operatorname{cosec} \alpha \cdot \cos \beta + \cos \theta \cdot \sin \beta). \end{aligned}$$

Let  $\cos \beta \operatorname{cosec} \alpha = r \cos \phi$ , and  $\sin \beta = r \sin \phi$ :

then  $h = ar (\cos \phi \sin \theta + \cos \theta \sin \phi) = ar \sin (\theta + \phi)$ .

Now the sphere is in a position of unstable equilibrium when  $h$  is a maximum, i.e. when  $\theta + \phi = \pi/2$ , i.e. when  $\theta = \cot^{-1} (\sin \alpha \tan \beta)$ .

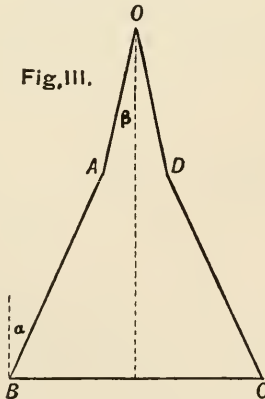
But  $AB = O'B \cot \alpha = a \cot \alpha \sin \theta$ ,

$$\therefore AB = \frac{a \cot \alpha}{\sqrt{(1 + \sin^2 \alpha \tan^2 \beta)}} = \frac{a \cot \alpha \cdot \cos \beta}{\sqrt{(1 - \cos^2 \alpha \sin^2 \beta)}}.$$

Ex. 5. Three equal heavy rods are connected by two hinges, a string is attached to the free ends and hung over a peg so that the middle rod is horizontal;  $\alpha$  is the angle which either of the other rods, and  $\beta$  the angle either part of the string, makes with the vertical. Prove that

$$2 \tan \alpha = 3 \tan \beta.$$

Let  $O$  be the peg,  $AB, BC, CD$  the rods.



Let  $2l$  be the length of the string, and  $a$  that of each rod.

The depth of the centre of mass of the whole below  $O$  is

$$l \cos \beta + \frac{2}{3} a \cos \alpha.$$



Since the algebraical sum of the horizontal projections of the sides of  $OABCD$  is zero,

$$2l \sin \beta + 2a \sin \alpha = 2a.$$

If the virtual displacement be such that the rod  $BC$  is moved vertically through a small distance, without interfering with any of the connections, no work is done by any of the forces except gravity, and therefore none is done by gravity; in other words, the displacement of the centre of mass is of the second order.

Let, in consequence of this displacement,  $\alpha$  become  $\alpha + \theta$ , and  $\beta$ ,  $\beta + \phi$ , then

$$l \cos \beta + \frac{2}{3}a \cos \alpha = l \cos (\beta + \phi) + \frac{2}{3}a \cos (\alpha + \theta),$$

and

$$l \sin \beta + a \sin \alpha = a = l \sin (\beta + \phi) + a \sin (\alpha + \theta),$$

$$\therefore l \sin \left( \beta + \frac{\phi}{2} \right) \sin \frac{\phi}{2} + \frac{2}{3}a \sin \left( \alpha + \frac{\theta}{2} \right) \sin \frac{\theta}{2} = 0,$$

and

$$l \cos \left( \beta + \frac{\phi}{2} \right) \sin \frac{\phi}{2} + a \cos \left( \alpha + \frac{\theta}{2} \right) \sin \frac{\theta}{2} = 0;$$

$$\therefore \tan \left( \beta + \frac{\phi}{2} \right) = \frac{2}{3} \tan \left( \alpha + \frac{\theta}{2} \right),$$

$$\therefore 3 \tan \beta = 2 \tan \alpha,$$

since  $\theta$  and  $\phi$  are indefinitely small.

Ex. 6. Four uniform thin heavy rods are freely jointed together at their extremities so as to form a parallelogram, and two opposite angular points of the frame so formed are connected by a light inextensible string; the system is suspended by another string attached to one of the same angular points: compare the tensions of the strings.

Let  $A$  be the point from which the frame is suspended,  $B$  the diagonally opposite point to which the string is attached.

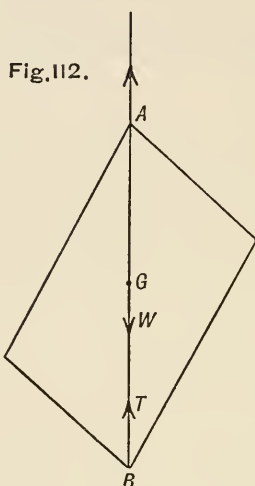
The centre of mass,  $G$ , is the middle point of  $AB$ , which is therefore vertical. Let the virtual displacement be such that  $B$  is moved vertically downwards through a small distance  $x$  without any separation of the rods at the joints.

By Art. 117, the only forces which occur in the equation of virtual work are  $T$ , the tension of the string  $AB$ , and  $W$  the weight of the four rods.

The equation is  $T \cdot x - W \cdot \frac{x}{2} = 0$ ;

$$\therefore T = \frac{1}{2}W,$$

i.e. the tension of the string  $AB$  is half that of the one which supports the whole framework.



The same reasoning would enable us to prove that the same relation holds when the framework of rods form the edges of a parallelepiped, or any figure, such that the centre of mass is always the middle point of the diagonal along which the string lies.

Ex. 7. Three equal particles, each of weight  $W$ , are fastened to an endless elastic string without weight, so as to be at equal distances from each other. The whole is then laid on a smooth sphere so that the string lies unstretched along a horizontal small circle of the sphere whose radius is  $\frac{2}{3}$  that of the sphere. Prove that the particles will be in equilibrium when the lines joining them subtend angles of  $60^\circ$  at the centre, the modulus of elasticity of the string being  $3W/2\sqrt{2}$ .

Let  $O$  be the centre of the sphere;  $A, B, C$  the positions of the particles when in equilibrium. Let  $H$  be the point where the vertical through  $O$  meets the plane  $ABC$ , which is from symmetry horizontal.

Let  $r$  = radius of the sphere. Let  $\phi$  be the angle which  $AB, BC$ , or  $CA$  subtends at  $O$ , and  $\theta$  the angle which  $OA, OB$ , or  $OC$  makes with  $OH$ .

$$\angle AHB = \angle AHC = \angle BHC = \frac{2}{3}\pi,$$

$$HA = r \sin \theta.$$

$$\begin{aligned} \therefore AB &= 2r \sin \theta \cdot \sin \frac{1}{3}\pi = \sqrt{3} \cdot r \sin \theta; \\ \therefore 2 \sin \frac{1}{2}\phi &= \sqrt{3} \cdot \sin \theta \dots\dots\dots(1). \end{aligned}$$

The original length of the string was  $\frac{3}{4}\pi r$ ; when stretched it is  $3r\phi$ .

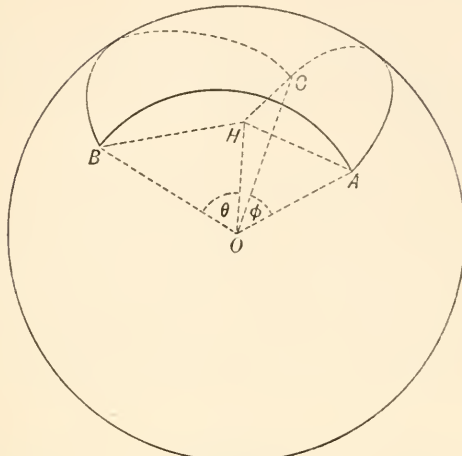


Fig. 113.

$T$ , the tension, therefore

$$= \frac{3r\phi - \frac{3}{4}\pi r}{\frac{3}{4}\pi r} \cdot \frac{3W}{2\sqrt{2}}, = \frac{3W}{2\sqrt{2}} \cdot \frac{4\phi - \pi}{\pi}.$$

Let the virtual displacement be such that all three particles descend through equal small distances, the consequent small increments in  $\theta$  and  $\phi$  being  $x$  and  $y$ . The equation of virtual work is then

$$\begin{aligned} 3Wr \{ \cos \theta - \cos (\theta + x) \} - T \cdot 3r \cdot y &= 0, \\ \therefore 2W \cdot \sin \left( \theta + \frac{x}{2} \right) \sin \frac{x}{2} - \frac{3W}{2\sqrt{2}} \cdot \frac{4\phi - \pi}{\pi} y &= 0, \\ \therefore x \sin \theta = y \cdot \frac{3}{2\sqrt{2}} \cdot \frac{4\phi - \pi}{\pi} \dots\dots\dots(2) \end{aligned}$$

From (1)  $2 \sin \frac{1}{2} (\phi + y) = \sqrt{3} \cdot \sin (\theta + x) \dots\dots\dots(3);$

$\therefore$  subtracting (1) from (3) we have

$$\begin{aligned} 2 \cos \left( \frac{\phi}{2} + \frac{y}{4} \right) \sin \frac{y}{4} &= \sqrt{3} \cdot \cos \left( \theta + \frac{x}{2} \right) \sin \frac{x}{2}, \\ \therefore y \cos \frac{\phi}{2} &= x \cdot \sqrt{3} \cdot \cos \theta \dots\dots\dots(4); \end{aligned}$$

eliminating  $x : y$  between (2) and (4),

$$\frac{3}{2} \sqrt{\frac{3}{2} \frac{4\phi - \pi}{\pi}} \cos \theta = \sin \theta \cos \frac{\phi}{2},$$

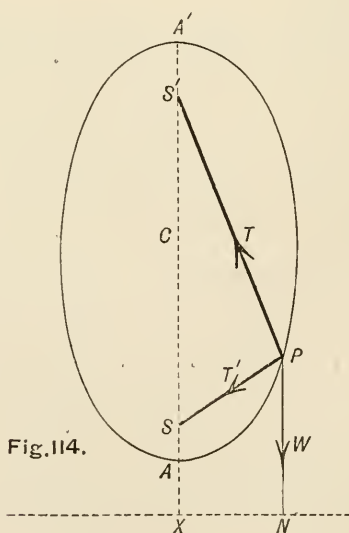
or substituting from (1)

$$\frac{3}{4} \sqrt{6} \cdot \frac{4\phi - \pi}{\pi} \sqrt{\left(3 - 4 \sin^2 \frac{\phi}{2}\right)} = 2 \cos \frac{\phi}{2} \sin \frac{\phi}{2} = \sin \phi.$$

This equation is satisfied by putting  $\phi = \frac{1}{3}\pi$ , and substituting in (1) we get a consistent value for  $\theta$ ; this value of  $\phi$  therefore corresponds to a position of equilibrium.

Ex. 8. A small ring slides on a smooth elliptic wire, whose axis is vertical: elastic strings connect it with each focus: the modulus of elasticity is half the weight of the ring: and either string is just unstretched when the ring is nearest the corresponding focus. Shew that in the unsymmetrical position of equilibrium the distance of the ring from the upper focus is equal to the distance of the centre from either directrix. Determine the nature of the equilibrium in the different positions.

Let  $P$  be any position of the ring,  $S', A'$  the upper focus and vertex,  $S, A$  the lower. Let  $W$  be the weight of the ring.



Let the system have its standard configuration (Art. 128) when the ring is at  $A$ . Then, the potential energy of the system when the

ring is at  $P$  is the total work done by the forces as the ring moves from  $P$  to  $A$ .

Draw  $PN$  perpendicular to the directrix  $NX$ . The potential energy of the system, when the ring is at  $P$ , is (Ex. 1, page 218),

$$\begin{aligned} W(PN - AX) &+ \frac{W}{2} \cdot \frac{SP^2 - SA^2}{2SA} - \frac{W}{2} \cdot \frac{S'A^2 - S'P^2}{2SA} \\ &= W \left\{ \frac{SP - a(1-e)}{e} + \frac{SP^2 + S'P^2 - a^2(1-e)^2 - a^2(1+e)^2}{4a(1-e)} \right\} \\ &= W \left\{ \frac{SP - a(1-e)}{e} + \frac{SP^2 - 2a \cdot SP + a^2(1-e^2)}{2a(1-e)} \right\} \\ &= W \frac{eSP^2 + 2a(1-2e)SP - a^2(1-e)(2-3e-e^2)}{2ae(1-e)} \\ &= W \frac{\left( SP - \frac{2e-1}{e}a \right)^2 - \frac{a^2}{e^2}(1-2e-e^2+2e^3+e^4)}{2a(1-e)}. \end{aligned}$$

The minimum value of this expression corresponds to  $SP = \frac{2e-1}{e}a$ ,

i.e.  $S'P = \frac{a}{e} = CX$ ; the maximum values correspond to the greatest and least values of  $SP$ , i.e. when  $P$  coincides with  $A$  and  $A'$ .

Hence the stable position of the ring is where its distance from  $S' = CX$ , and the unstable positions are  $A$  and  $A'$ . This supposes that there is a point  $P$  on the ellipse such that  $S'P = \frac{a}{e}$ , which will not be the case unless  $e$  be less than a certain quantity. If there is no such point, it is easily seen that  $A'$  is the position of unstable and  $A$  of stable equilibrium.

### EXAMPLES.

1. A heavy beam  $AB$  is moveable freely about the end  $A$  which is fixed; an elastic string is attached to  $A$ , passes through a fixed ring  $C$  vertically above  $A$  and is fastened to  $B$ .  $AC$  is equal to  $AB$ . Find the position of equilibrium. If the natural length of the string be  $AC$ , discuss the problem in the case when its modulus of elasticity is  $>$ ,  $=$ , or  $<$  half the weight of the beam.

2. A rhombus is composed of four equal rods jointed at their extremities. Two opposite corners are connected by an elastic string whose natural length is  $a\sqrt{2}$ ,  $a$  being the length of each rod, and the system stands in a vertical plane with one of the corners on a horizontal table. Find the angle between the rods.

3. A solid homogeneous hemisphere of radius  $a$  and weight  $W$  rests in apparently neutral equilibrium on the top of a fixed sphere of radius  $b$ . Prove that  $5a=3b$ . A weight  $P$  is now fastened to a point in the rim of the hemisphere. Prove that if  $55P=18W$ , it still can rest in apparently neutral equilibrium on the top of the sphere.

4. Two heavy rings slide on a fixed smooth parabolic wire whose axis is horizontal, and the rings are connected by a string which passes over a smooth peg at the focus. Prove that in the position of equilibrium the depths of the rings below the axis of the parabola are proportional to their weights. Is the equilibrium stable or unstable?

5. A prolate spheroid rests upon another equal and similar fixed spheroid, the point of contact being on the equatorial plane of each, their major axes being horizontal and at right angles to each other. Prove that the equilibrium will be stable for a displacement in a plane through either axis, if the upper spheroid be loaded at its lowest point with a weight bearing to its own weight a ratio greater than the duplicate ratio of its least and greatest diameters.

6. A uniform rod  $AB$  of length  $2a$  is freely moveable about  $A$ : a smooth ring of weight  $P$  slides on the rod and has attached to it a fine string which passes over a pulley at a height  $b$  vertically above  $A$  and supports a weight  $Q$  hanging freely; find the position of equilibrium of the system.

7. A cylinder rests in equilibrium with the centre of its base on the highest point of a fixed and perfectly rough sphere. The altitude and diameter of the base of the cylinder are each equal in length to a quadrant of a great circle of the sphere. Find the greatest angle through which the cylinder may be made to rock without falling off.

8. A wire in the form of an ellipse, whose semi-axes are  $a$  and  $b$ , is placed with its minor axis vertical. A light string of length  $a$  on which slides a ring of weight  $W$  has one end fastened to the centre, and the other to a ring of weight  $W'$ , which slides on the wire. Shew that, if there is no friction, there will be equilibrium if  $W'$  is anywhere on the upper half of the ellipse, and  $b/a = W/(W + 2W')$ .



9. Two particles are connected by a fine inextensible string and can move freely in a smooth cycloidal tube whose vertex is upwards, the string passing over the vertex. Prove that in equilibrium the arcual distances of the particles from the vertex must be inversely as their masses.

10. A heavy hemispherical bowl of radius  $a$  containing water rests on a rough inclined plane of angle  $\alpha$ , prove that the ratio of the weight of the bowl to that of the water cannot be less than  $\frac{2 \sin \alpha}{\sin \phi - 2 \sin \alpha}$ , where  $\pi a^2 \cos^2 \phi$  is the area of the surface of the water.

11. A parallelogram composed of jointed rods, each of length  $a$  and weight  $P$ , is hung up by one angle, and inside it is placed a circular disc of radius  $b$  and weight  $W$ . Prove that there will be equilibrium, when the inclination of the rods to the vertical is

$$\sin^{-1} \left\{ \frac{Wb}{2a(W+2P)} \right\}^{\frac{1}{3}}.$$

12. A lamina in the form of a rhombus made up of two equilateral triangles rests with its plane vertical between two smooth pegs in the same horizontal plane at a distance apart equal to a quarter of the longer diagonal: prove that either a side or a diagonal of the rhombus must be vertical, and that the stable position is that in which a diagonal is vertical.

13. A parallelogram  $ABCD$  formed of four uniform rods freely jointed at the corners has the side  $AB$  fixed horizontally, and the frame hangs in a vertical plane with the joint  $A$  attached by a light string of length  $l$  to the opposite joint  $C$ :  $AC$  is the shorter diagonal and  $\alpha$  the acute angle of the parallelogram: shew that the tension of the string is  $\frac{Wl}{2a} \cot \alpha$ , where  $a$  is the length of the fixed side and  $W$  the weight of the four rods.

14. A surface rests in contact with a perfectly rough fixed surface, the common normal at the point of contact making an angle  $\alpha$  with the vertical: prove that the equilibrium is stable or unstable, according as the distance of the centre of mass from the point of contact is less or greater than

$$\frac{\cos \alpha}{1/\rho + 1/\rho'},$$

where  $\rho, \rho'$  are the radii of the surfaces, supposed spherical at the point of contact.

15. A heavy body in the shape of a paraboloid of revolution placed on a rough horizontal plane, has its C. G. at the critical height: determine this height, and find the real nature of the equilibrium.

16. A thin straight rod is suspended by a fine inextensible string fastened to it at the two ends and passing over a fixed smooth peg. If the centre of gravity of the rod is not at its middle point, determine whether the equilibrium is stable or not.

17. A uniform rod of length  $c$  rests with one end on a smooth elliptic arc whose major axis is horizontal and with the other on a smooth vertical plane at a distance  $h$  from the centre of the ellipse: prove that, if  $\theta$  be the angle which the rod makes with the horizon and  $2a$ ,  $2b$ , the axes of the ellipse,  $2b \tan \theta = a \tan \phi$ , where  $a \cos \phi + h = c \cos \theta$ .

18. Two elastic strings are fastened at a fixed point  $P$  and pass through fixed smooth rings  $A$  and  $B$  such that  $PA$ ,  $PB$  are the natural lengths of the respective strings; the other ends of the strings are fastened to  $C$  and  $D$ , two points of a rigid lamina which is moveable in its plane about a fixed point  $O$ . If  $A$  and  $B$  are in the same plane as the lamina and if the angles  $COA$ ,  $DOB$  are supplementary and the system is in equilibrium, prove that the equilibrium will be neutral.

19. Twelve equal uniform rods form a cube having universal joints at each of its angles; shew that, if it be suspended by one of its angles, and be prevented from collapsing by a rod without weight forming a diagonal not passing through the point of suspension, the tension of the rod will be eighteen times the weight of one of the rods.

20. Two equal rods rigidly fastened at right angles to each other are placed over an ellipse whose plane is vertical and major axis horizontal; find the least length of the rods that the equilibrium may be stable.

21. A smooth fixed sphere supports a zone of very small equal smooth spherical particles and the whole is prevented from slipping off the sphere by an elastic ring occupying a horizontal circle of angular radius  $\alpha$ , shew that in the position of equilibrium the tension of the band is  $T$ , where  $2\pi T = W \tan \alpha$ , and  $W$  is the whole weight of the ring and particles together.

22. A uniform elliptic hoop is weighted at an extremity of its major axis by a weight equal to that of itself: shew that if it be placed on a smooth horizontal plane with its plane vertical, it will have two or four

positions of equilibrium according as its eccentricity is less or greater than  $2^{-\frac{1}{2}}$ . What is the nature of the equilibrium in the several positions?

23. Two similar uniform straight rods of lengths  $2a$ ,  $2b$  rigidly united at their ends at an angle  $\alpha$  rest over two smooth pegs in the same horizontal plane: prove that the angle which the rod  $2a$  makes with the vertical is given by the equation

$$c(a+b)\sin(2\theta-\alpha) = a^2\sin\alpha\sin\theta - b^2\sin\alpha\sin(\alpha-\theta),$$

$c$  being the distance between the pegs.

24. Three equal and in every way similar uniform rods  $AB$ ,  $BC$ ,  $CD$ , freely jointed at  $B$  and  $C$ , have small smooth weightless rings attached to them at  $A$  and  $D$ : the rings slide on a smooth parabolic wire whose axis is vertical and vertex upwards, and whose latus rectum is half the length of the three rods: prove that in the position of equilibrium, the inclination ( $\theta$ ) of  $AB$  or  $CD$  to the vertical is given by the equation

$$\cos\theta - \sin\theta + \sin 2\theta = 0.$$

Is the equilibrium stable or unstable?

25. A number of uniform thin rods, all equal and similar, are freely jointed together at their middle points, so that they form the generators of a right circular cone, symmetrically placed about the axis. Within the cone thus formed is placed a smooth sphere, and round the rods a smooth thin ring of the same weight and radius as the sphere. The whole is placed on a smooth horizontal plane, so that the ring is below and the sphere above the vertex of the cone; prove that the semi-vertical angle ( $\theta$ ) of the cone in one position of equilibrium is given by

$$2\sin\theta + \sin 2\theta = Pr/(P+W)a,$$

where  $W$  is the weight of the rods,  $P$  that of the sphere and ring together,  $2a$  the length of each rod, and  $r$  the radius of the ring or sphere. Determine the stress on any rod at the joint.

26.  $A$ ,  $B$ ,  $C$ ,  $D$  are four fixed points in the same horizontal plane, at the corners of a square whose semidiagonal is  $b$ .  $A'$ ,  $B'$ ,  $C'$ ,  $D'$  are the corresponding corners of a square plate of weight  $W$  and semidiagonal  $a$ . Four equal cords join  $AA'$ ,  $BB'$ ,  $CC'$ ,  $DD'$ . When the plate is hanging by the cords the distance between  $A'B'C'D'$  and  $ABCD$  is  $k$ . Shew that if a couple  $L$  about a vertical axis be applied to the plate so that it is turned through an angle  $\theta$ , then

$$L = Wab\sin\theta/\sqrt{(k^2 - 4ab\sin^2\frac{1}{2}\theta)}.$$

27. Two equal equilateral triangular laminae freely jointed together at their vertices are placed with their bases on a smooth horizontal table, and have their base angular points connected by two inextensible strings, one of which is equal in length ( $2a$ ) to a side of either triangle. Shew that the tension of the other string ( $2b$ ) is equal to

$$\frac{2a^2 W}{3(3a-b)^{\frac{3}{2}}(2a-b)^{\frac{1}{2}}},$$

$W$  being the weight of either triangle.

## CHAPTER VII.

### MACHINES.

131. It is frequently desirable that we should be able to counteract one force by another, differing from it in magnitude, point of application, or direction, or in all three. To enable us to do this we employ machines more or less complicated.

In Statics we suppose the machine to be in equilibrium under the action of the forces due to the geometrical conditions of constraint, the force at our disposal generally called the *Power*, and the force which we wish to counteract, generally called the *Resistance* or the *Weight*.

It is found practically that, when the power is just on the point of overcoming the weight, other resistances are called into play, owing chiefly to the friction between the different parts of the machine, and the imperfect flexibility of ropes: all these resistances oppose the power, so that the latter has to be greater than would be necessary, were the machine a perfect one. If the weight were on the point of overcoming the power, these resistances would assist the latter. It is usual to call the resistance or weight, which it is the object of the machine to enable us to overcome, the *useful* resistance, while the other resistances are called *wasteful* resistances. When we take these latter into consideration, we shall suppose that motion is just about to take place, and that the power is overcoming the useful resistance.

If motion just occurs, the work done by the power will equal that done against both the useful resistance and the wasteful ones; the former part of the work is termed *useful* and the latter *lost* work.

132. *Def.* When motion just takes place in a machine, the ratio of the useful work done to the whole work done in the same indefinitely short time is called the *efficiency* of the machine. It is of course desirable to have the efficiency as near unity as possible.

Let  $P$  denote the power,  $W$  the useful resistance, and  $W'$  the wasteful resistance.

If  $P$  move its point of application through a small distance  $s$ , and in consequence the work done against  $W$  be  $w$ , and that done against  $W'$  be  $w'$ , we have from the principle of virtual work,

$$Ps = w + w',$$

the efficiency then is  $w/(w + w')$ .

Let  $P_0$  be the force which would just move  $W$  were there no wasteful resistance, then  $P_0s = w$  by the principle of virtual work. Hence the efficiency  $= P_0s/Ps = P_0/P$ , or the efficiency is the ratio of the power, which would just move the weight were there no wasteful resistance, to the actual power required.

Unless otherwise stated, we shall suppose the machines perfect ones, i.e. with efficiency equal to unity.

133. The simple machines are,—the *Lever*, the *Wheel* and *Axle*, the *Pulley*, the *Inclined Plane*, the *Screw* and the *Wedge*. The principle of the wheel and axle is the same as that of the lever, and the screw and wedge are identical in principle with the inclined plane.

134. *The Lever.* This is a rigid rod, straight or curved, and free to turn about a fixed axis, which is called the *fulcrum*. The two parts into which the rod is divided by the fulcrum are called *arms*.



Levers are usually classified as follows. In the lever of the first class, the fulcrum is between the power and the weight: a poker where the bar of the grate is used as the fulcrum, and a pair of scissors are instances of it. In the second class, the weight is between the fulcrum and the power, as in a wheelbarrow, where the point of the wheel in contact with the ground is the fulcrum, or in an oar, where the blade in contact with the water is the fulcrum, and the resistance is applied at the rowlock. In levers of the third class, of which a pair of shears is an example, the power is between the fulcrum and the weight.

135. *The condition of equilibrium of a Lever.* As in Art. 74 we can shew that the necessary and sufficient condition of equilibrium of any body whatsoever, which is free to turn about a fixed axis, and under the action of any number of forces, is, that the algebraical sum of the moments of the forces about the fixed axis be zero. In the case of the simplest form of the lever the forces are generally only two, the power and the weight, acting in one plane, so that the condition of equilibrium becomes that the moment of  $P$  about the fulcrum should be numerically equal but of opposite sign to that of  $W$ .

This condition may also be easily found by the Principle of Virtual Work.

136. To determine the pressure on the fulcrum when the lever is in equilibrium.

Since the action of the fulcrum together with the power and the weight keeps the lever in equilibrium, the reaction on the fulcrum is obviously the resultant of the power and the weight. If, however, the lines of action of  $P$  and  $W$  are not in one plane, they do not reduce to a single resultant, and the pressure on the fulcrum is not a single force.

We shall assume that the lines of action of  $P$  and  $W$  are in one plane.

When the power and the weight are parallel, the reaction ( $R$ ) of the fulcrum ( $F$ ) is parallel to each of them ; and in a lever of the first class  $R = P + W$ ,

of the second class  $R = W - P$ ,

of the third class  $R = P - W$ .

When the lines of action of the power and weight are not parallel but meet in  $C$ , let  $A, B$  be their respective

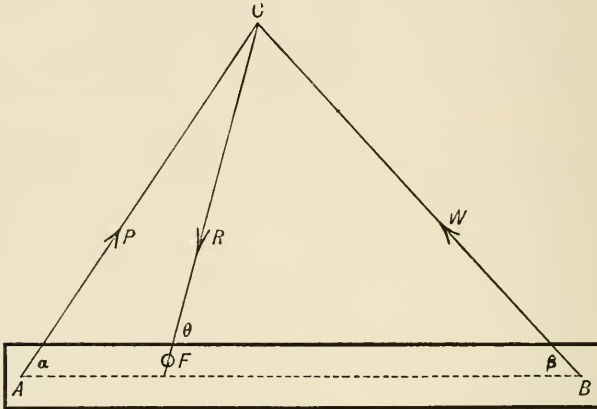


Fig. 115.

points of application,  $\alpha, \beta$  the angles, which their lines of action make with  $AB$ .

It is required to find the magnitude of  $R$ , and the angle ( $\theta$ ) its direction makes with  $AB$ .

Since the lever is in equilibrium under the action of the three forces,  $R$ 's line of action passes through  $C$ .

Also (Art. 18)  $\sin ACF : \sin BCF = W : P$  ;

$$\therefore \sin(\theta - \alpha) : \sin(\pi - \theta - \beta) = W : P ;$$

$$\therefore \frac{\sin \theta \cos \alpha - \cos \theta \sin \alpha}{\sin \theta \cos \beta + \cos \theta \sin \beta} = \frac{W}{P} ;$$

$$\therefore \tan \theta = \frac{W \sin \beta + P \sin \alpha}{P \cos \alpha - W \cos \beta} .$$

Also  $R^2 = P^2 + Q^2 + 2PQ \cos ACB$  ;

$$\therefore R = \sqrt{\{P^2 + Q^2 - 2PQ \cos(\alpha + \beta)\}} .$$

137. To find the relation between the Power and the Weight in a rough Lever, when the Power is on the point of moving the Weight.

Let  $A, B$  be the points of application of the power ( $P$ ) and the weight ( $W$ ) respectively: let their lines of action

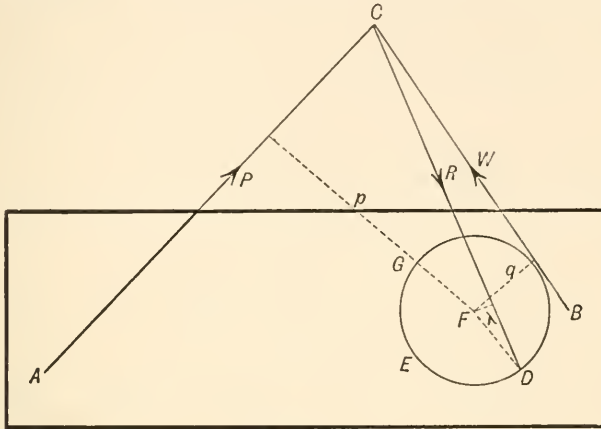


Fig. 116.

meet at  $C$  at an angle  $\theta$ . The fulcrum is a rough solid cylinder, which passes through a cylindrical hole in the lever, just so much bigger in diameter that there is contact along one generating line only.

Let the plane  $ABC$ , which we assume to be perpendicular to the axis of either cylinder, cut the hole in the circle  $DEG$  of radius  $r$  and centre  $F$ ,  $D$  being the point where the line of contact meets the circle. Join  $DC$ , then the reaction of the fulcrum ( $R$ ) acts along  $CD$ . Also, since the lever is on the point of turning round  $F$  in the direction in which  $P$  tends to turn it, the reaction  $R$  will make with the normal  $FD$  an angle equal to  $\lambda$ , the angle of friction, and on the side which enables it to assist  $W$ .

Let  $p, q$  be the perpendiculars from  $F$  on the lines of action of  $P, W$  respectively.

Since  $R$  counteracts  $P$  and  $W$ ,

$$R^2 = P^2 + W^2 + 2PW \cos \theta.$$

Also, by taking moments about  $F$ , we have

$$\begin{aligned} Pp &= Wq + Rr \sin \lambda \\ &= Wq + r \sin \lambda \cdot \sqrt{(P^2 + W^2 + 2PW \cos \theta)} \dots (1). \end{aligned}$$

If  $P$  could only just balance  $W$ , or, in other words, were  $W$  on the point of moving  $P$ , the relation would be

$$Pp = Wq - r \sin \lambda \cdot \sqrt{(P^2 + W^2 + 2PW \cdot \cos \theta)}.$$

138. To find the efficiency ( $E$ ) of the rough Lever.

Let  $P_0$  be the power just required to move  $W$ , when the fulcrum is perfectly smooth.

Then 
$$P_0 p = Wq.$$

But the efficiency, 
$$E = \frac{P_0}{P} = \frac{Wq}{Pp}.$$

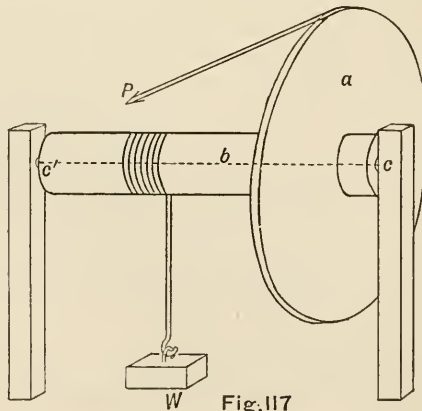
Therefore from (1) we have

$$1 = E + \frac{r \sin \lambda}{p} \cdot \sqrt{\left(1 + \frac{p^2 E^2}{q^2} + 2 \frac{pE}{q} \cos \theta\right)};$$

$$\therefore pq(1 - E) = r \sin \lambda \cdot \sqrt{(q^2 + p^2 E^2 + 2pq \cdot E \cdot \cos \theta)},$$

which gives us  $E$ .

139. *The Wheel and Axle.* This machine consists of a cylinder  $a$  (the wheel) with a groove cut round the circumference, and a cylinder  $b$  of smaller radius (the axle).



The two form one rigid body and have a common horizontal axis  $cc'$ , at the ends of which are two pivots  $c$  and  $c'$ , resting in fixed sockets so that the whole can turn about this axis.

The power  $P$  is applied tangentially at the circumference of the wheel, generally by means of a rope, while the weight is suspended by a rope which is wound round the axle so that it tends to turn the machine in the opposite direction to the power.

The apparatus for drawing a bucket of water out of a well is frequently a machine of this kind, the power being applied by means of a handle attached to the wheel instead of by a rope. A windlass for hauling up an anchor on board ship is a modification of the wheel and axle, in which the common axis is vertical, and the power is applied at the end of poles which project from the wheel so as to form radii produced.

The wheel and axle, as before stated, is a kind of lever, and we can shew as in Art. 74 that the condition of equilibrium is that the moment of  $P$  about the axis should be equal and opposite to the moment of  $W$ , i.e. that  $P \times$  the radius of the wheel =  $W \times$  radius of the axle.

Ex. 1. Four sailors, each exerting a force of 112 lbs., can just raise an anchor by means of a capstan whose radius is 1 ft. 2 in. and whose spokes are 8 ft. long (measured from the axis). Find the weight of the anchor. Ans.  $1\frac{2}{3}$  tons.

Ex. 2. If the length of each of a pair of sculls be 8 ft. 6 in., and the distance from the hand to the rowlock be 2 ft. 3 in., find the resultant force on the boat when the sculler pulls each scull with a force of 25 lbs., assuming that the blade does not move through the water. Ans. 18 lbs.

Ex. 3. A fly-wheel 10 ft. in radius weighs 15 tons, its axle is 6 in. in radius and revolves in bearings between which and it the coefficient of friction is  $\cdot 2$ : find the smallest weight which, hung from a band round the circumference of the wheel, will just turn it. Ans. 333 lbs. nearly.

140. *The Pulley.* A pulley-block consists of two plates, connected by an axis about which a circular disc, with a groove cut in its circumference, can turn. Rigidly connected with the axis is a hook to which a string can

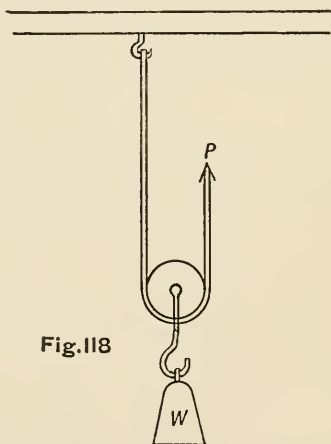
be attached so as to support the pulley, or by means of which the pulley can support a weight. Sometimes there are several discs, either turning about the same axis or placed one below another; they then form *double*, *treble*, &c. blocks.

When the block is fixed, the pulley is said to be *fixed*; otherwise it is called a *moveable* pulley.

A rope passes along the groove in the circumference of the disc, and, as the latter is supposed smooth, the tension of the rope will be the same on both sides the pulley.

If a *fixed* pulley be used to enable us to overcome resistance, the only object gained by the use of the pulley is that the force applied is enabled to counteract a force in a *different* direction, though of no greater magnitude.

When a *single moveable* pulley is used, the weight  $W$  is attached to the block, and the power  $P$  is applied at



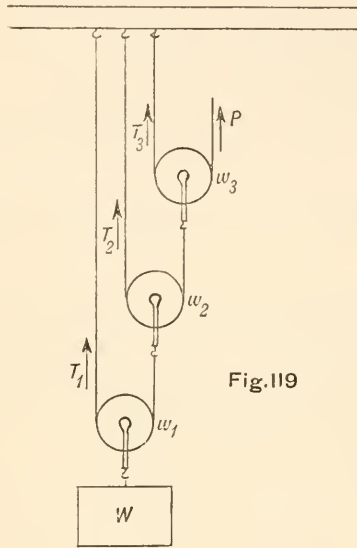
one end of a rope which passes under the disc of the pulley, the other end of the rope being fastened to a fixed point.

It is obvious, when the strings are parallel, that  $W = 2P$ , and when they are not parallel, but each makes an angle  $\theta$  with the vertical, that  $W = 2P \cos \theta$ .



141. There are three systems of pulleys usually described in text-books.

In the *first* system, the weight is attached to the lowest pulley, which is supported by a rope, one end of which is



attached to a fixed beam, and the other end to the next pulley above, which is in turn supported in a similar way: the power is applied at the end of the rope supporting the highest pulley. The portions of the ropes not in contact with the pulleys are vertical.

Assuming the ropes to be without weight, we can easily investigate the condition of equilibrium. Let there be  $n$  pulleys, whose weights in order from the lowest are  $w_1, w_2, \dots, w_n$ , and let the tensions of the ropes supporting them be  $T_1, T_2, \dots, T_n$ . Then from the equilibrium of the different pulleys, we have

$$2T_1 = W + w_1 \dots\dots\dots(1),$$

$$2T_2 = T_1 + w_2 \dots\dots\dots(2),$$

$$2T_3 = T_2 + w_3 \dots\dots\dots(3),$$

$$\dots = \dots\dots\dots$$

$$2T_n = T_{n-1} + w_n \dots\dots\dots(n),$$

also  $P = T_n \dots\dots\dots(n + 1).$

Multiplying equations (2), (3)...(n + 1) by 2, 2<sup>2</sup>, 2<sup>3</sup>,...2<sup>n</sup> respectively, and adding, we have

$$2^n \cdot P = W + w_1 + 2w_2 + 2^2w_3 + \dots 2^{n-1}w_n.$$

If the pulleys be without weight, this equation reduces to 2<sup>n</sup> · P = W.

We can deduce the same equation by the principle of virtual work.

Let the virtual displacement be the one which would actually be produced by moving the end of the rope to which P is applied through a small distance x in P's direction. By this, the uppermost pulley would be raised through a height  $\frac{x}{2}$ , the next lower pulley through a height  $\frac{x}{2^2}$ , and so on, the lowest pulley and weight being raised through a height  $\frac{x}{2^n}$ .

During this displacement, the actions of the fixed points to which the ends of the different ropes are attached do no work, nor is any done by the internal forces of the system (Art. 117). The equation of virtual work then is

$$P \cdot x - w_n \cdot \frac{x}{2} - w_{n-1} \cdot \frac{x}{2^2} - \dots - (W + w_1) \frac{x}{2^n} = 0,$$

i.e.  $2^n P = W + w_1 + 2w_2 + 2^2w_3 + \dots 2^{n-1}w_n.$

142. In the *second* system there are two pulley-blocks, the upper of which is fixed, and the lower moveable: a rope passes over one of the discs of the upper block and under one of the lower block alternately, the radii of the different discs being such that the portions

of the rope not in contact with a pulley are vertical, or nearly so. One end of the rope is attached to one of the

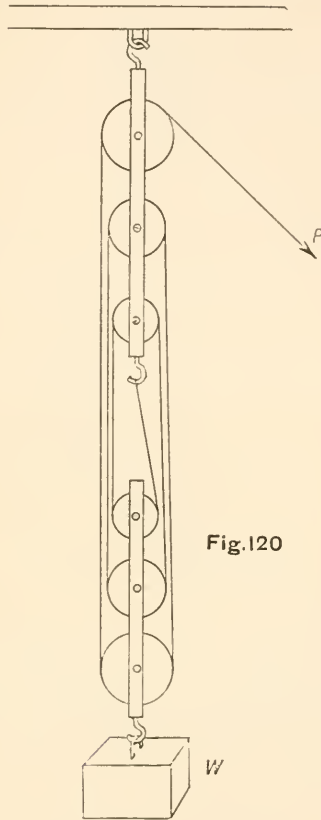


Fig. 120

two blocks, and at the other end the power is applied. The weight is attached to the lower block.

Let  $W$  be the weight to be raised, including that of the lower block: let  $P$  be the power which just raises it: then the tension of the rope is  $P$  throughout, and if there be  $n$  strings coming from the lower block, the total force exerted by them is  $nP$ , and we must have  $W = nP$ .

143. In the *third* system, the uppermost pulley is fixed: each pulley has a rope passing over it, with one end attached to the weight and the other to the pulley

next below. The power is applied at the end of the string passing over the lowest pulley.

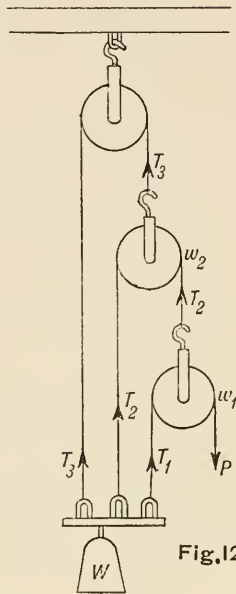


Fig. 121

In investigating the relation between the weight  $W$  and the power  $P$  which will support it, we shall suppose the portions of the ropes not in contact with the pulleys vertical, and the ropes to be without weight.

Let there be  $n$  pulleys, including the fixed one, and let  $w_1, w_2, w_3 \dots w_{n-1}$  be the weights of the moveable ones beginning with the lowest; let  $T_1, T_2 \dots T_n$  be the tensions of the ropes passing over them.

Since each pulley is in equilibrium, we have

$$T_2 = 2T_1 + w_1 \dots\dots\dots(1),$$

$$T_3 = 2T_2 + w_2 \dots\dots\dots(2),$$

... = .....

$$T_n = 2T_{n-1} + w_{n-1} \dots\dots\dots (n - 1),$$

from the equilibrium of the weight

$$T_1 + T_2 + T_3 + \dots T_n = W \dots \dots \dots (n),$$

also

$$T_1 = P.$$

Multiplying equations (1), (2) ... (n - 1) by  $2^{n-1}$ ,  $2^{n-2}$ ,  $2^{n-3}$  ... 2 respectively, and adding, we have

$$2T_n = w_1 \cdot 2^{n-1} + w_2 \cdot 2^{n-2} + \dots 2w_{n-1} + P \cdot 2^n.$$

Adding equations (1), (2) ... (n - 1), and employing equation (n), we have

$$W - P = 2 (W - T_n) + w_1 + w_2 + \dots w_{n-1}.$$

Eliminating  $T_n$ , we have

$$W = P (2^n - 1) + w_1 (2^{n-1} - 1) + w_2 (2^{n-2} - 1) + \dots w_{n-1} (2 - 1).$$

To deduce the relation between  $W$  and  $P$  from the principle of virtual work.

Let the weight  $W$  be supposed moved vertically downwards through a small distance  $x$ . Then the highest moveable pulley,  $w_{n-1}$ , will be raised through a height  $x$ : the next pulley below will be raised twice the height through which the highest is raised, together with the distance through which the weight descends, i.e. through a height  $3x$ . Similarly we can see that any pulley will rise through a height  $x$ , together with twice the distance through which the next pulley above rises. The distances therefore through which the weights  $w_{n-1}, w_{n-2} \dots w_1$ , are respectively raised are  $x, (2^2 - 1)x, (2^3 - 1)x, \dots (2^{n-1} - 1)x$ . Also the point of application of  $P$  will be moved vertically upwards through a distance  $(2^n - 1)x$ .

Hence the equation of virtual work is

$$W \cdot x - w_{n-1} \cdot x - (2^2 - 1) w_{n-2} \cdot x - (2^3 - 1) w_{n-3} \cdot x - (2^{n-1} - 1) w_1 \cdot x - (2^n - 1) P \cdot x = 0 ;$$

$$\therefore W = (2^n - 1) P + (2^{n-1} - 1) w_1 + (2^{n-2} - 1) w_2 + \dots (2^2 - 1) w_{n-2} + w_{n-1}.$$

Ex. 1. If there are three moveable pulleys arranged as in the first system, their weights beginning from the lowest being 9, 3, and 1 lbs. respectively, find what power will support a weight of 69 lbs. *Ans.* 11 lbs.

Ex. 2. If in the second system there are altogether nine pulleys and each pulley weigh one pound, what force will be required to support a weight of 86 lbs.? *Ans.* 10 lbs.

Ex. 3. If the weight supported in the third system be 56 lbs., and each moveable pulley, of which there are 3, weigh 1 lb., find the horizontal distance of the centre of mass of the weight from the centre of the fixed pulley, supposing the diameters of all the pulleys equal.

*Ans.*  $9/28$  the radius of any pulley.

144. *The Inclined Plane.* A line in the plane perpendicular to its intersection with the horizontal plane is called the *line of greatest slope*, and the vertical plane containing this line the *principal plane*.

To find the condition of equilibrium on an inclined plane, where  $W$  is the weight and  $P$  the power.

(i) When the plane is *smooth*.

Let  $BAC$  be a section of the inclined plane made by a principal plane,  $BA$  being the line of greatest slope and

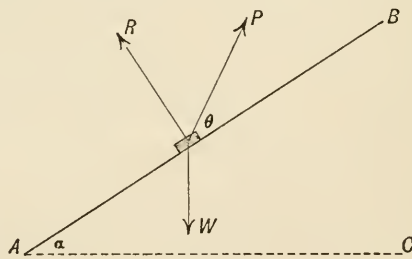


Fig. 122.

$AC$  being horizontal. Let  $\alpha$  = the angle of inclination  $BAC$ .

The reaction  $R$  of the plane acts at right angles to the plane and therefore parallel to the plane  $BAC$ : the weight  $W$  acts parallel to this plane also, so that the power  $P$  must also act parallel to this plane. Let  $\theta$  be the angle which  $P$ 's line of action makes with  $AB$  mea-



sured up the plane,  $\theta$  being positive when  $P$ 's direction is above the plane.

By Art. 18,

$$\begin{aligned} P : W : R &= \sin (W, R) : \sin (R, P) : \sin (P, W) \\ &= \sin \alpha : \cos \theta : \cos (\alpha + \theta). \end{aligned}$$

$P$  clearly has its least value for a given value of  $W$  when  $\theta = 0$ .

(ii) When the plane is *rough*, and the direction of  $P$  is in the principal plane.

The total reaction  $R$  of the plane will act in the principal plane, since  $W$  and  $P$  do; its direction cannot

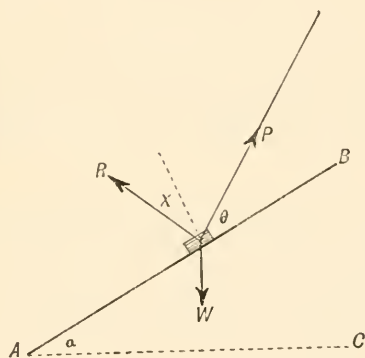


Fig.123

make with the normal an angle greater than  $\lambda$ , the angle of friction, but may make any smaller angle.

Let  $\lambda'$  be the angle which  $R$  makes with the normal,  $\lambda'$  being measured towards the lower part of the plane.

We have then the equations

$$\begin{aligned} R^2 &= P^2 + W^2 + 2PW \cdot \cos \left( \theta + \frac{\pi}{2} + \alpha \right) \\ &= P^2 + W^2 - 2PW \sin (\theta + \alpha), \end{aligned}$$

and 
$$\frac{P}{W} = \frac{\sin\left(\frac{\pi}{2} - \lambda' + \frac{\pi}{2} - \alpha\right)}{\sin\left(\lambda' + \frac{\pi}{2} - \theta\right)} = \frac{\sin(\alpha + \lambda')}{\cos(\theta - \lambda')},$$

to determine  $R$  and  $\lambda'$ .

When  $P$  is just on the point of moving  $W$  so that the latter is just about to slip up the plane, the total reaction will make with the normal an angle  $\lambda$  on the side towards the lower part of the plane: in that case

$$P = W \cdot \frac{\sin(\alpha + \lambda)}{\cos(\theta - \lambda)}.$$

Also 
$$R = W \cdot \frac{\cos(\alpha + \theta)}{\cos(\theta - \lambda)}.$$

The value of  $\theta$  which will give the least value of  $P$  for a given value of  $W$  is  $\lambda$ ; i.e. for  $P$  to be most effective it should make with the plane an angle equal to the angle of friction.

By changing the sign of  $\lambda$  in the preceding investigation we can obtain the value of  $P$  which will just prevent  $W$  from slipping down the plane, when the reaction  $R$  will make an angle  $\lambda$  on the other side of the normal. This gives us

$$P = W \cdot \frac{\sin(\alpha - \lambda)}{\cos(\theta + \lambda)},$$

and 
$$R = W \cdot \frac{\cos(\alpha + \theta)}{\cos(\theta + \lambda)}.$$

(iii) When the plane is *rough* and  $P$ 's direction does not lie in the principal plane.

Let  $P$  make with the plane an angle  $\theta$ , and let its resolved part along the plane make an angle  $\phi$  with the line of greatest slope drawn up the plane. Let the reaction  $R$  of the plane be resolved into  $R \cos \lambda'$  along the

normal, and  $R \sin \lambda'$  along the plane, the latter making an angle  $\beta$  with the line of greatest slope. Resolving the

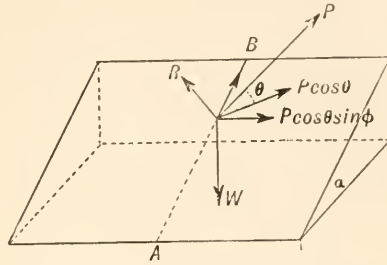


Fig. 124

forces at right angles to the plane, along the line of greatest slope, and in the plane at right angles to the line of greatest slope, we have

$$P \sin \theta + R \cos \lambda' - W \cos \alpha = 0,$$

$$P \cos \theta \cos \phi + R \sin \lambda' \cos \beta - W \sin \alpha = 0,$$

$$P \cos \theta \sin \phi + R \sin \lambda' \sin \beta = 0.$$

These equations are sufficient to determine  $R$ ,  $\lambda'$  and  $\beta$ , when the other quantities are known.

If  $P$  be on the point of moving  $W$ , the reaction  $R$  makes with the normal an angle  $\lambda$ , so that writing  $\lambda$  for  $\lambda'$  in the above equations, they enable us to determine  $P$ ,  $R$  and  $\beta$ , when the other quantities are known.

145. *The Screw.* A screw may be supposed constructed as follows:—

Let  $aa'd'd$  be a solid right circular cylinder, and let  $AA'D'D$  be a rectangle, whose breadth  $AA'$  is equal to the circumference of the cylinder. Draw  $BB'$ ,  $CC'$ ,  $DD'$  &c. parallel to  $AA'$  and at equal distances from one another: join  $AB'$ ,  $BC'$ ,  $CD'$ . Now let the rectangle  $AD'$  be supposed wrapped round the cylinder, so that the sides  $ABCD$ ,  $A'B'C'D'$  coincide with the generator  $ad$ , the points  $A, A'$  coinciding in  $a$ ,  $B, B'$  in  $b$ ,  $C, C'$  in  $c$ , and  $D, D'$

in  $d$ . The lines  $AB'$ ,  $BC'$ ,  $CD'$  will now form a con-

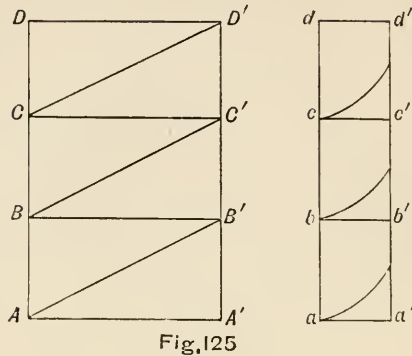


Fig. 125

tinuous line going round the cylinder, called a *helix*. It is clear that in wrapping the rectangle round the cylinder, we have not altered the inclination to  $A'B'$  of any of the lines  $AB'$ ,  $BC'$ ,  $CD'$ , so that the helix everywhere makes the angle  $B'AA'$  with the base of the cylinder. This angle is called the *pitch* of the helix; and it is equal to

$$\tan^{-1} \frac{AB}{AA'}$$

or  $\tan^{-1} \cdot \frac{\text{distance between two consecutive coils } (ab)}{\text{circumference of the cylinder}}$ .

Now imagine a solid figure generated by a small rectangle  $abcd$ , which moves so that one side  $ad$  always coincides with a generating line, while a corner  $a$  describes the helix, and its plane always contains the axis of the cylinder. Each point in  $ab$  will describe a helix, the pitch of the helix being smaller the further the point is from  $a$ : the distance between two consecutive coils will be the same for all, but the circumference of the cylinder round which any particular helix would wrap being greater the further the generating point is from  $a$ .

This thread is called a *square* one: an *angular* thread is sometimes generated by an isosceles triangle  $abc$ , whose plane always contains the axis of the cylinder, and whose

base  $ab$  moves exactly as the side  $ad$  of the rectangle  $abcd$  which generates the square thread.

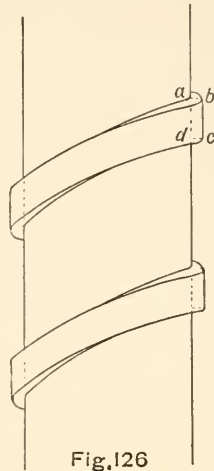


Fig.126

The solid cylinder, together with the solid figure above described, form a solid screw, which works in a hollow cylinder of the same diameter as the solid one, and with a groove cut in it, which just fits the thread of the solid screw. The hollow screw is generally fixed in a support.

The screw is generally used as follows:—

The solid screw has at one end an arm at right angles to the axis: the power  $P$  is applied at the end of this arm

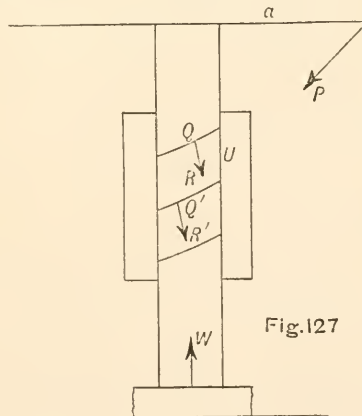


Fig.127

and perpendicular to it, so as to tend to turn the screw round and so move it in the direction of its axis, and thus produce pressure on any body situate at the end of the axis: the pressure which is thus overcome is called the weight ( $W$ ).

146. To find the condition of equilibrium in a screw with a square thread.

Let  $a$  be the length of the arm, at the end of which the power  $P$  acts:  $h$  the distance between two consecutive threads. The surface of the groove of the hollow screw will exert pressures perpendicular to the surface of the thread at a very large number of points. Let  $R$  be the resistance at one of these points  $Q$ , which is at a distance  $r$  from the axis of the screw: we have seen that the pitch ( $\alpha$ ) of the helix, which passes through this point, and has as axis the axis of the screw, is  $\tan^{-1} h/2\pi r$ . The direction of  $R$  is normal to the surface of the thread at  $Q$ , and therefore to any line in that surface, passing through  $Q$ . From the way in which the surface of the thread has been generated,  $R$  must be at right angles to the line from  $Q$  perpendicular to the axis of the screw; it must also be at right angles to the tangent to the helix through  $Q$ , i.e. it makes an angle  $\alpha$  with the axis of the screw. We may resolve  $R$  into two components, one along the axis of the screw,  $R \cos \alpha$ , and the other  $R \sin \alpha$ , perpendicular to the axis, and at a distance  $r$  from it. Similarly all the resistances, such as  $R$ , can be resolved in the same way.

Resolving along the axis, we have

$$W = \Sigma (R \cos \alpha).$$

Taking moments about the axis,

$$Pa = \Sigma (Rr \sin \alpha).$$

But

$$2\pi r \sin \alpha = h \cos \alpha;$$

$$\therefore Pa = \Sigma \left( \frac{Rh \cos \alpha}{2\pi} \right) = \frac{h}{2\pi} \Sigma (R \cos \alpha) = \frac{Wh}{2\pi},$$



$$\therefore \frac{W}{P} = \frac{2\pi a}{h}$$

$$= \frac{\text{circumference of circle traced out by end of } P\text{'s arm}}{\text{distance between two consecutive threads}}$$

We can easily deduce the same relation for a screw with any smooth thread, square or angular, from the principle of virtual work, by a method similar to that used in Art. 155.

Ex. A smooth screw makes three revolutions while it advances half an inch, find the power which must be applied at the extremity of an arm one foot long in order to produce a pressure of 144 lbs. *Ans.* 32 lbs.

147. When the screw thread is not smooth, we can find the condition of equilibrium, if we assume that the breadth of the thread, i.e. the side  $ab$  of the rectangle which is supposed to generate it, is very small. The pitch of the screw will be the same then at every point of the thread: let it be  $\alpha$ .

Let us suppose that the power ( $P$ ) is just on the point of moving the weight  $W$ , then the limiting friction is called into play at every point of contact of the thread with the groove, and acts in the direction in which it can most efficiently oppose  $P$ , i.e. directly opposite to that in which the point of the thread is about to move: it makes then an angle  $\frac{1}{2}\pi - \alpha$ , with the axis of the screw, and is perpendicular to the line drawn from its point of application at right angles to the axis. Let  $\lambda$  be the angle of friction,  $R_1, R_2, R_3 \dots$  the normal reactions at the different points of contact;  $r$  the distance of each of them from the axis of the screw.

Resolving along the axis of the screw, we have

$$W - \Sigma (R \cos \alpha) + \Sigma (R \tan \lambda \sin \alpha) = 0,$$

taking moments about the axis,

$$Pa - \Sigma (Rr \sin \alpha) - \Sigma (Rr \tan \lambda \cos \alpha) = 0.$$

But 
$$r \sin \alpha = \frac{h \cos \alpha}{2\pi},$$

$$\therefore W = (\cos \alpha - \sin \alpha \tan \lambda) \Sigma(R) = \frac{\cos(\alpha + \lambda)}{\cos \lambda} \Sigma(R),$$

and 
$$Pa = \left( \frac{h \cos \alpha}{2\pi} + \frac{h \tan \lambda \cos^2 \alpha}{2\pi \sin \alpha} \right) \Sigma(R)$$

$$= \frac{h \cot \alpha}{2\pi} \cdot \frac{\sin(\alpha + \lambda)}{\cos \lambda} \cdot \Sigma(R),$$

$$\therefore \frac{P}{W} = \frac{h}{2\pi a} \cdot \frac{\tan(\alpha + \lambda)}{\tan \alpha}.$$

When  $W$  is on the point of overcoming  $P$ , the relation becomes

$$\frac{P}{W} = \frac{h}{2\pi a} \cdot \frac{\tan(\alpha - \lambda)}{\tan \alpha}.$$

Since the power ( $P_0$ ) which would just move  $W$ , when the screw is smooth is  $Wh/2\pi a$ , the efficiency of the rough screw is  $= \tan \alpha / \tan(\alpha + \lambda)$ .

148. The *wedge*, which is a solid prism, whose section is an isosceles triangle, and which is used to split wood, &c., by being driven in by blows of a hammer, is so essentially dynamical in principle, that we shall not discuss it here.

149. Besides its use as an instrument for multiplying Force, the Lever is employed for weighing purposes: in one form it is known as the *Common Balance*.

This in its simplest form consists of a straight uniform beam  $AB$ , from the two ends of which scale-pans hang. The lever turns about a fulcrum  $C$ , which is situated above it in a short beam  $CD$ , which projects at right angles to  $AB$ , from its middle point  $D$ .

The substance to be weighed is placed in one scale-pan, and such weights in the other, that the beam is horizontal when in equilibrium.

In well-constructed balances for accurate weighing the fulcrum is formed by the edge of a triangular prism of hardened steel (a knife-edge),

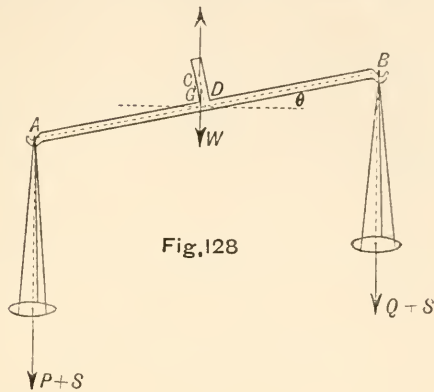


Fig. 128

which rests on a plate of smooth agate. Hence (Art. 137) the effect of friction is rendered very small.

Fig. 128, like the other figures of the machines, is not intended as a *realistic* representation. It is assumed that the student is familiar with the actual forms of the simple machines.

150. A good Balance should have the following requisites.

(1) It should be *true*, i.e. when loaded with equal weights, the beam should be horizontal. This requisite is obtained by making the scale-pans of equal weight, and the two arms exactly the same in weight, length and sectional area. We can easily test the *Truth* of a Balance by interchanging the weights, which keep the beam in equilibrium, when horizontal: if the beam settles again into a horizontal position, the weights are equal and the balance *true*, but not otherwise.

(2) A Balance should be *sensible*, i.e. when the weights differ by a small quantity the deviation of the beam from the horizontal should be easily perceptible.

To ascertain how to secure this requisite, we must find the position of equilibrium when the balance is loaded with weights  $P$  and  $Q$ .

Let  $G$  be the centre of mass of the lever, not including the scale-pans,  $W$  its weight. Let  $AB = 2a$ ,  $CD = h$ ,  $CG = k$ . Let  $S$  be the weight of each scale-pan acting through  $A, B$  respectively. Then if  $\theta$  be the angle which  $AB$  makes with the horizontal when  $P$  is placed in the scale-pan hanging from  $A$  and  $Q$  in the other, we have, by taking moments about  $C$  for the equilibrium of the beam,

$$(P + S)(a \cos \theta - h \sin \theta) - (Q + S)(a \cos \theta + h \sin \theta) - Wk \sin \theta = 0,$$

$$\therefore \tan \theta = \frac{(P - Q)a}{(P + Q + 2S)h + Wk}.$$

For a given value of  $P - Q$ , the sensibility will be the greater, the greater  $\tan \theta$  is, and for a given value of  $\theta$ , the sensibility is the greater, the smaller  $P - Q$  is, so that we may take  $\frac{\tan \theta}{P - Q}$  as a measure of the sensibility.

Hence the second requisite is best obtained by making  $\frac{a}{(P + Q + 2S)h + Wk}$  very large, i.e. by making  $a$  large in comparison with  $h$  and  $k$ .

(3) A good balance should be *stable*, i.e. it should readily return to its position of equilibrium, when moved from it, i.e. its time of oscillation about its position of equilibrium should be small. It is shewn in works on Rigid Dynamics that the time of oscillation is small when the arm  $a$  is small compared with  $h$  and  $k$ , so that the conditions of sensibility and stability are at variance one with another.

In making a balance, however, consideration is paid to the sort of weighing it is required for. In scientific measurements, where the greatest accuracy is desired, the third requisite is sacrificed to obtain the second; but for ordinary commercial purposes, where it is more necessary to save time than to be very accurate, the reverse is the case.

The stability is often measured by the sum of the moments of the forces which tend to bring back the beam into its position of equilibrium, but it is obvious that the time required to do this, and therefore the stability, will depend on the mass to be moved and on its shape, as well.

151. *The Common Steelyard.* This is a lever used as a balance, in which the necessity of keeping a number

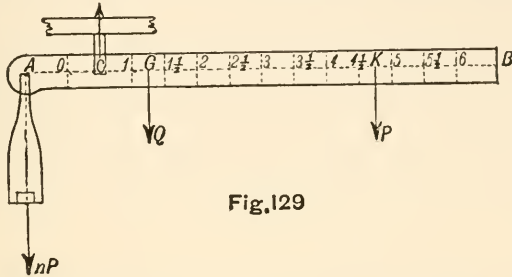


Fig. 129

of weights is obviated. It consists of a straight beam  $AB$ , which is free to turn about a fulcrum  $C$ . The weight to be ascertained is placed in a scale-pan, which hangs from the end  $A$ . A fixed moveable weight slides along the beam, which is graduated so that the graduation at which the moveable weight is situated, when the beam rests in a horizontal position, gives the required weight.

To shew how the graduations are obtained.

Let  $P$  be the moveable weight,  $Q$  that of the beam and scale-pan,  $G$  the point of the beam through which  $Q$  acts.

Let  $K$  be the position of the graduation  $n$ , i.e. the position  $P$  occupies when there is a weight  $nP$  in the scale-pan, and the beam balances in a horizontal position. Taking moments about  $C$ , we have

$$nP \cdot AC - Q \cdot CG - P \cdot CK = 0.$$

Putting  $n = 0$ , in this equation, we get the position  $O$  of the zero of the scale,  $CO = -\frac{Q}{P} \cdot CG$ , or  $O$  is on the other side of  $C$  to  $G$ , and at a distance  $\frac{Q}{P} \cdot CG$  from it.

Hence  $nP \cdot AC = P \cdot OK,$

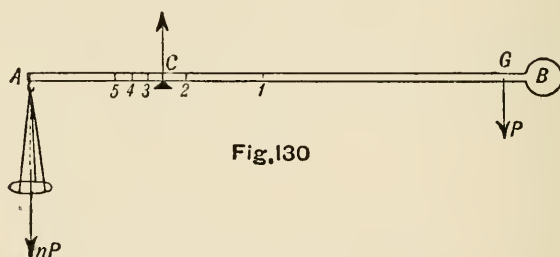
or  $OK = nAC.$

The graduations are obtained then by marking off distances from  $O$ , equal to  $AC$ ,  $2AC$ ,  $3AC$ , &c. By giving  $n$  fractional values we can obtain intermediate graduations.

152. *The Danish Steelyard.* This steelyard consists of a beam  $AB$ , terminating in a ball  $B$ ; from the end  $A$  hangs the scale-pan in which the body to be weighed is placed. The fulcrum  $C$  is moved until the weight placed in the scale-pan is counterbalanced by that of the steelyard. The beam is graduated so that the position of  $C$ , when the beam balances, gives the corresponding weight in  $A$ .

To obtain the graduations.

Let  $P$  be the weight of the steelyard and scale-pan,



acting through the point  $G$  of the steelyard. It is obvious that the zero graduation is at  $G$ , since the fulcrum must be at  $G$ , when the beam balances without any weight in the scale-pan.

Let  $C$  be the position of the graduation  $n$ , i.e. the point where the fulcrum is when there is a weight  $nP$  in the scale-pan, and the beam balances.

Taking moments about  $C$ , we have

$$nP \cdot AC = P \cdot CG = P (AG - AC),$$

$$\therefore AC = \frac{AG}{n + 1}.$$



Hence the graduations are at a distance from  $A$  equal to

$$\frac{AG}{2}, \frac{AG}{3}, \frac{AG}{4}, \&c.$$

Ex. 1. If the beam of a balance be horizontal, when there are no weights in the scale-pans, shew that if the balance be a false one, the actual weight of a body is the geometric mean of its apparent weights when weighed first in one scale-pan, and then in the other.

Ex. 2. If the arms of a false balance be without weight and one arm longer than the other by  $\frac{1}{3}$ th part of the shorter arm, and if in using it the substance to be weighed is put as often into one scale as the other, shew that the seller loses  $\frac{5}{9}$  per cent. on his transactions.

Ex. 3. If the bar of the common steelyard be 18 inches long, weigh 3 lbs. and be suspended at a point 3 inches from one extremity, what is the greatest weight which can be measured by a moveable weight of 2 lbs.? *Ans.* 16 lbs.

Ex. 4. A common steelyard is 12 inches long, and with the scale-pan weighs 1 lb., the centre of gravity of the two being 2 inches from the end to which the scale-pan is attached; find the position of the fulcrum when the moveable weight is 1 lb. and the greatest weight that can be ascertained by means of the steelyard is 12 lbs. *Ans.* 1 in. from scale-pan.

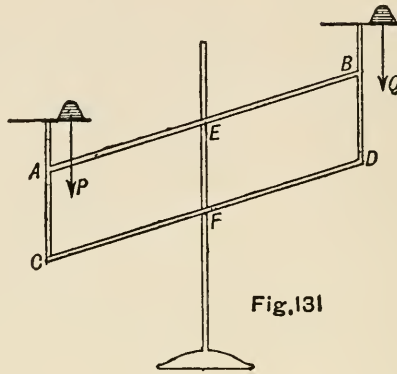
Ex. 5. The moveable weight of a common steelyard is 6 oz. A tradesman diminishes its weight by half an ounce: of how much is a person defrauded who buys what appears to weigh 6 lbs. by this steelyard? *Ans.*  $\frac{1}{2}$  oz.

Ex. 6. Find the length of a Danish steelyard, weighing 1 lb., when the distance between the graduations 4 lbs. and 5 lbs. is 1 inch. *Ans.* 30 in.

153. *Roberval's Balance.* This consists of four uniform rods,  $AB, BD, DC, CA$ , freely jointed at their extremities and forming a parallelogram. The rods  $AB, CD$  can turn about pivots at their middle points  $E, F$ , which are fixed in a vertical support. The rods  $AB, CD$  are similar in every respect, as are the rods  $AC, BD$ . Equal scale-pans are rigidly connected with  $AC$  and  $BD$ .

The peculiar advantage of this balance is that it does not matter whereabouts the scale-pans the weights to be compared are placed.

Let the weight  $P$ , when placed in the scale-pan attached to  $AC$ , counterbalance the weight  $Q$  placed in



the other scale-pan. If now the system be supposed displaced by the beams  $AB, CD$  turning through a small angle, it is clear that the centres of mass of  $AB, CD$  suffer no displacement, while that of  $BD$  and its scale-pan is raised or lowered through a vertical distance  $p$ , say, and the centre of mass of  $AC$  and its scale-pan is lowered or raised through the same distance. The virtual work done by the weight of  $BD$  will be equal to, but of opposite sign to, that done by the weight of  $AC$ . Also the algebraical sum of the virtual work done by the internal forces of the system is zero. The equation of virtual work is therefore  $Pp - Qp = 0$ , since  $P, Q$  move through the same vertical distance as  $AC$ , and  $BD$  viz.  $p$ ; therefore  $P = Q$ . This result holds wherever  $P$  and  $Q$  are placed in their respective scale-pans, i.e. whatever be their distances from the vertical support.

154. *The Differential Wheel and Axle.* In order to raise a very large weight by means of a comparatively small power, with the help of the ordinary 'wheel and axle', it would be necessary to make either the radius of the wheel inconveniently large, or else that of the axle so small that it would be unable to bear the strain put upon it. This difficulty is got over in the 'Differ-

ential Wheel and Axle'. This consists of two axles  $B$  and  $C$ , of different radii, rigidly connected together and

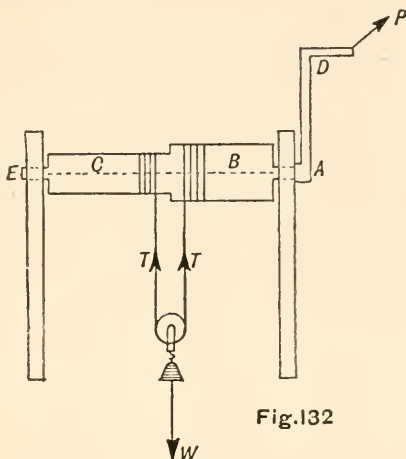


Fig. 132

turning about their common axis  $AE$ , which is horizontal and turns in fixed sockets. The power  $P$  is applied at right angles to the axis, and at the end of an arm  $AD$ , the 'wheel'; the weight  $W$  is attached to a pulley supported by a rope which is wrapped one way round  $B$ , and the other way round  $C$ :  $P$  and the rope round the thicker axle  $B$  tend to turn the machine in opposite directions.

To find the conditions of equilibrium.

Let  $a$ ,  $b$ ,  $c$  be the radii of  $AD$ ,  $B$ ,  $C$  respectively, and  $T$  the tension of the rope supporting the pulley.

Since the pulley is in equilibrium

$$2T = W.$$

Since the machine is in equilibrium, taking moments about the axis  $AE$ , we have

$$Pa - Tb + Tc = 0,$$

$$\therefore Pa = T(b - c) = \frac{W}{2}(b - c),$$

or

$$P : W = b - c : 2a.$$

Hence by making the radii of  $B$  and  $C$  as nearly equal as we please, the weight which a given power  $P$  can raise, may be increased to any extent.

The principle of work also enables us to obtain this result very easily.

155. *Hunter's Differential Screw.* This consists of a screw  $AD$  which works in a fixed nut  $CC'$ .  $AD$  is hollow and has a thread cut inside it, in which a solid screw  $DE$

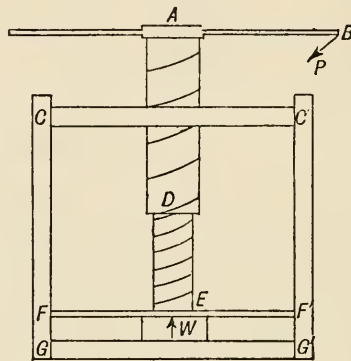


Fig. 133

works.  $DE$  is prevented from turning round by some means, for instance, by means of a rod  $FEF'$  rigidly connected with it, and whose ends work in smooth grooves, so that the screw  $DE$  can only move in a direction parallel to its axis.

The *weight*  $W$  is the resistance exerted by any substance placed between  $E$  and the base  $GG'$  of the framework  $CGG'C'$ . The *power*  $P$  is applied at the extremity of the arm  $AB$  which is at right angles to and rigidly connected with the screw  $AD$ .

Let  $a$  be the length of  $AB$ ,  $h$ ,  $h'$  the distances between consecutive threads of  $AD$ ,  $DE$  respectively.

Let us see the effect of the arm  $AB$  making a complete revolution.  $AD$  will clearly descend through a

distance  $h$ :  $DE$  cannot turn with  $AD$ , and therefore will move upwards relatively to  $AD$  through a space  $h'$ , i.e. will actually descend through a space  $h - h'$ : this is therefore the distance through which the weight is moved.

Let us suppose the virtual displacement made to be that which would be produced by  $P$  moving its point of application through a small angle  $\theta$ , so that in consequence the weight descends through a distance  $x$ : as the distance through which  $DE$  descends is proportional to the angle through which  $AD$  turns,  $x/(h - h') = \theta/2\pi$ . As  $P$  and  $W$  are the only forces that do work during the above displacement, the equation of virtual work is

$$P \cdot a\theta - Wx = 0,$$

$$\therefore P \cdot 2\pi a = W(h - h').$$

This relation might have been obtained by an extension of the method adopted in Art. 146.

It is clear that by making  $h$  and  $h'$  sufficiently nearly equal, we can make  $W/P$  as great as we please; whereas the same result is obtained in the simple screw only by making  $a$  inconveniently large, or by making  $h$  so small that the thread is too weak to support the pressure on it.

#### EXAMPLES ON CHAPTER VII.

1. If a power  $P$  acting horizontally will support a weight  $W$  on a plane of inclination  $\alpha$ , and would also support it on a plane of inclination  $\beta$ , acting parallel to the plane, the pressure on the plane in the former case being double that in the latter, prove that  $\alpha = \frac{1}{2} \cos^{-1}(\frac{1}{3})$ .

2. If in the first system there be two pulleys, the fixed ends only of the strings being parallel, and the power horizontal, prove that the mechanical advantage is  $\sqrt{3}$ .

3. In the first system, the weights of the pulleys beginning with the highest are in A. P. and a power  $P$  supports a weight  $W$ ; the pulleys are then reversed, the highest being placed lowest and so on, and now  $W$  and  $P$  when interchanged are in equilibrium: shew that  $n(W + P) = 2W'$ , where  $W'$  is the total weight of the pulleys and  $n$  is the number of them.



4. If there be  $n$  pulleys in the third system, and if the string which goes over the lowest have the end at which the power is usually hung, passed under another moveable pulley, over a fixed pulley, and then attached to the weight  $W$ ; and if the weight of each pulley be  $w$  and no other power be used, prove that  $W = (3 \cdot 2^{n-1} - n - 1) w$ .

5. In a weighing machine constructed on the principle of the common steelyard the pounds are read off by graduations reaching from 0 to 14, and the stones by weights hung at the end of the arm; if the weight corresponding to one stone be 7 oz., the moveable weight  $\frac{1}{2}$  lb., and the length of the arm one foot, prove that the distances between the graduations are  $\frac{3}{4}$  inches.

6. Shew that, in the third system, if there are  $n$  pulleys, each of diameter  $2a$  and weight  $w$ , the distance of the point of suspension of the weight from the line of action of the power is equal to

$$na \frac{2^{n+1} W + [(n-3) 2^n + n + 3] w}{2(2^n - 1) W}$$

7. In the first system of pulleys, shew that, if the weights of the pulleys are all equal, the equilibrium will not be affected by increasing  $P$ ,  $W$ , and the weight of each pulley, by the same amount.

8. A weight  $W$  is weighed by a common steelyard, but a weight  $Q$  is substituted for the proper moveable weight  $P$ . Shew that the error is  $(W - wb/a)(P - Q)/Q$ , where  $w$  is the weight of the steelyard, and  $b$ ,  $a$  the distances from the fulcrum of the centre of gravity and of the scalepan in which  $w$  is placed.

9. A false balance, the weight of whose beam may be neglected, has given weights in the pans, which weights are afterwards interchanged. In the two positions of equilibrium the beam makes complementary angles with the vertical. Shew that the line, joining the point of suspension to the middle point of the beam, makes with the beam twice the angle, that the beam makes with the vertical in one of its positions.

10. The weight of a common steelyard is  $Q$ , and the distance of its fulcrum from the point from which the weight hangs is  $a$ , when the instrument is in perfect adjustment; the fulcrum is displaced to a distance  $a + a$  from this end; shew that the correction to be applied to give the true weight of a body, which in the imperfect instrument appears to weigh  $W$ , is  $(W + P + Q) a / (a + a)$ ,  $P$  being the moveable weight.

11. If in the first system,  $P$  is the power (acting upwards),  $W$  the weight, and  $R$  the stress on the beam from which the pulleys hang, shew that  $R$  is greater than  $W(1 - 2^{-n})$  and less than  $(2^n - 1)P$ .



12. If on a steelyard the moveable weight  $P$  which forms the power be increased in the ratio  $1+k : 1$ , prove that the consequent error in  $W$ , the weight to be found, is  $kY$ , where  $Y$  is the weight that must be removed from  $W$  in order to preserve equilibrium when  $P$  is moved close to the fulcrum.

13. Prove that, if in a machine the weight can be supported by the friction alone, then in raising the weight half the power at least is wasted in overcoming friction.

Apply this to the differential pulley; and prove that if the weight can be supported by friction alone, the radius of the axle must be greater than the difference of the radii of the pulleys multiplied by the cosecant of the angle of friction.

14. A single moveable pulley, weight  $W$ , is just supported by the power  $P$ , which is applied at one end of a cord which goes under the pulley and is then fastened to a fixed point: shew that if  $\phi$  be the angle subtended at the centre by the part of the string in contact with the pulley, it is given by the equation

$$P(1 - 2\epsilon^{\mu\phi} \sin \phi + \epsilon^{2\mu\phi})^{\frac{1}{2}} = W.$$

15. A true balance is in equilibrium with unequal weights  $P, Q$  in its scales. If a small weight be added to  $P$ , the consequent vertical displacement of  $Q$  is equal to that which would be the vertical displacement of  $P$ , were the same small weight to be added to  $Q$  instead of to  $P$ .

16. Prove that in the third system, if the pulleys be small compared with the lengths of the strings, the necessary correction for the weights of the strings is the addition to  $W, P_2, P_3, \dots P_n$  respectively, of the weights of lengths  $h_2 + h_3 \dots + h_n + h, 2(h_2 - h_3), 2(h_3 - h_4), \dots 2(h_n - h)$  of string: where  $h_1, h_2, h_3, \dots h_n$  are the heights of the  $n$  pulleys (whose weights are  $p_1, p_2, \dots p_n$  respectively) above the line of attachment, supposed horizontal, of the strings to the weight  $W$ , and  $h$  the height of the point of attachment of the power above the same line.

17. In graduating a steelyard to weigh pounds marks are made with a file, a weight  $x$  being removed for each notch. With the moveable weight  $P$  at the end of the beam  $n$  lbs. can be weighed after the graduation is completed,  $(n+1)$  before it is begun, shew that  $n(n+1) = 2P/x$ , and find the error made in weighing  $m$  pounds. The c. g. of the steelyard is originally under the point of suspension.

18. An old Danish steelyard, originally of weight  $W$  lbs. and accurately graduated, is found coated with rust. In consequence of the rust, the apparent weights of two known weights of  $X$  lbs. and  $Y$  lbs. are found when weighed by the steelyard to be  $(X - x)$  lbs.,  $(Y - y)$  lbs. respectively. Prove that the centre of gravity of the rust divides the graduated arm in the ratio  $W(x - y) : Yx - Xy$ ; and that its weight is, to a first approximation,  $x(W + Y)/(X - Y) + y(W + X)/(Y - X)$ .

19. A brass figure  $ABDC$ , of uniform thickness, bounded by a circular arc  $BDC$  (greater than a semicircle) and two tangents  $AB, AC$  inclined at an angle  $2\alpha$ , is used as a letter-weigher as follows.  $O$  the centre of the circle is a fixed point, about which the machine can turn freely, and a weight  $P$  is attached to the point  $A$ , the weight of the machine itself being  $w$ . The letter to be weighed is suspended from a clasp (whose weight may be neglected) at  $D$  on the rim of the circle,  $OD$  being perpendicular to  $OA$ . The circle is graduated and is read by a pointer which hangs vertically from  $O$ : when there is no letter attached, the point  $A$  is vertically below  $O$ , and the pointer indicates zero. Obtain a formula for the graduation of the circle, and shew that if  $P = \frac{1}{3} w \sin^2 \alpha$ , the reading of the machine will be  $\frac{1}{3} w$  when  $OA$  makes with the vertical an angle equal to

$$\tan^{-1} \left\{ \frac{(\pi + 2\alpha) \sin^2 \alpha + 2 \sin \alpha \cos \alpha}{(\pi + 2\alpha) \sin^3 \alpha + 2 \cos \alpha} \right\}.$$

## APPENDIX.

1. IF a solid cube of finite size be cut by parallel planes into  $n$  slices of equal thickness, we can by sufficiently increasing  $n$  make the volume of each slice smaller than any assignable volume. The volume of a slice is in this case said to be ultimately an *indefinitely small quantity*.

An indefinitely small quantity, then, is one which though itself less than any assignable quantity, yet when multiplied by a sufficiently great number amounts to a finite quantity. It is often said to be *ultimately zero*, but it must be understood that it is not *absolute zero*, which does not amount to a finite quantity, however great a quantity it is multiplied by.

Let the above cube be now cut by planes parallel to another face, so that each slice is divided into  $n$  equal prisms, each having square ends. Again, let the cube be cut by planes parallel to a third face, so that each prism is divided into  $n$  equal cubes. The total number of cubes is  $n^3$ , of prisms  $n^2$ , and of slices  $n$ ; and it requires  $n$  prisms to make a slice, and  $n^2$  cubes. It follows then that, when  $n$  is increased indefinitely, a slice, a prism, and a cube become all indefinitely small, but that though  $n$  slices make up a finite volume,  $n$  prisms do not, and though the sum of  $n^2$  prisms is finite, that of  $n^2$  cubes is indefinitely small. Therefore the ratio of a prism to a slice is indefinitely small, and also that of a cube to a prism, and *à fortiori* that of a cube to a slice. This is usually expressed by saying that a slice, a prism, and a cube are respectively of the *first, second and third orders* of indefinitely small quantities.

One indefinitely small quantity is *of a higher order* than another, when the ratio of the first to the second is indefinitely small.

Two quantities are equal when their difference is indefinitely small compared with either: i.e. two finite quantities are equal when their difference is an indefinitely small quantity, and two indefinitely small quantities are equal when their difference is a small quantity of higher order.

When we assert that the algebraical sum of a finite number of indefinitely small quantities is zero, we are not stating a truism, but mean that they are so related that their algebraical sum is of a higher order than that of the quantities involved.

2. *Prop.* If two series, consisting of the same number of indefinitely small quantities of the same order, are such, that each term of the one bears to the corresponding term of the other a ratio differing from  $k$  (a finite quantity) by an indefinitely small quantity, the sum of the one series is  $k$  into the sum of the other.

Let  $a_1, a_2, \dots a_n$  be the first series,  $b_1, b_2, \dots b_n$  the second, so that

$$\frac{a_1}{b_1} = k + c_1, \quad \frac{a_2}{b_2} = k + c_2, \dots \frac{a_n}{b_n} = k + c_n,$$

where  $c_1, c_2, \dots c_n$  are indefinitely small: let  $c$  be the greatest of these quantities.

Then

$$a_1 + a_2 + \dots a_n = k(b_1 + b_2 + \dots b_n) + b_1 c_1 + b_2 c_2 + \dots b_n c_n;$$

$$\therefore \Sigma(a) - k \Sigma(b) \text{ is not } > c \Sigma(b);$$

$$\therefore \Sigma(a) = k \Sigma(b),$$

since  $c \Sigma(b)$  is indefinitely small compared with  $k \Sigma(b)$ .

*Cor.* Hence two infinite series of indefinitely small quantities of the first order, such that each term of the one differs from the corresponding term of the other by a quantity of the second order, are equal.

This explains why in Arts. 97, 99, 101 and 102 we have neglected one infinite series and retained another:

this is done when the first series is of a higher order than the second.

3. As an illustration of these principles we will give a proof of Guldin's theorems.

One theorem is, that the volume, generated by the complete revolution of a plane area about any straight line in its plane and not cutting it, is equal to that of a right cylinder whose section is the plane area and height the length of the path described by the centre of mass of the area.

Draw a number of straight lines at right angles to the line  $AB$ , about which the revolution takes place, dividing the area  $S$  into  $n$  strips of equal breadth. Let  $Pp, Qq$  be two consecutive lines of this system, typical of the rest,  $M, N$  the points where they meet  $AB$ .

Draw  $PR, pr$  perpendicular to  $Qq$ .

The volume, generated by the revolution of  $PRrp$  about  $AB$ , differs from that generated by  $PQqp$  by the volumes generated by the two curvilinear triangles  $PQR, pqr$ .

But when  $n$  is increased indefinitely, the breadth only of the rectangle is diminished indefinitely, whereas both length and breadth of each triangle is diminished indefinitely; the volumes generated by the latter are therefore of a higher order than that generated by the former.

Hence the total volume generated by the area equals the sum of the volumes generated by the rectangles of which  $Pr$  is a type, i.e.

$$\begin{aligned} &= \Sigma (\pi PM^2 \cdot MN - \pi pM^2 \cdot MN) \\ &= \pi \Sigma \{(PM - pM)(PM + pM)MN\} \\ &= \pi \Sigma \{Pp \cdot MN(PM + pM)\}. \end{aligned}$$

Also the sum of the areas of the rectangles is the area of the figure  $S$ ; and since they differ by the sum of the areas of the triangles  $PQR, pqr$ , &c., which are of a higher order than the rectangles, the centres of mass of the sum of the rectangles and the figure  $S$  must be coincident.



Therefore  $x$ , the distance of the c. m. of  $S$  from  $AB$

$$\begin{aligned} &= \frac{\Sigma \{Pp \cdot MN \cdot \frac{1}{2}(PM + pM)\}}{\Sigma (Pp \cdot MN)} \\ &= \frac{\frac{1}{2} \text{ vol. generated by } S}{\pi \times \text{area } S}, \end{aligned}$$

$\therefore$  volume generated by  $S = S \cdot 2\pi x$ .

The second theorem is, that the area of the surface, generated by the revolution of a curve about any straight line in its plane and not cutting the curve, is equal to the rectangle, whose length is the length of the curve and breadth the distance of the curve's centre of mass from the straight line.

Let  $PQ$  be a side of a polygon, either inscribed within or circumscribed about the curve: let  $R$  be the middle point of  $PQ$ , and therefore its centre of mass. Draw  $RK$  perpendicular to the line  $AB$ , about which the curve revolves.

As in Art. 99, it can be shewn that the area of the surface generated by the revolution of  $PQ$  about  $AB$  is  $2\pi PQ \cdot RK$ .

Therefore the total surface generated by the revolution of the polygon about  $AB$

$$\begin{aligned} &= \Sigma (2\pi PQ \cdot RK) \\ &= 2\pi \Sigma (PQ \cdot RK) \\ &= 2\pi x \times \text{perimeter of polygon,} \end{aligned}$$

where  $x$  is the distance of its centre of mass from  $AB$ .

When the lengths of the sides of the inscribed and circumscribed polygons are diminished indefinitely and their number increased indefinitely, their perimeters differ by indefinitely small quantities, and their centres of mass become coincident. The surfaces generated by each are therefore equal.

It is assumed as axiomatic, that as the perimeter of the curve lies in position between the two polygons which ultimately coincide, it is equal to the perimeter of either



polygon, its centre of mass coincides with that of either polygon, and the surface generated by it is equal to that generated by either polygon.

Hence the surface generated by the curve is equal to the product of the length of the curve into the length of the path traced out by its centre of mass.

Each of Guldin's theorems can easily be extended to the case in which the revolution is not a complete one. There is no limitation in either as to the number of times, in which a straight line at right angles to  $AB$  cuts the generating curve.

Ex. Find the volume and surface of an anchor-ring, the figure generated by the revolution of a circle about a line in its plane, and not intersecting it.

Ans. Vol. =  $2\pi^2 a^2 c$ , surface =  $4\pi^2 ac$ , where  $a$  is the radius of the circle, and  $c$  the distance of its centre from the line.

4. To prove that the limit of

$$\frac{1^p + 2^p + 3^p + \dots (n-1)^p}{n^{p+1}} = \frac{1}{p+1},$$

where  $p$  is any positive quantity, and  $n$  is increased indefinitely.

Let  $S_p$  denote  $1^p + 2^p + 3^p + \dots (n-1)^p$ .

$$n^{p+1} - (n-1)^{p+1} = (p+1)(n-1)^p + \frac{(p+1)p}{2!}(n-1)^{p-1} + \&c.$$

$$(n-1)^{p+1} - (n-2)^{p+1} = (p+1)(n-2)^p + \frac{(p+1)p}{2!}(n-2)^{p-1} + \&c.$$

..... = .....

$$2^{p+1} - 1^{p+1} = (p+1)1^p + \frac{(p+1)p}{2!}1^{p-1} + \&c.$$

$\therefore$  by addition

$$n^{p+1} - 1^{p+1} = (p+1)S_p + \frac{(p+1)p}{2!}S_{p-1} + \frac{(p+1)p(p-1)}{3!}S_{p-2} + \&c.$$

$$\begin{aligned} \therefore \frac{1}{p+1} &= \frac{1}{(p+1)n^{p+1}} + \frac{S_p}{n^{p+1}} \\ &+ \frac{p}{2!} \cdot \frac{1}{n} \cdot \frac{S_{p-1}}{n^p} + \frac{p(p-1)}{3!} \cdot \frac{1}{n^2} \cdot \frac{S_{p-2}}{n^{p-1}} + \&c., \end{aligned}$$

But  $\frac{S_p}{n^{p+1}}$  is obviously  $< \frac{(n-1)^{p+1}}{n^{p+1}}$ , i.e. is  $< 1$ .

Similarly  $\frac{S_{p-r}}{n^{p-r+1}}$  is  $< 1$ , if  $p$  is  $> r$ .

Hence, when  $p$  is integral,

$$\frac{1}{p+1} = \frac{S_p}{n^{p+1}} + \frac{A_1}{n} + \frac{A_2}{n^2} + \frac{A_3}{n^3} + \dots + \frac{A_{p+1}}{n^{p+1}},$$

where  $A_1, A_2, A_3, \&c.$  are all finite quantities;

$$\therefore \frac{S_p}{n^{p+1}} = \frac{1}{p+1}, \text{ when } n \text{ is increased indefinitely.}$$

If  $p$  be fractional

$$\frac{S_{p-r}}{n^{p-r+1}} = 0 \text{ ultimately, when } p \text{ is } > r,$$

$$\text{when } p \text{ is } < r, \frac{S_{p-r}}{n^{p-r+1}} \text{ is } < \frac{1}{n^p};$$

$$\therefore \frac{1}{p+1} - \frac{S_p}{n^{p+1}} \text{ is numerically } < \frac{1}{n^p} \left\{ \frac{p}{2!} + \frac{p(p-1)}{3!} + \&c. \right\};$$

$$\text{i.e. } < \frac{1}{(p+1)n^p} \left\{ (1+1)^{p+1} - 1 - \frac{(p+1)}{1!} \right\};$$

$$\text{i.e. } = 0 \text{ ultimately.}$$

Hence the result holds, whether  $p$  is integral or not.  $\times$

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